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ຕ STATIC TESTS OF SEGMENTS OF ₩ TUNNEL LININGS 34

Volume II - Data

Merritt CASES, Incorporated

▼ P.O. Box 1206

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Redlands, California 92373

30 June 1979

Final Report for Period 14 February 1977-30 June 1979

CONTRACT No. DNA 001-77-C-0143

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Tunnel Linings	Static Te	sts
Composite-Intergral Linings	Material	Properties
Voussoir Block Linings		
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structures fielded in the MIGHTY		
new structural concepts: the com		
new serviceural concepts. the con	prione timer and	the fouggott block tillel.

#### PREFACE

The work reported herein was accomplished under Contract No. DNA001-77-C-0143 with Headquarters, Defense Nuclear Agency. The Contracting Officers Representatives were LTC Danny N. Burgess, USAF, who was replaced by LTC John C. Galloway, USAF, when LTC Burgess reported to the Air Staff College. The interest and assistance of LTC Burgess and Galloway throughout the work is gratefully acknowledged. Also acknowledged is the assistance of Dr. E. Sevin, Director of Strategic Structures Division of the Shock Physics Directorate.

Fabrication of the steel components of the segments was performed by Rettig Machine Shop, Redlands, California, under the direction of D. F. Rettig. Design and casting of the cellular concrete inserts for use in the compliant liner was performed by the United States Army Waterways Experiment Station, Vicksburg, Mississippi, under the direction of R. L. Denson.

Actively working on the program at CASES, in addition to the writers, were: Gilbert W. Lo, Michael F. Mullins and several student interns from the Department of Engineering, University of Redlands, Redlands, California. The late Frank W. Galbraith of CASES completed the original conceptual design of the loading and reaction system.

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DDC	Buff Section
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# Conversion factors for U.S. customary to metric (SI) units of measurement.

To Convert From	То	Multiply By
angstrom	meters (m)	1. 000 000 X E -10
atmosphere (normal)	kilo pascal (kPa)	1.013 25 XE+2
bar	kilo pascal (kPa)	1.000 000 X E + 2
barn	meter <sup>2</sup> (m <sup>2</sup> )	1.000 000 X E -28
British thermal unit (thermochemical)	joule (J)	1.054 350 X E +3
calorie (thermochemical)	joule (J)	4. 184 000
cal (thermochemical)/cm <sup>2</sup> .	mega joule/m <sup>2</sup> (MJ/m <sup>2</sup> )	4. 184 000 X E -2
curie	*giga becquerel (GBq)	3. 700 000 X E +1
degree (angle)	radian (rad)	1. 745 329 X E -2
degree Fahrenheit	degree kelvin (K)	$t_{K} = (t^*f + 459.67)/1.8$
electron volt	joule (J)	1.602 19 X E -19
erg	joule (J)	1.000 000 X E -7
erg/second	watt (W)	1. 000 000 X E -7
foot	meter (m)	3.048 000 X E -1
foot-pound-force	joule (J)	1. 355 818
gallon (U.S. liquid)	meter <sup>3</sup> (m <sup>3</sup> )	3. 785 412 X E -3
inch	meter (m)	2. 540 000 X E -2
jerk	joule (J)	1.000 000 X E +9
joule/kilogram (J/kg) (radiation dose absorbed)	Gray (Gy)	1.000 υ00
kilotons	terajoules	4.183
kip (1000 lbf)	newton (N)	4, 448 222 X E +3
kip/inch <sup>2</sup> (ksi)	kilo pascal (kPa)	6. 894 757 X E +3
ktap	newton-second/m <sup>2</sup> (N-s/m <sup>2</sup> )	1.000 000 X E + 2
micron	meter (m)	1 000 000 X E -6
mil	meter (m)	2.540 000 X E -5
mile (international)	meter (m)	1.609 344 X E +3
ounce	kilogram (kg)	2, 834 952 X E -2
pound-force (lbs avoirdupois)	newton (N)	4. 448 222
pound-force inch	newton-meter (N-m)	1. 129 848 X E -1
pound-force/inch	newton/meter (N/m)	1.751 268 X E +2
pound-force/foot <sup>2</sup>	kilo pascal (kPa)	4. 788 026 X E -2
pound-force/inch <sup>2</sup> (psi)	kilo pascal (kPa)	6, 894-757
pound-mass (lbm avoirdupois)	kilogram (kg)	4. 535 924 X E -1
pound-mass-foot <sup>2</sup> (moment of inertia)	kilogram-meter <sup>2</sup> (kg·m <sup>2</sup> )	4. 214 011 X E -2
pound-mass/foot <sup>3</sup>	kilogram/meter <sup>3</sup> (kg/m <sup>3</sup> )	1, 601 846 X E +1
rad (radiation dose absorbed)	**Gray (Gy)	1,000 000 X E -2
roentgen	coulomb/kilogram (C/kg)	2, 579 760 X E -4
shake	second (s)	1 000 000 X E -×
slug	kilogram (kg)	1, 459 390 X E +1
torr (mm Hg, 0°C)	kilo pascal (kPa)	1,333 22 X E -1

<sup>\*</sup>The becquerel (Bq) is the SI unit of radioactivity; 1 Bq - 1 event/s.

\*\*The Gray (Gy) is the SI unit of absorbed radiation.

A more complete listing of conversions may be found in "Metric Practice Guide E 380-74," American Society for Testing and Materials.

# TABLE OF CONTENTS

Section			Page
1.	INTR	ODUCTION	5
2.	TEST	PROGRAM	6
	2.1	TEST PROCEDURE	6
	2,2	TEST APPARATUS	6
	2.3	DATA ACQUISITION	10
	2.4	TEST ARTICLES	13
3.	TEST	DATA	19
	3.1	STEEL LINER	21
		3.1.1 Specimen #0	21
		3.1.2 Reload of Specimen #J	42
	3.2	C-Y-16 MODELS	63
		3.2.1 Specimen #1	63
		3.2.2 Specimen #2	94
		3.2.3 Specimen #4	125
		3.2.4 Reload of Specimen #4	149
		3.2.5 Specimen #3	173
	3.3	COMPLIANT LINER	203
		3.3.1 Specimen #10	203
		3.3.2 Reload of Specimen #10	213
	3.4	C-X-9 MODELS	223
		3.4.1 Specimen #5	223
		3.4.2 Reload of Specimen #5	247
		3.4.3 Reload of Specimen #5	271
		3.4.4 Specimen #6	295
		3.4.5 Specimen #8	323
		3.4.6 Specimen #9	353
	3.5	VOUSSOIR BLOCK LINER	377
		3.5.1 Specimen #7	377

#### SECTION 1

#### INTRODUCTION

Volume II presents the complete set of reduced data obtained from the initial series of 16 quasi-static tests of segments of cylindrical tunnel linings. These linings represent several advanced rock opening reinforcement concepts proposed for use in deep-based protective facilities in rock. Test specimens included a steel liner to evaluate the test apparatus and scale models of two composite integral structures fielded by Merritt CASES, Inc. (CASES) in the MIGHTY EPIC structures add-on experiment conducted at the Department of Energy's Nevada Test Site (NTS). In addition, two new structural concepts were also tested: the "compliant lining" and the "voussoir block" or segmented lining.

This volume is organized into three main sections. The first section is the introduction. The second section provides a brief summary of the testing program, including descriptions of the testing apparatus, the data acquisition system and the various test articles. The final section furnishes the actual data obtained during the tests. The data is presented in the form of Cal-Comp plots of applied load distribution, applied load versus strain and applied load versus diametral displacements. A brief description of each test specimen and instrumentation location is given for each test. Also, a computer printout of the actual data points used in generating the plots is included for completeness.

The tests are arranged in chronological order. The data are also grouped into sub-sections based on the five different types of models tested. These models are discussed in Section 2.

#### SECTION 2

#### TEST PROGRAM

#### 2.1 TEST PROCEDURE

The principle objective of the tests of segments program was to determine the detailed behavior of several different types of sophisticated lining segments subjected to carefully controlled loading histories. A test procedure was devised in which a radial load distribution, consisting of a superposition of a uniform component and a sinusoidally varying component, was applied to the outer surface of the test specimen in an incremental fashion. A loading ratio was used to specify the particular load distribution used during a test. This loading ratio was defined as the quotient of the minimum and maximum amplitudes of the total applied load as shown in Figure 2.1.

#### 2.2 TEST APPARATUS

The loading system consisted of 16 hydraulic jacks, eight of 100-ton (890 kN) and eight of 150-ton (1330 kN) nominal capacity, resulting in a total load capacity of four million pounds (17.8 MN). For the test specimen dimensions used in this program, this load capacity translated into an equivalent hydrostatic pressure capability of approximately 2000 psi (13.8 MPa). The jacks were supported at their base by a reaction system consisting of a heavy steel ring, weighing approximately 18,000 pounds (80 kN), capable of withstanding at any point a diametrically opposed force of 300 tons (2660 kN) with a "factor of safety" of approximately four (stiffness was considered at least as important as strength in the original design). Figure 2.2 is a detailed drawing of the reaction system showing several jacks in place in the support ring as well as details of the ring cross-section. The 16 jacks were equally spaced around the circumference of the support ring. They, in turn, loaded the exterior surface of the cylindrical test specimen as shown in Figure 2.3. The 16 jacks were controlled through a 10-channel Edison

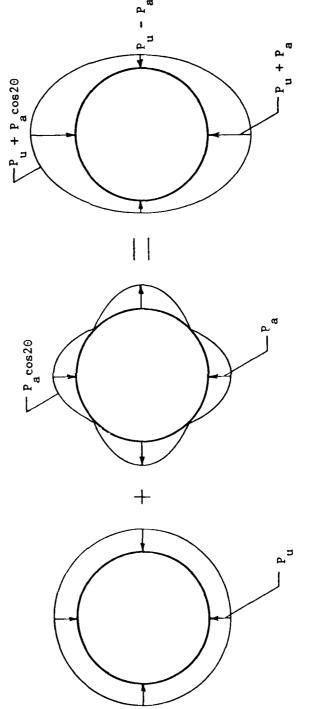


Figure 2.1 Schematic of loading distribution used in tests of segments.

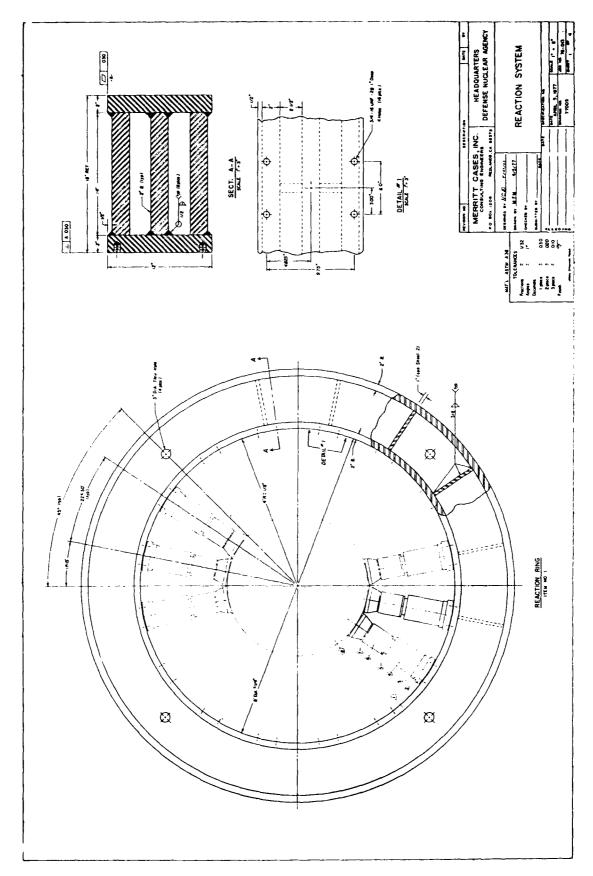


Figure 2.2 Reaction system for test of segments.

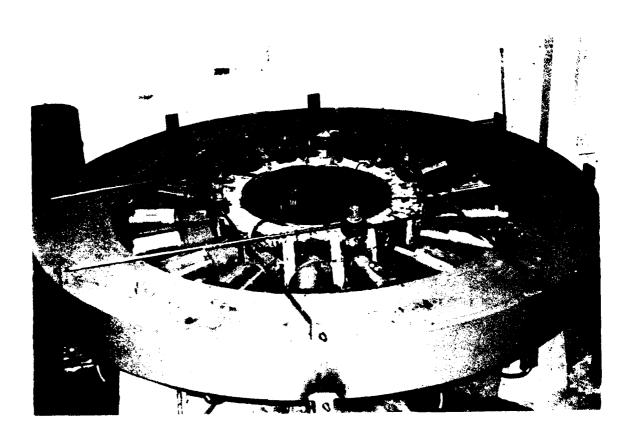


Figure 2.3 Reaction system with test specimen in place.

hydraulic controller, but only five channels were used because of symmetry of the load distributions used in the test program.

#### 2.3 DATA ACQUISITION

Instrumentation typically consisted of eight displacement gages to measure changes in diameter between each of the points at which the load is applied; 12 strain gages to measure strain at selected points on the test specimen; eight cells to measure load under one of the matching pairs of jacks and 16 measurements of torque and drift of the specimen being tested within the support ring.

The data acquisition system if shown in Figure 2.4. This block diagram presents the typical configuration used during the segment testing. Different specimen designs resulted in changes in both the number and location of strain gages. A schematic showing typical gage locations is shown in Figure 2.5.

The primary recording was accomplished with the Fluke Data Logger which produced a printed paper tape output. Approximately 40 channels were recorded on each test. These were sampled sequentially and printed and displayed at  $2\frac{1}{2}$  samples per second. An X-Y plot of applied load versus deflection (or strain) was also generated for monitoring and control during each test.

The eight 300k load cells remained in the same positions throughout the test program with each cell measuring axial load in a pair of opposing rams. Since these  $180^{\circ}$  pairs were connected together hydraulically, the loads imposed on opposite sides of the test items were continuously equalized. Dummy load cells were installed on the opposing rams to act as permanent spacers.

Retention rods were attached to the specimen loading blocks at the major and minor axes to restrict lateral or rotational movement of the test item. These 16 rods, mounted top and bottom, were strain gaged to monitor

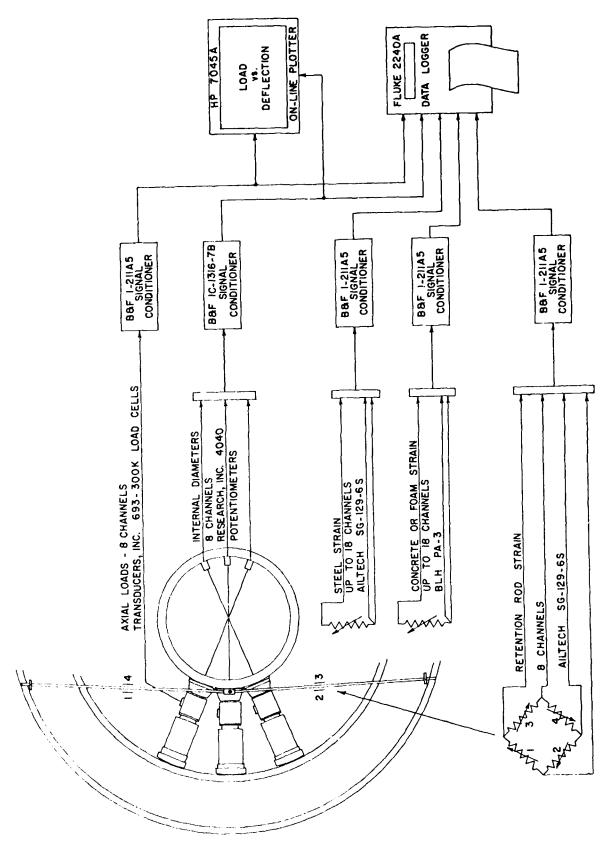
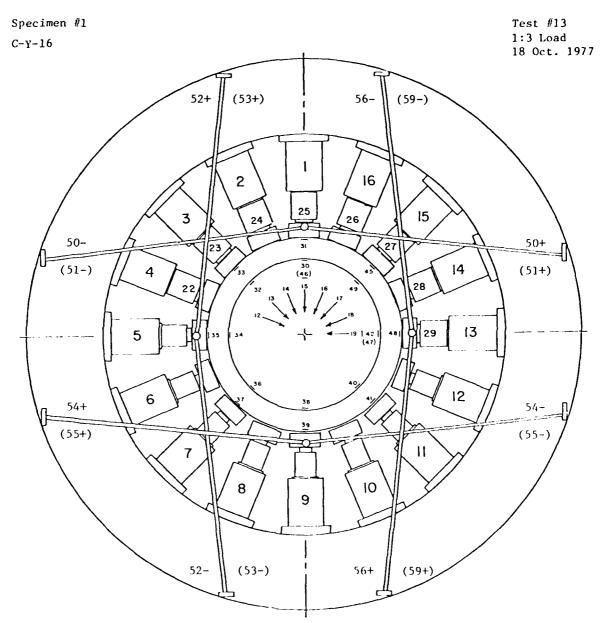


Figure 2.4 Data acquisition system.

# REACTION FRAME TEST SET-UP



- CH 12-19 Load axis I.D. (Research, Inc. Model 4040).
- CH 22-29 Axial load (Transducers, Inc. Model 693-300K).
- CH 30-42, 45-49 (Ailtech SG 129-6S) Radial pairs 2" from top, except 46-47 2" from bottom. Odd gages 31-45 and 48 on rebar.
- CH 50-56, and 59 (Ailtech SG 129-68) Polarity indicates rod under tension. Lower rod shown (XX).

Figure 2.5 Typical instrumentation layout for tests of segments.

and record the tension forces imposed during the test. The strain gages on each two opposing rod assemblies were connected into a single four-arm bridge such that tension could be measured in either rod with the output polarity indicating the direction of force. The strain level in each rod was also monitored automatically by the data logger and an alarm was triggered if the load exceeded a pre-set limit. This safety feature prevented excessive build-up of unbalanced forces as the specimens yielded which could have produced a dangerous, catastrophic failure.

The eight specimen diameters at each load axis were continuously monitored with cable-type potentiometers. These were mounted inside each specimen or on top depending on the configuration of the model. Steel strains were measured using Ailtech weldable strain gages.

After each test was completed, data from the logger was transferred to punched cards for processing in the IBM 360 computer at the University of California, Riverside, Computer Center. A special data reduction software package developed specifically for the CASES data acquisition system decommutated the data and automatically plotted results using an off-line Cal-Comp drum plotter. Programs provided for plotting any function versus another function; that is, load versus strain, load versus displacement, strain versus displacement, etc. Typical generated plots for the tests of segments program included a polar plot of incremented load distribution, load versus strain and load versus displacement. Overall data reduction turn-around for a typical segment test was generally accomplished within a 24 hour period once the system was automated.

#### 2.4 TEST ARTICLES

The test program was composed of five different structural types of lining segments: a steel lining, two composite integral linings, a compliant lining and a voussoir block lining. All specimens were 12 inch (305 mm) long segments of cylindrical linings. The steel lining was one inch (25.4 mm)

thick and 44.25 inches (1.12 m) in diameter. This lining was used for initial checkout of the reaction system. The composite integral specimens were scale models of two MIGHTY EPIC structures designated C-Y-16 and C-X-9 as shown in Figures 2.6 and 2.7. The compliant and voussoir block specimens were models of a proposed configuration for each of these special types of linings. Details of the compressible insert of the compliant lining and a segment of the voussoir block lining are shown in Figures 2.8 and 2.9, respectively.

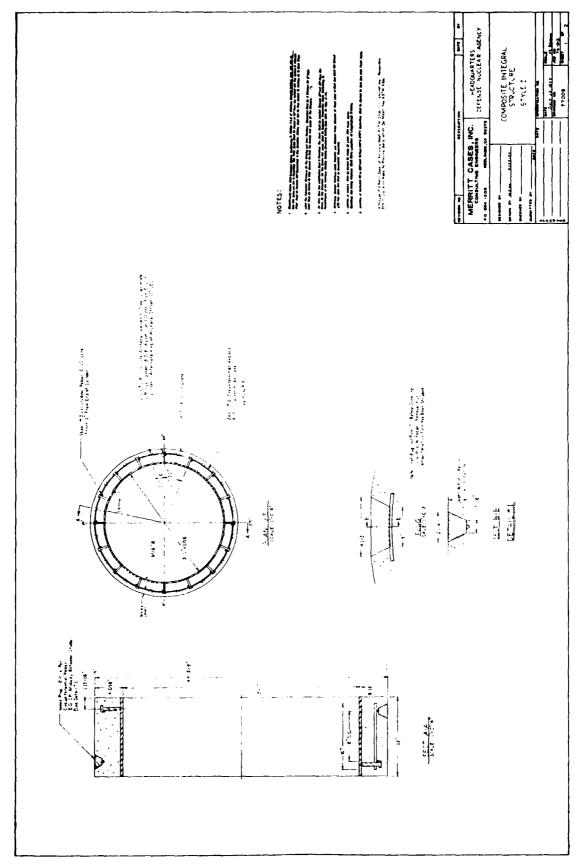


Figure 2.6 Details of MIGHTY EPIC C-Y-16 test specimen.

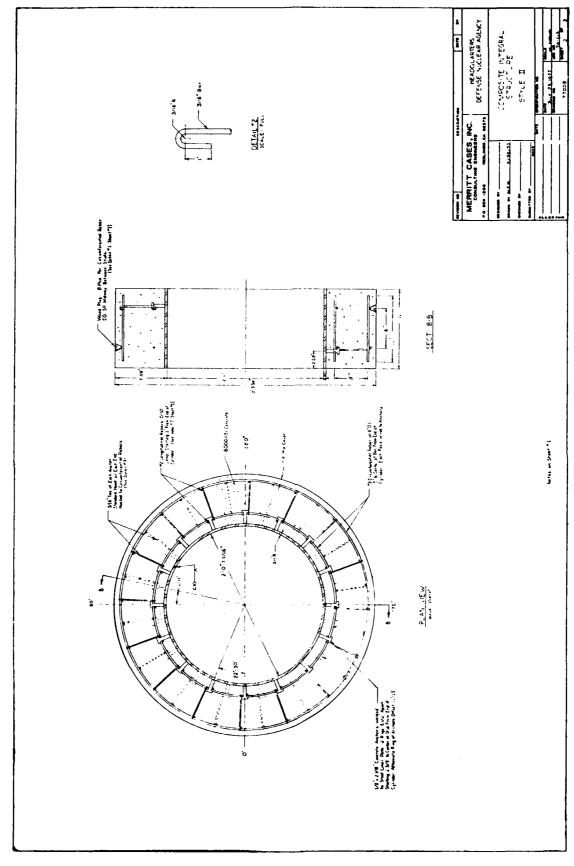


Figure 2.7 Details of MIGHTY EPIC C-X-9 test specimen.

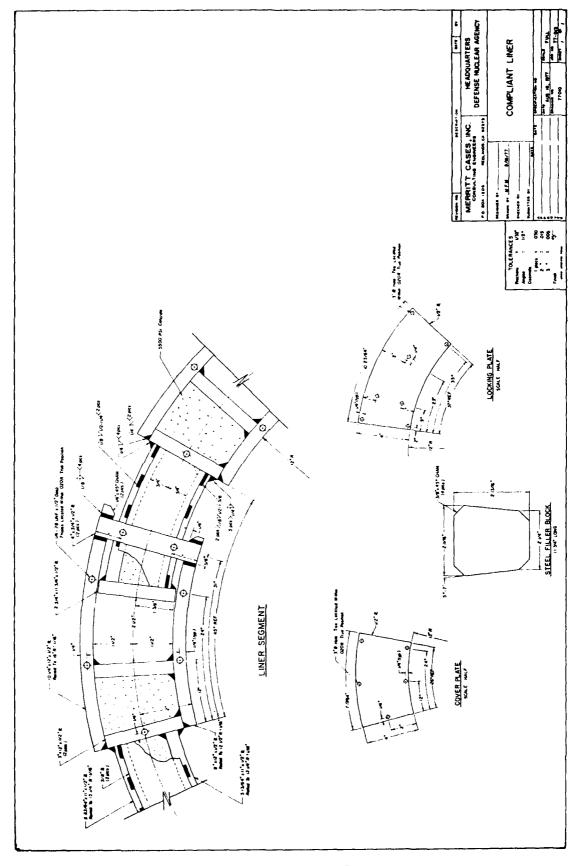


Figure 2.8 Details of compliant lining compressible insert.

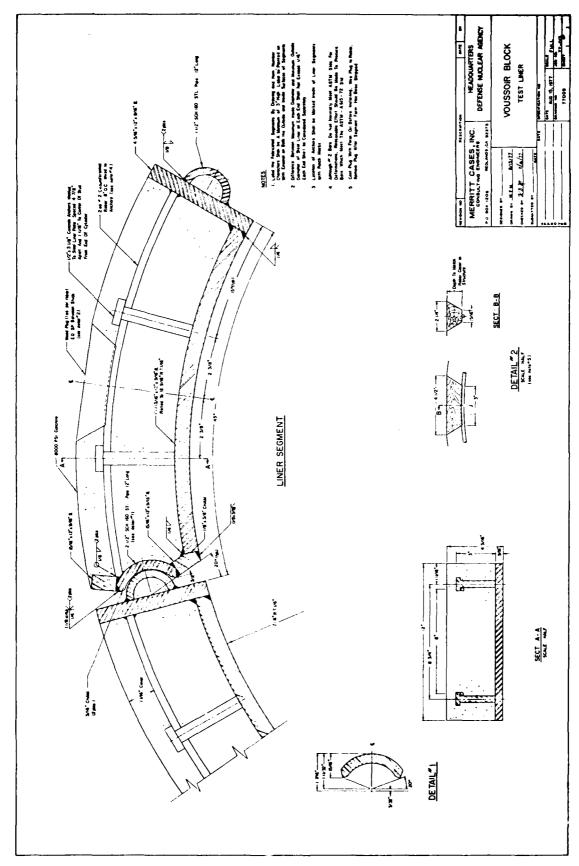


Figure 2.9 Details of voussoir block.
liner segment.

### SECTION 3

#### TEST DATA

The complete set of data for the test program is presented in this section. The data is arranged into groups determined by structural type. A summary of the test program is given by the test matrix shown in Table 1.

STATIC TESTS OF SEGMENTS
OF TUNNEL LININGS

				ŢE	TEST MATRIX						
TEST 1 NO.	STRUCTURE	SPECIMEN NO.	DESCRIPTION	HUDEL SCALE	1. p.	0.D.	نا	DRAWING NO.	TEST DATE	LOAD	MAX. RAM LOAD kipe (kN)
12 180	Steel Liner	0	System Check-	!	42 1/4"	44 1/4"	1,71	:	10-8-77	1:1	50 (222)
12 2nd	Steel Liner	0	Reload		42 1/4"	44 1/4"	12	:	10-10-77	1:1	100 (448)
C1	Composite Integral	-	C-Y-16 Model	3/4	36"	14 5/8"	12"	77008-1	10-18-77	1:3	43 (191)
16	Composite Integral	2	C-Y-16 Model	3/4	36"	.8/5 77	12"	77008-1	10-27-77	1:2	84 (374)
50	Composite Integral	•	C-Y-16 Model	3/4	36"	.8/5 77	12	77008-1	11-7-77	1:1	199 (885)
21	Composite Integral	4	Reload	3/4	36"	8/5 77	12	77006-1	11-8-77	1:1	223 (992)
2	Composite Integral	m .	C-Y-16 Model 2	3/,5	36"	14 5/8"	12"	77608-12	11-22-77	1:2	63 (280)
22	Compliant Liner	10	Test Model	;	24"	32"	12	77010	12-15-77	1:1	117 (520)
56	Compliant	10	Reload		24"	32"	12	77010	12-19-77	1:1	135 (601)
32	Composite Integral	5	C-X-9 Nodel	1/2	24"	39 3/4"	12"	77008-2	2-24-78	1:3	300 (1330)
£	Composite Integral	S	Reload	1/2	24"	39 3/4"	12"	77008-2	3-8-78	1:3	298 (1325)
36	Composite Integral	5	Reload	1/2	24"	39 3/4"	12"	77008-2	3-8-78	1:4	269 (1200)
ε	Composite Integral	•	C-X-9 Model	1/2	24"	39 3/4"	12"	77008-2	4-12-78	1:4	300 (1330)
36	Composite Integral	60	C-X-9 Nodel	1/2	24"	39 3/4"	12	77008-2	4-25-78	1:5	195 (867)
37	Composite Integral	σ.	C-X-9 Model	1/2	24"	39 3/4"	12"	77008-2	5-3-78	1:4	202 (899)
38	Voussofr Block	7	Test Podel	-	36"	.8/5 77	12	7,009	5-31-78	1:1	176 (783)
									-		

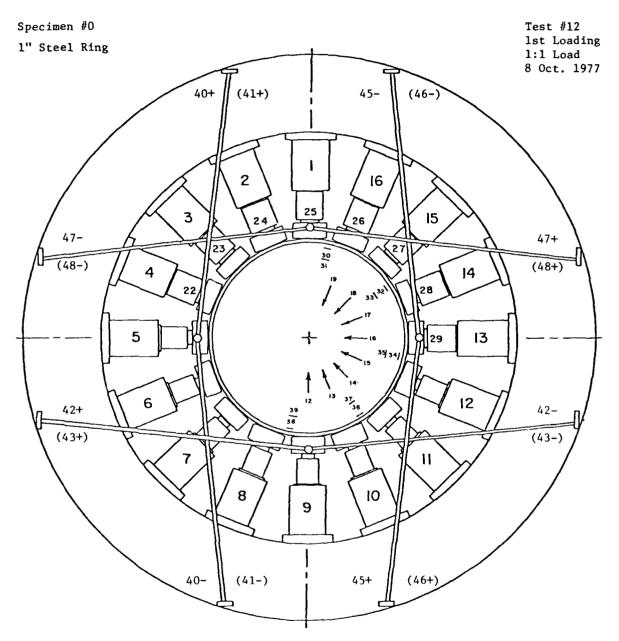
2. Without Concrete Studs 1. Test Nos. are assigned serially for the lab.; not for each program.

TABLE 1. Fest matrix.

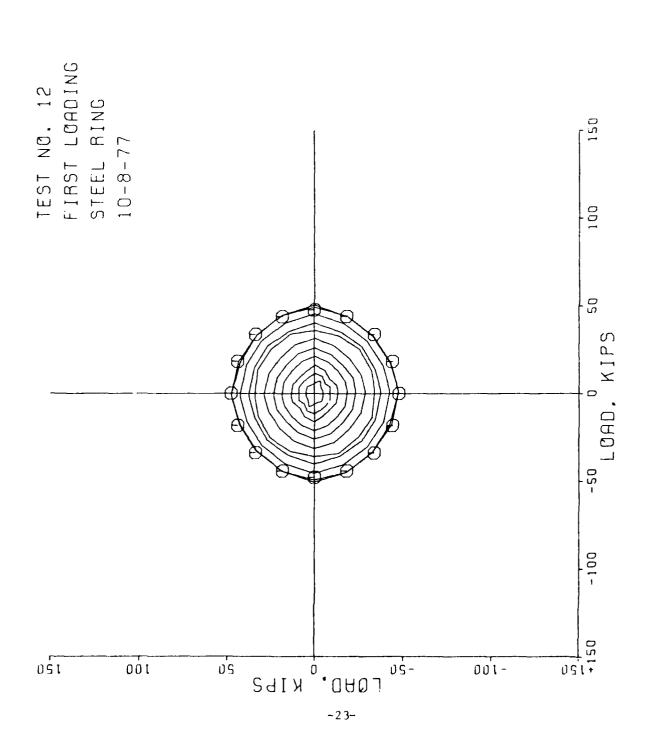
# 3.1 STEEL LINER 3.1.1 SPECIMEN #0

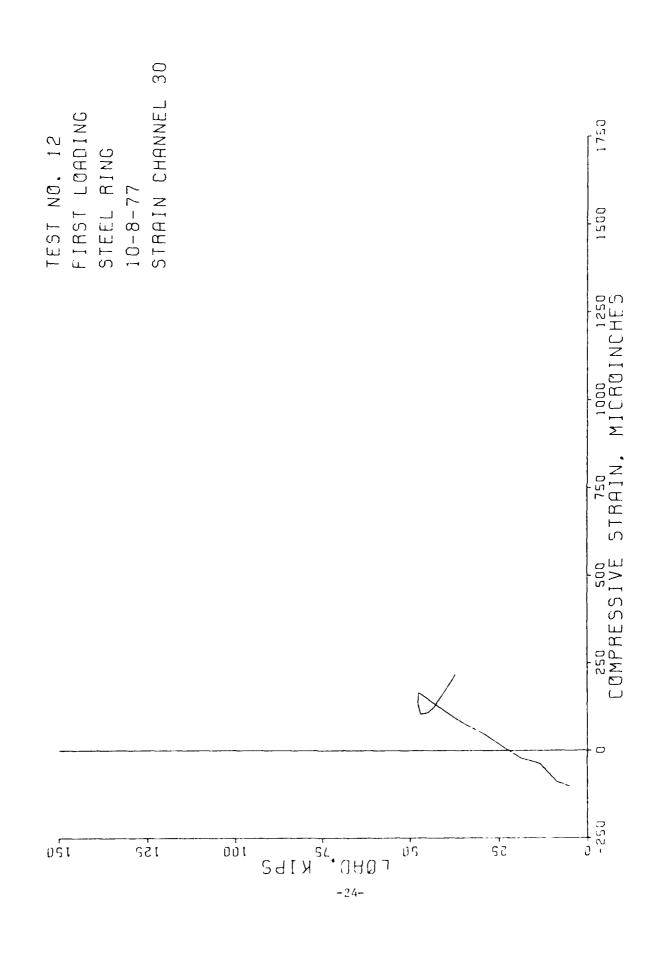
TEST NO. 12 (1st)
STEEL LINER
1:1 LOADING RATIO
TESTED 8 OCTOBER 1977

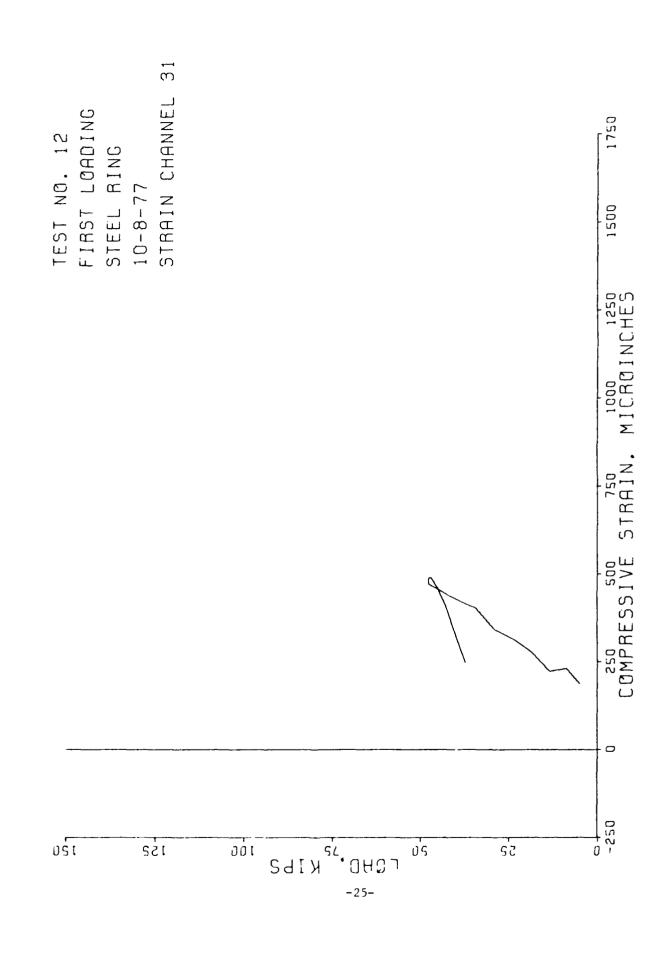
# REACTION FRAME TEST SET-UP

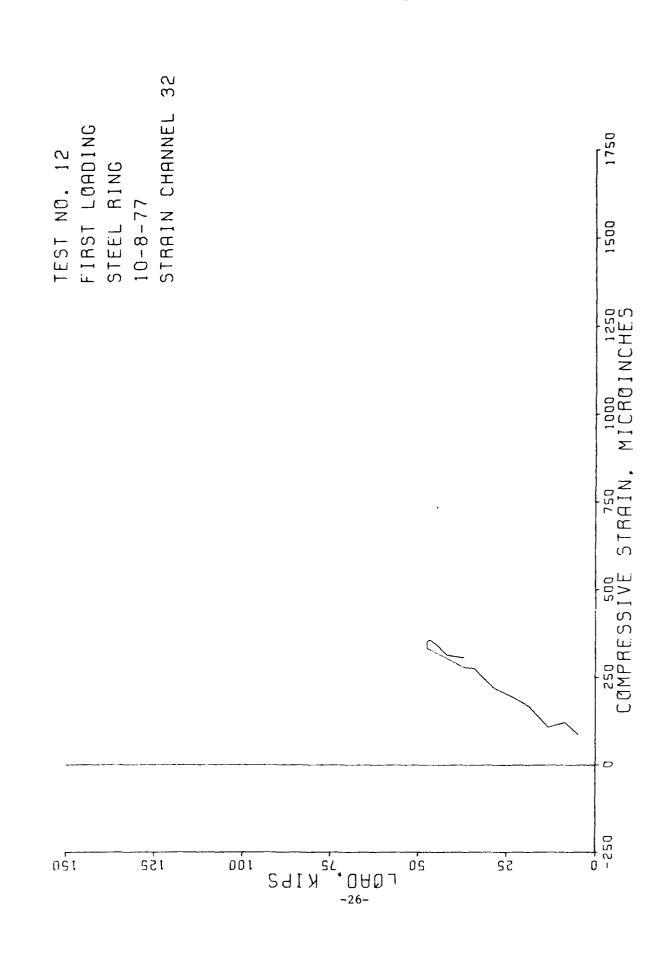


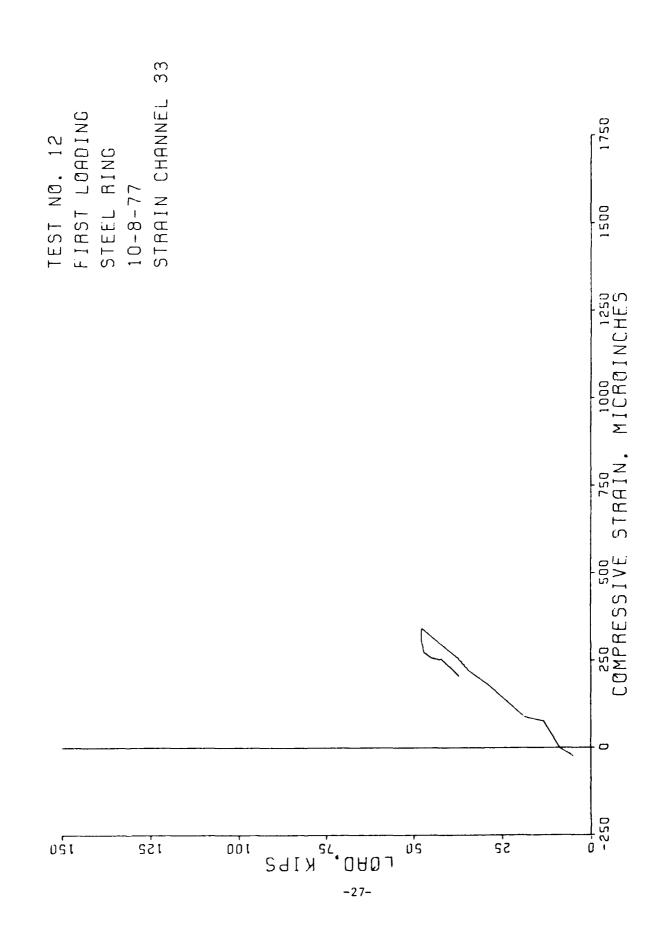
- CH 12-19 Load axis I.D. (Research, Inc. Model 4040).
- CH 22-29 Axial load (Transducers, Inc. Model 693-300K).
- CH 30-39 (Ailtech SG 129-6S) Radial pairs inside and out at center between axes.
- CH 40-43, 45-48 (Ailtech SG 129-6S) Polarity indicates rod under tension. Lower rod shown (XX).

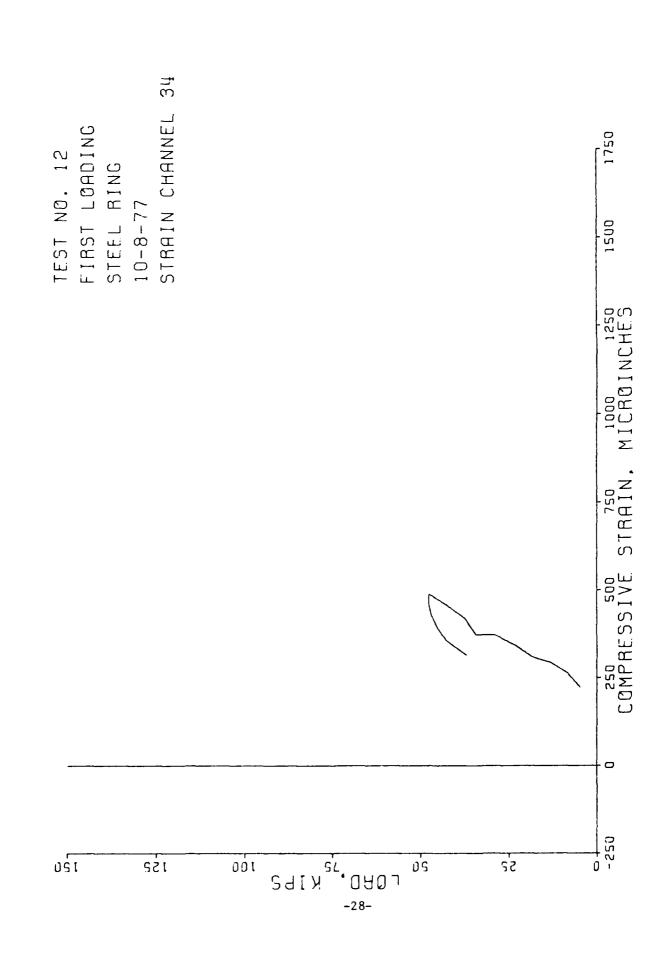


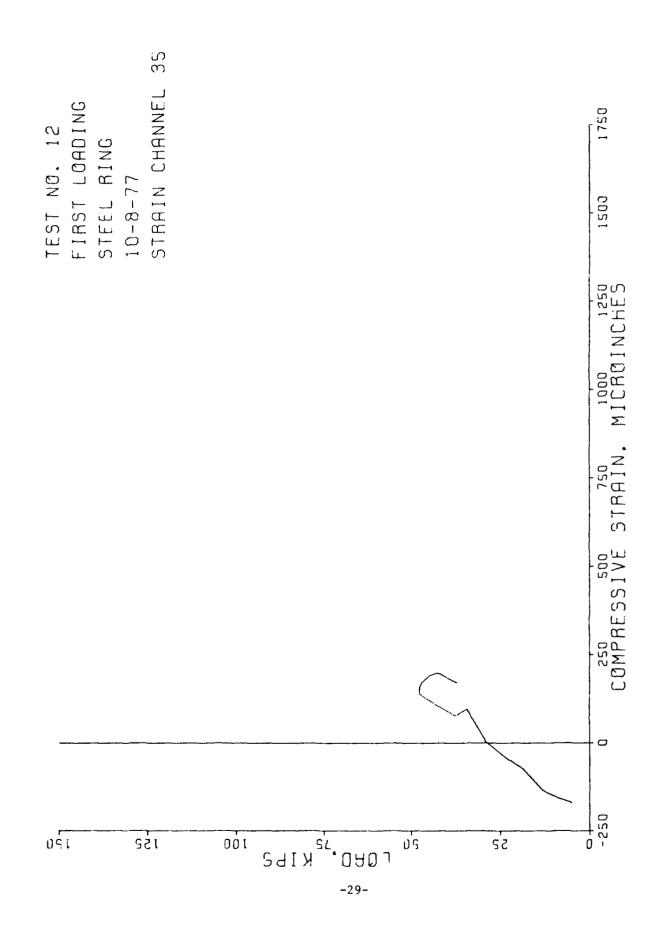


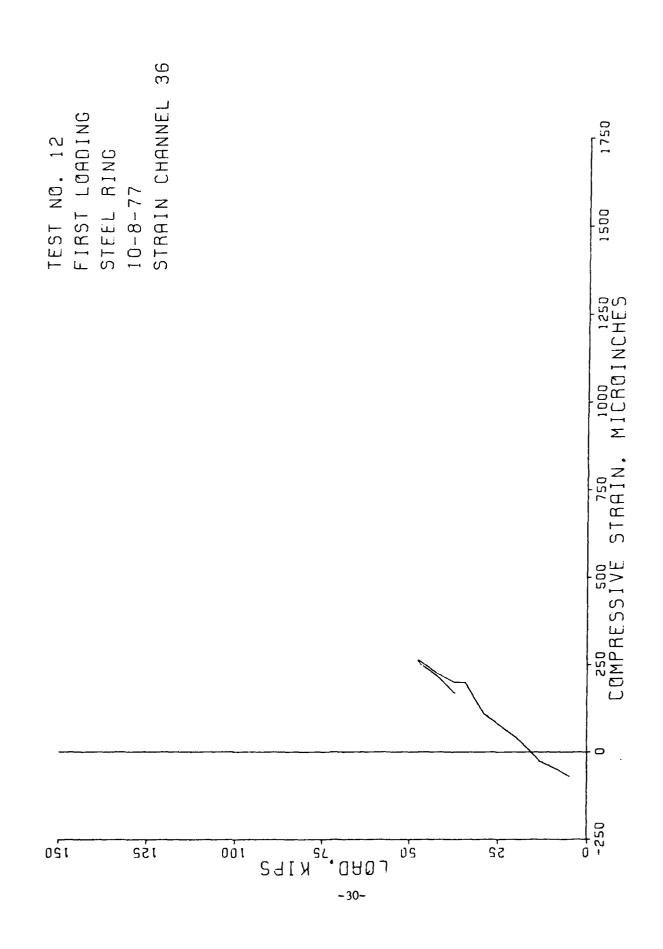


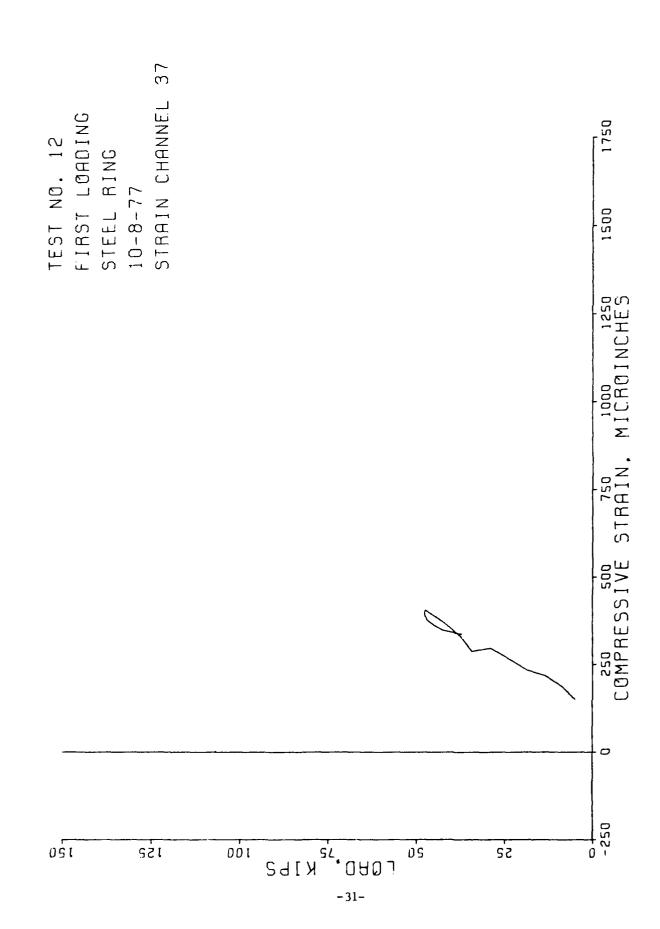


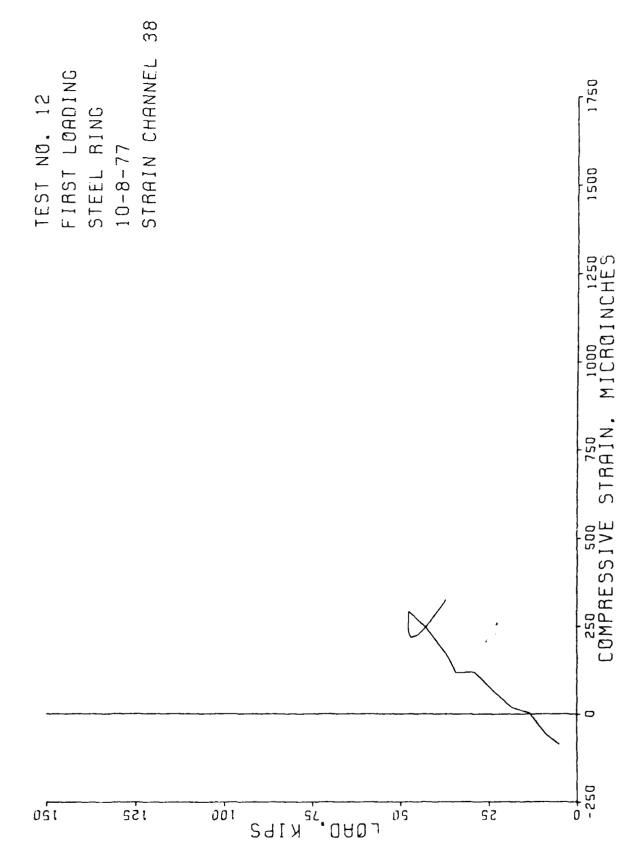


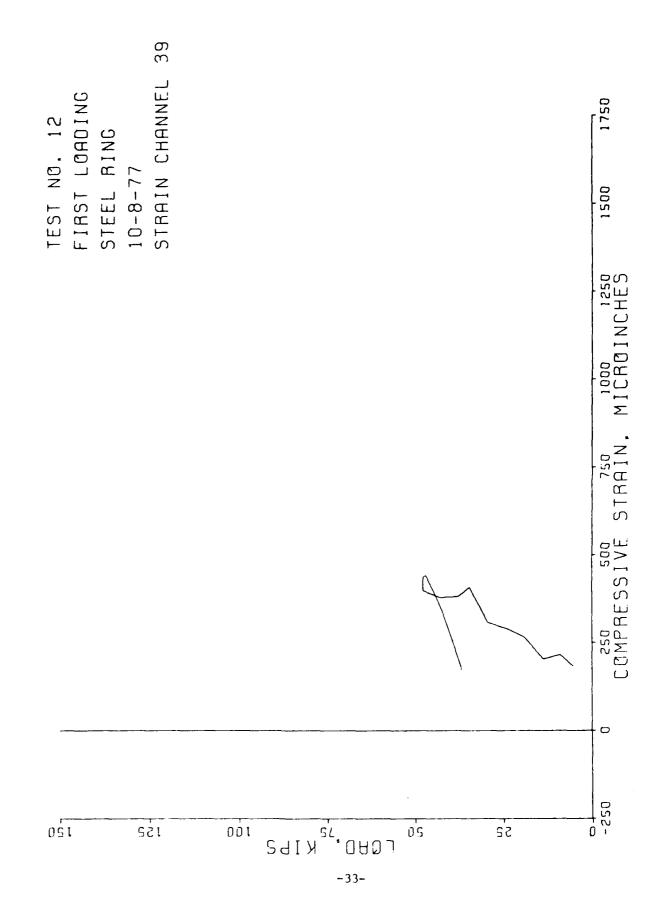












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F STRAIN CHANNELS= 10
F DISPLACEMENT CHANNELS=
F LOAD CHANNELS= 8
F RESSURE CHANNELS= 0
F RODS= 8
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1.000	CALIBRATION	0	CALIBRATION	10.000 10.000 10.000 10.000 10.000 10.000	CALIBRATION	1.000 1.000 1.000 1.000 1.000 1.000
331	DISPLACEMENT CHANNEL	13 17 18 15 13 12	LOAD CHANNEL	222222222 22225428	ROD CHANNEL	444444 011235678

E.

	CH.12	-0.075	-0.048	6 50 0 -	-0.045	-0.019	-0.021	-0.018	-0.018	-0.018	-0.018	-0.018	-0.018	-0.018	-0.017	-0.017	-0.017
	CH.13	-0.063	-0.032	-0.032	-0.032	-0.024	-0.024	-0.023	-0.001	-0.001	-0.001	-0.001	-0.001	-0.001	-0.001	-0.001	-0.001
	CH.14	-0.004	-0.006	-0.005	-0.005	-0.005	-0.005	-0.004	-0.003	-0.004	-0.005	-0.005	-0.005	-0.006	-0.005	-0.004	-0.003
	CH.15	0.075	0.055	0.053	0.052	0.050	0.050	0.050	0.054	0.051	0.051	0.051	0.052	0.052	0.052	0.054	0.054
	CH.16	0.108	0.109	0.105	0.080	0.080	0.079	0.080	0.079	0.079	0.079	0.080	0.079	0.079	0.079	0.078	0.079
	CH.17	0.059	0.060	0.058	0.059	0.059	0.059	0.058	0.059	0.059	0.059	0.060	0.059	0.059	0.059	0.759	0.060
N E L S	CH.18	20.810 10.060	20.750	19.030	21.950	25.280	-0.970	1.300	-1.650	-2.190	1.000	-0.990	1.390	25.270	-23.930	22.900	22.500
N T C H A N	CH.19	-0.540	-0.500	-0.540	-0.310	-0.260	-0.260	-0.260	-0.260	-0.260	-0.260	-0.260	-0.260	-0.250	-0.260	-0.250	-0.260
PLACEME	TIME	8:10:32:58 8:10:35:11	:10:3	. 10:4	10:4	:10:4	:10:4	:10:5	:10:5	:10:5	:10:5	:10:5	:10:5	:10:5	:10:5	:11:1	: 11 : 1
S I 0		1.	m d		9	٦.	∞.	6	10.	11.	12.	13.	14.	15.	16.	17.	18.

CH.22	8040 10760 10760 10750 19380 294160 294160 388120 477780 4
CH.23	\$300.000 11760.000 128360.000 22740.000 287240.000 287260.000 37780.000 46790.000 45200.000 45200.000 45200.000 45200.000 45200.000 45200.000 45200.000 45200.000
CH.24	4750 13390 13390 13350 13350 13520 14580 14580 14720 1
CH.25	5080.000 13520.000 13520.000 23460.000 23160.000 34370.000 47740.000 47750.000 47750.000 47250.000 47250.000 47250.000 47250.000
CH.26	5540.000 13540.000 13540.000 23500.000 286810.000 28650.000 472490.000 47250.000 471180.000 41180.000 41670.000
CH.27	6100 12870 12870 12870 12850 18560 18560 18580 18580 18580 18690 18600 18600 1
CH.28	5520.000 13660.000 13660.000 24720.000 36710.000 36710.000 48560.000 48350.000 47770.000 47770.000 49500.000 52770.000
CH.29	5940 111380 16230 25970 25970 31550 40290 40290 40290 40290 40290 40290 40290 40290 40290 40290 40290 40290 40290 40290 40290 40290 4020 402
TIME	88888888888888888888888888888888888888
	44444444444444444444444444444444444444

CH.40		
CH.41	-255.62 -251.262.42 -251.262.42 -1160.930 -1204.930 -1204.930 -1204.930 -1204.930 -1204.930	-230.612
CH.42	1 1 2 2 2 5 2 5 2 5 2 5 2 5 2 5 2 5 2 5	38.435
CH.43	11111111111111111111111111111111111111	
CH.45		-192.177
CH.46	12556 2256 2256 236 236 236 236 236 236 236 236 236 23	-345.918
CH.47	- 128 - 128	128.118
CH.48	8 3 2 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3	845.579
TIME	88:100:35:10 88:100:45:10 10:35:10 10:45:10 10:47:10	8:11:12:23
	LUMAROS SASSASSAS ACCESSES ACC	18.

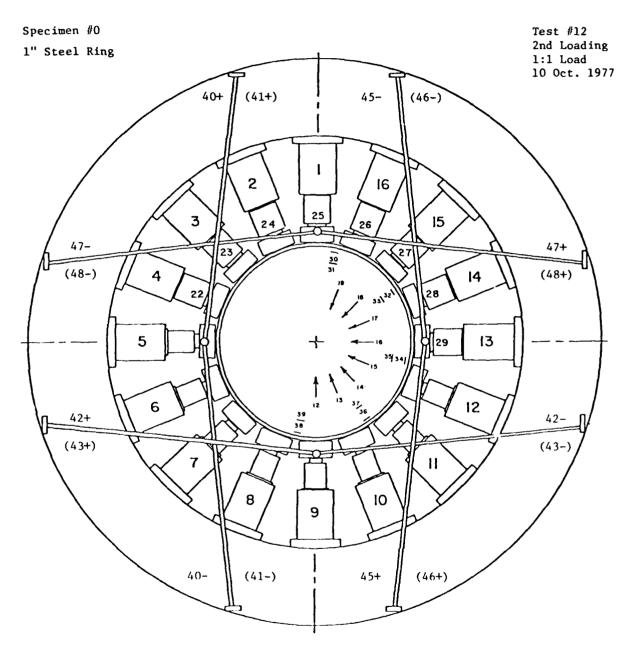
5718.7	19166.250	9162.50	8137.50	7713.75	7383.75	6210.00	3000.002	1098.75	0483.75	6292.50
	n d u			<b>,</b> 0	-		<b>ر</b> د د	S	9	7

17. 18. MAXIMUM LOAD CHANNEL, 25 REACHES A MAXIMUM VALUE AT STEP NUMBER 11

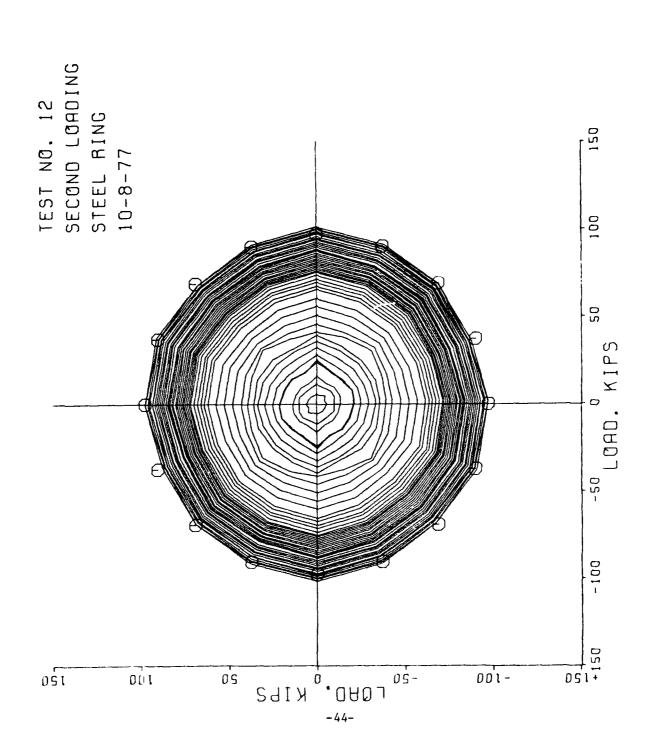
## 3.1.2 RELOAD OF SPECIMEN #0

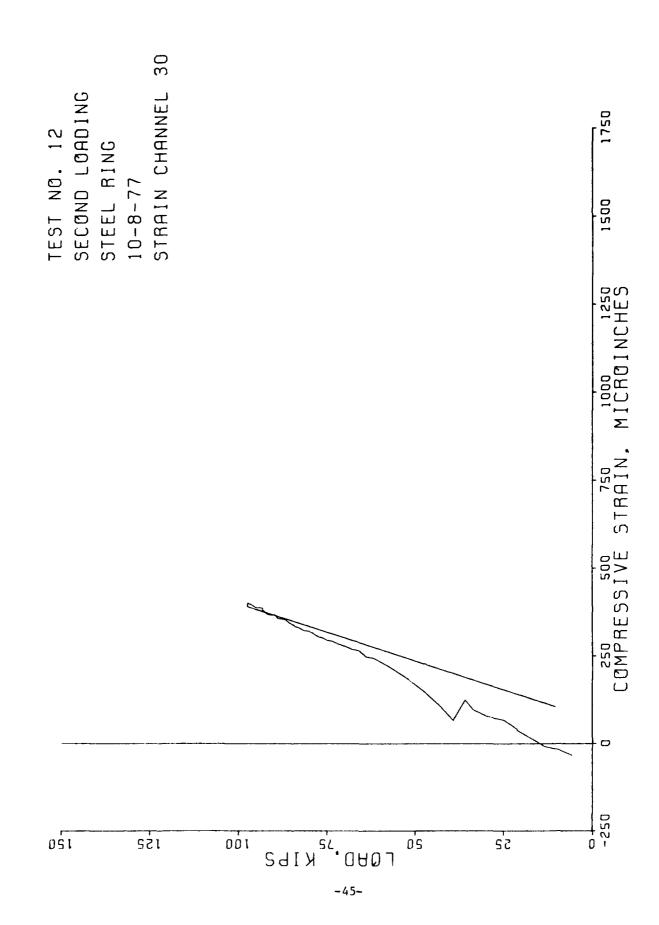
TEST NO. 12 (2ND)
STEEL LINER
1:1 LOADING RATIO
TESTED 10 OCTOBER 1977

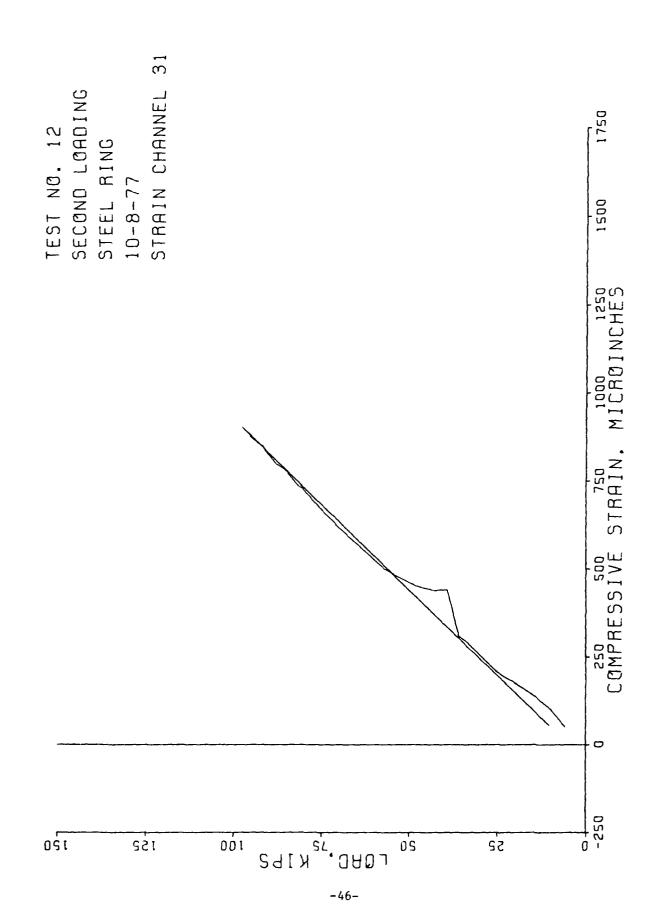
## REACTION FRAME TEST SET-UP

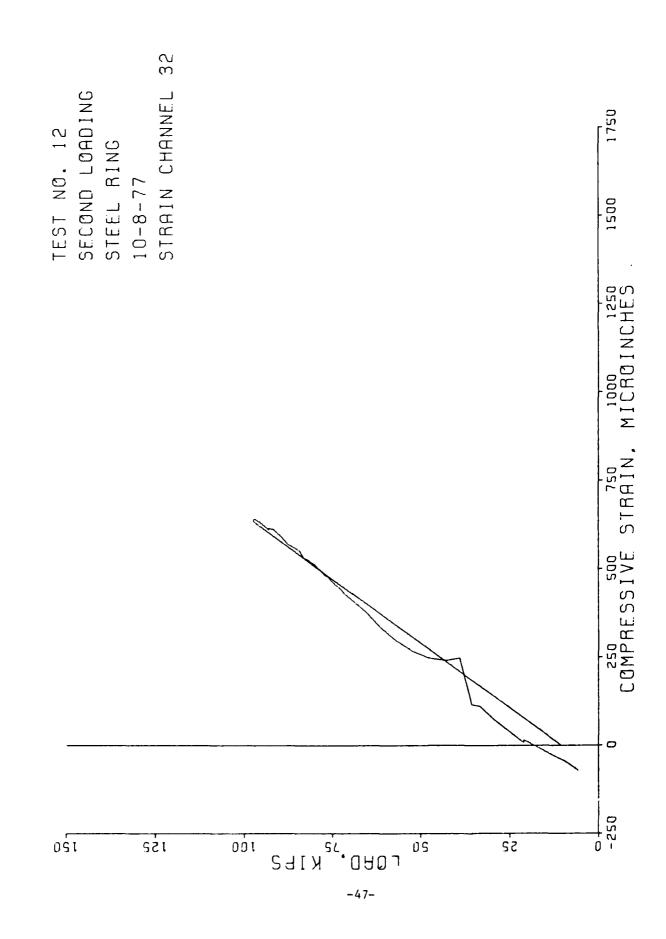


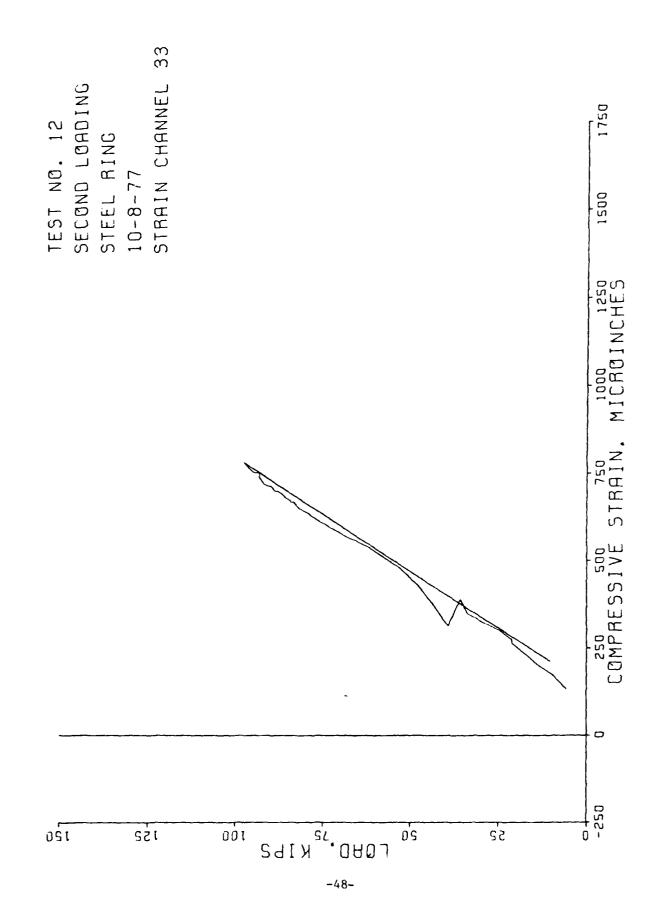
- CH 12-19 Load axis I.D. (Research, Inc. Model 4040).
- CH 22-29 Axial load (Transducers, Inc. Model 693-300K).
- CH 30-39 (Ailtech SG 129-6S) Radial pairs inside and out at center between axes.
- CH 40-43, 45-48 (Ailtech SG 129-6S) Polarity indicates rod under tension. Lower rod shown (XX).

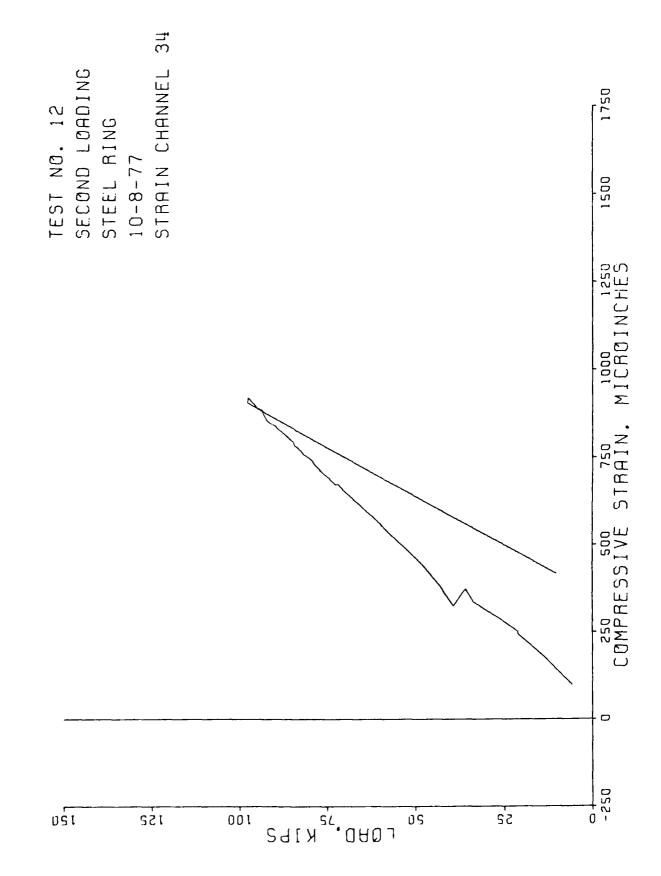


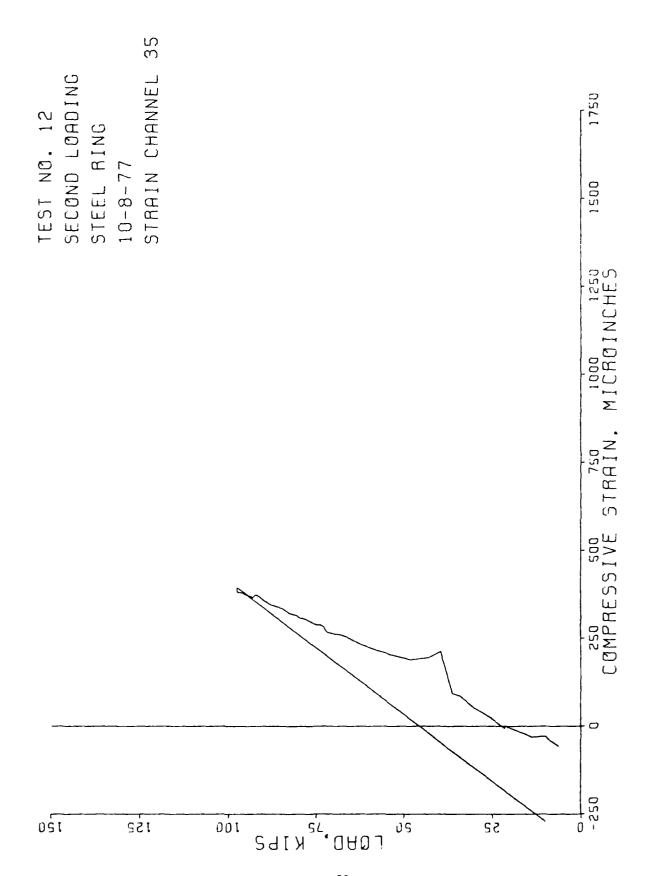


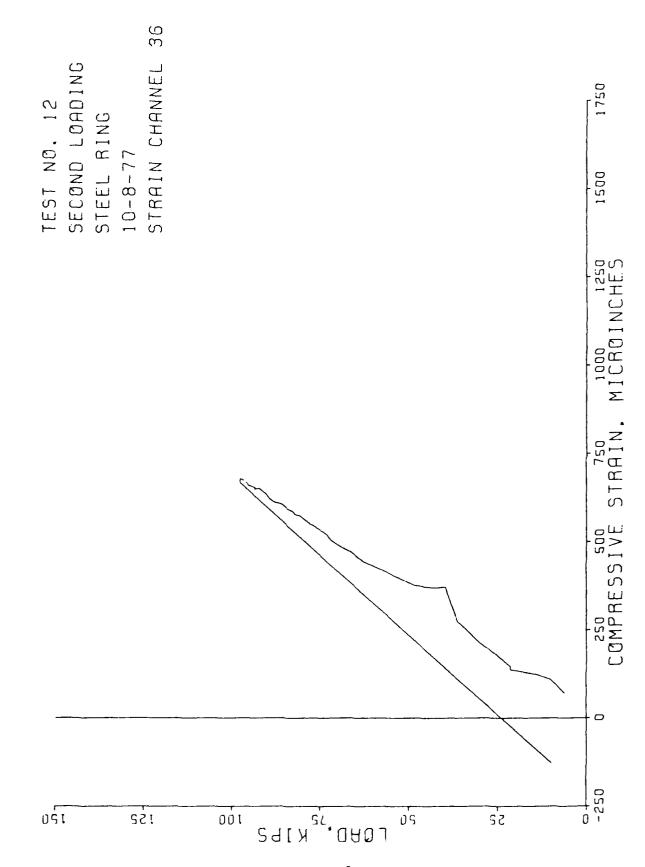


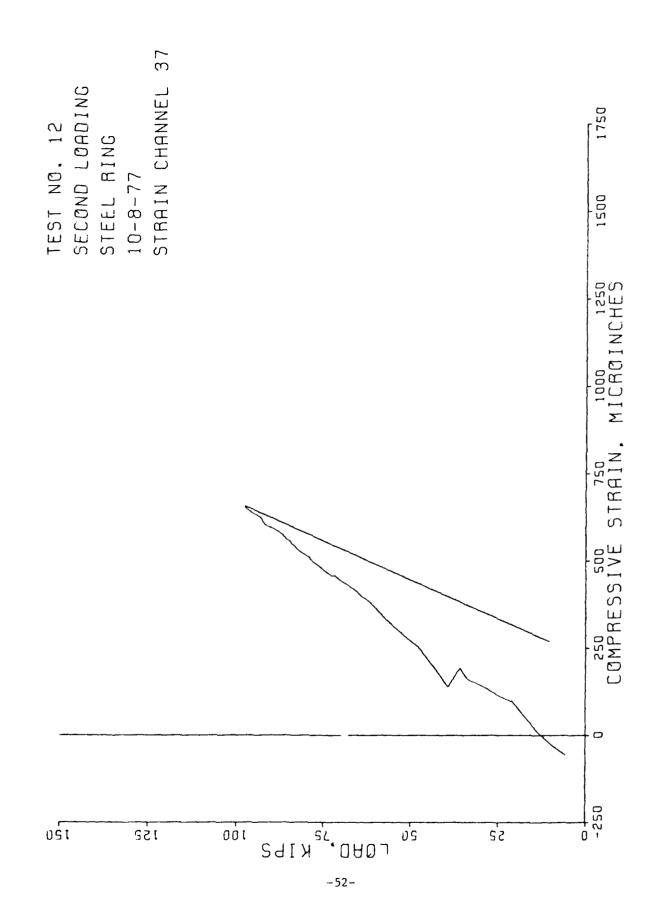


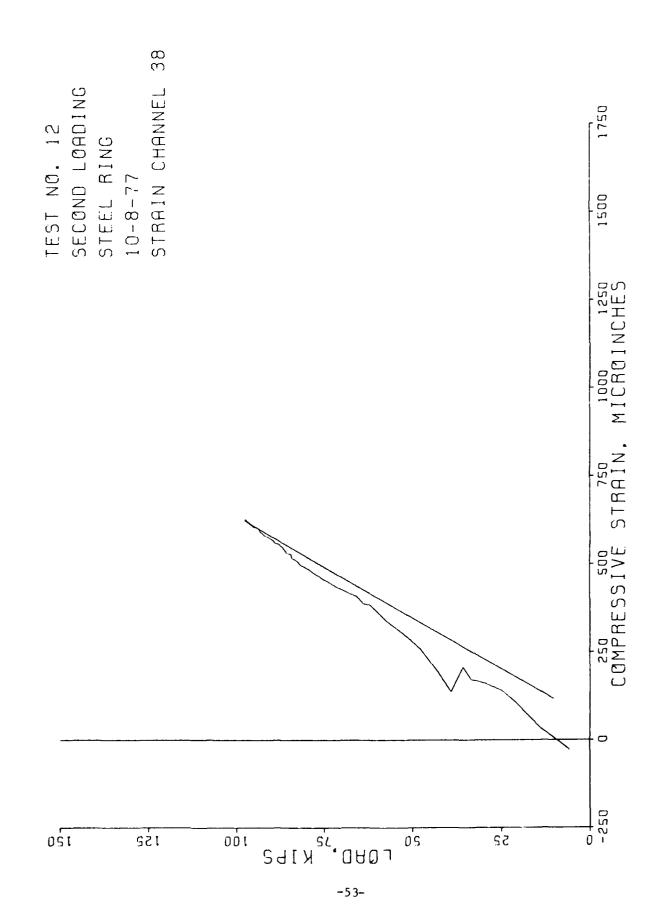


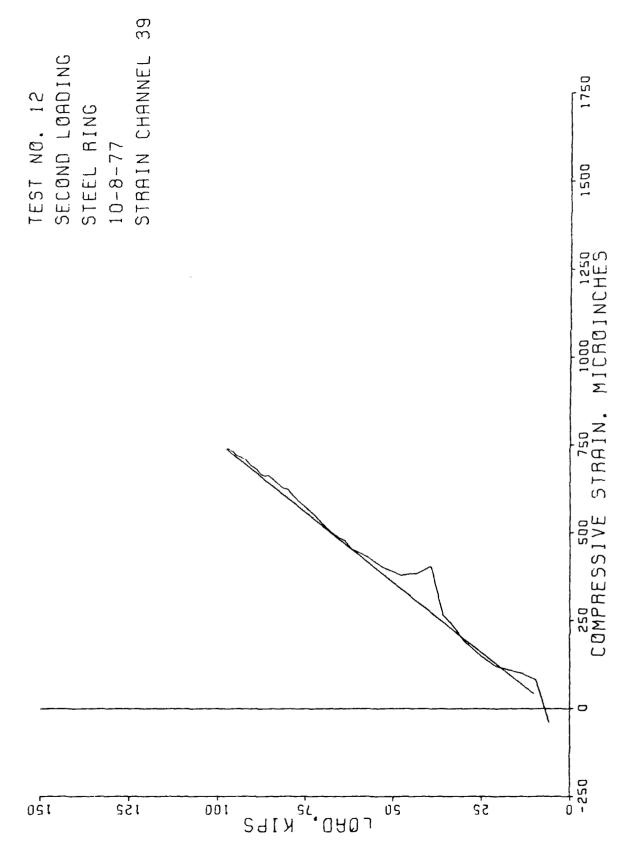












1.000	CALIBRATION	000000000000000000000000000000000000000	CALIBRATION	10.000 10.000 10.000 10.000 10.000 10.000	CALIBRATION	11111111111111111111111111111111111111
31	DISPLACEMENT CHANNEL	18 17 16 11 12	LOAD CHANNEL	22 22 23 23 23 24 25	ROD CHANNEL	44444 44444 0115335678

CH. 32	6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6	2.00
CH.33		211.00
CH.34	1 1 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	416.00
CH.35	33.000 1.3.2.2.2.2.2.2.2.2.2.3.3.3.3.3.3.3.3.3.	71.00
CH. 36	11109 11	28.00
CH.37		269.00
CH.38		15.00
CH.39	7.7.10000000000000000000000000000000000	42.00
TIME	11. 10:11:59:59  2. 10:12:13:14  4. 10:12:13:14  11. 10:12:13:15  11. 10:12:13:15  11. 10:12:13:15  12. 10:12:13:15  13. 10:12:13:15  13. 10:12:13:15  13. 10:12:13:15  13. 10:12:13:15  13. 10:12:13:15  13. 10:12:13:15  13. 10:12:13:15  13. 10:12:13:15  13. 10:12:13:15  13. 10:12:13:15  13. 10:12:13:15  13. 10:12:13:15  13. 10:12:13:15  14. 10:12:13:15  15. 10:12:13:15  16. 10:12:13:15  17. 10:12:13:15  18. 10:12:13:15  18. 10:12:13:15  18. 10:12:13:15  18. 10:12:13:15  18. 10:12:13:15  18. 10:12:13:15  19. 10:12:13:15  10:12:13:15  10:12:13:15  10:12:13:15  10:12:13:15  10:12:13:15  10:12:13:15	9. 10:12:42:3

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CH.33.00 116.00 33.00 33.00 41.00 68.00 79.00	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	391.00 105.00
CH.3 100.00 133.00 182.00 182.00 206.00	12.24 12.24 12.24 12.24 12.24 12.24 12.24 12.24 12.24 12.24 13	-55.00
TIME 10:11:59:5 10:12: 4: 10:12:11:2 10:12:11:3 10:12:11:3 10:12:12:4	7. 10 11 12 12 12 12 12 13 14 15 15 15 15 15 15 15 15 15 15 15 15 15	10:12:42:3

CH.12	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
CH.13	00000000000000000000000000000000000000
CH.14	
CH.15	
CH.16	
CH.17	 
CH.18	\$
CH.19	
TIME	1. 10:11:59:59 3. 10:12: 3.34 4. 10:12: 11:50 6. 10:12:11:50 7. 10:12:11:50 10:12:11:50 10:12:11:50 10:12:11:50 10:12:11:50 10:12:13:59 112. 10:12:13:59 113. 10:12:14:37 114. 10:12:14:37 115. 10:12:14:37 116. 10:12:14:37 117. 10:12:14:37 118. 10:12:14:4 119. 10:12:14:14 119. 10:12:14:14 119. 10:12:14:14 119. 10:14:14 119. 10:14:14 119. 10:14:14 119. 10:14:14 119. 10:14:14 119. 10:14:14 119. 10:14:14 119. 10:14:14 119. 10:14:14 119. 10:14:14 1

CH.22	5780.00 3200.00 0390.00 0390.00 0170.00 64330.00	55510.00 5550.00 3760.00 8560.00 8250.00 72850.00 72850.00	8880.00 8880.00 8880.00 4660.00 4450.00 8260.00 9450.00	80470.000 821610.000 823340.000 84270.000 84270.000 84270.000 84270.000 87180.000 91330.000 91330.000 914800.000 944800.000 944800.000 944800.000 944800.000
CH.23	7160.00 3681.00 3681.00 9420.00 9740.00 0220.00 4050.00	5520.00 5520.00 6050.00 3440.00 7310.00 22110.00	7860.00 9690.00 1480.00 2770.00 3760.00 5510.00 6690.00	79560.000 81700.000 82740.000 82740.000 83800.000 84650.000 84650.000 87160.000 87160.000 97560.000 97590.000 97560.000
CH.24	4870.00 3780.00 3780.00 1410.00 1510.00 1590.00 4550.00	77777777777777777777777777777777777777	6460.00 8430.00 0130.00 0810.00 15590.00 3210.00 4400.00 6290.00	77380.000 78580.000 78580.000 81060.000 81770.000 83710.000 84940.000 85550.000 85550.000 869170.000 91650.000 91650.000 91830.000 9410.000
CH.25	5950.00 3880.00 11190.00 11560.00 5180.00	5,720.00 6000.00 30710.00 7990.00 7460.00 2100.00	7980.00 0080.00 1930.00 2790.00 3700.00 5680.00	79390.000 80330.000 82470.000 83500.000 84190.000 85750.000 86880.000 889920.000 91970.000 91970.000 93350.000 91860.000
CH.26	5410.00 3260.00 00390.00 0380.00 0560.00	52740.00 6710.00 6710.00 74020.00 74030.00 78120.00 7620.00	1090.00 2780.00 3790.00 5460.00 5440.00 5300.00	816890.000 823880.000 823350.000 854370.000 854370.000 854370.000 854370.000 854370.000 87350.000 8750.000 97750.000 97750.000
CH.27	5350.00 2940.00 0240.00 0470.00 0520.00 3390.00	25910.00 3710.00 3710.00 57270.00 8580.00 85390.00 1250.00	7030.00 8930.00 0770.00 1870.00 2870.00 4740.00 5750.00	78710.000 80860.000 81850.000 837310.000 837340.000 85240.000 86140.000 86150.000 91550.000 92520.000 92520.000 92520.000 92520.000
CH.28	720.00 380.00 190.00 140.00	7460.00 7440.00 7310.00 7320.00 7380.00 850.00 630.00	8640.00 0770.00 22470.00 3540.00 4410.00 6120.00 6120.00 8030.00	80330.000 81270.000 82940.000 83870.000 85840.000 86850.000 86850.000 91070.000 91070.000 94580.000 94580.000 94580.000 94580.000
CH.29	5590.00 5590.00 5590.00 3390.00 55140.00 5510.00	99470.00 9480.00 57200.00 5870.00 5840.00 5130.00	1250.00 3400.00 5340.00 5980.00 6930.00 7910.00 8950.00	83040.000 84230.000 85220.000 87400.000 87950.000 89690.000 91850.000 91850.000 92940.000 95760.000 97360.000 97360.000 97360.000 97360.000
TIME	10:11:59:10:10:10:10:10:10:10:10:10:10:10:10:10:	100112	10:12:22:3:10:10:10:12:22:3:14:0:10:12:22:22:3:14:0:10:12:22:22:3:14:0:12:22:22:3:14:0:12:22:22:22:22:22:22:22:22:22:22:22:22:	9. 10:12:25:11 10:12:25:32 11:10:12:26:15 5. 10:12:27:25 6. 10:12:27:25 7. 10:12:28:11 7. 10:12:28:11 9. 10:12:29:40 11:10:12:29:40 11:10:12:29:40 11:10:12:29:40 12:10:12:29:40 13:10:12:29:40 14:10:12:29:40 15:10:12:29:40 16:12:29:40 17:10:12:29:40 18:10:12:31:35 19:10:12:31:35 10:12:33:33
			00000000000000000000000000000000000000	COMUMMUMUMAGAGAGGAGAAAAAAAAAAAAAAAAAAAAAA

CH.40	-768.70 -960.88 -960.88 -960.88 -973.69	11111111111111111111111111111111111111	2459.865 -2498.301 -2552.362 -2552.362 -2552.362 -2600.795 -2652.042 -2652.042 -2652.042 -2652.042 -2652.042 -2652.042 -2652.042 -2652.042 -2716.101 -2716.101 -2792.972 -2818.595 -2818.595	28882 2882 2882 28882 28882 28882 28882 28882 28882 28882 28882 28882 28882 28
CH.41	166.55 1166.55 1166.55 1128.11 115.30 1153.74	2004.98 2014.98 2014.98 2014.98 2016.20 3045.91 4435.10	1 6 6 0 9 5 5 4 6 4 6 4 6 4 6 4 6 8 6 8 6 8 6 8 6 8 6	6666 6666 6666 6666 6666 6666 6666 6666 6666
CH.42	W0.081450 V4.0400 408W404		12230 12230 12234 12244 12244 12244 12244 1224 1224	22252 22844 22844 22844 22869 22869 22869 22869 22869 280 280 280 280 280 280 280 280 280 280
CH.43	66.55 89.68 0.0 0.0 12.81 25.62 0.0	100 110 110 110 110 110 110 110 110 110	- 1399 - 1399 - 166 - 167 - 166 - 167 - 166 - 167 - 166 - 16	44.86.86.86.86.86.86.86.86.86.86.86.86.86.
CH.45	0.000000000000000000000000000000000000	126.01 338.43 346.68 359.68 115.30 117.80 117.80 117.80 117.80	345 347 347 347 347 347 347 347 347 347 347	2012 2012 2012 2012 2012 2012 2012 2012
CH.46	46000000000000000000000000000000000000	2000 2000	555 586.586.586.586.586.586.586.586.586.7966.7966.5966.5966.717.717.7661.77.7681.7661.7661.7661.7	2522 8820 94 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
CH.47	881. 556.256. 7440. 7440. 933. 744. 744.	200 200 200 200 200 200 200 200 200 200	5448 5478 5474 5474 5486	20.55
CH.48	09.63 32.76 32.77 27.77 27.77 27.77	227.17 227.17 207.17 20.27 20.27 20.27 20.27 20.27	768.708 794.520 794.520 794.3320 807.14331 819.91431 845.579 858.390 871.202	71.20 884.01 884.01 71.20 71.20 71.20 71.20 71.20
TIME	10:11:59:5 10:12:4:3:3 10:12:11:2 10:12:11:3 10:12:11:3	20.00.00.00.00.00.00.00.00.00.00.00.00.0	20. 10:12:21:38 22. 10:12:22:3 24. 10:12:22:49 25. 10:12:22:49 26. 10:12:23:31 26. 10:12:24:5 27. 10:12:24:5 29. 10:12:24:5 31. 10:12:25:33 32. 10:12:25:33 33. 10:12:25:33 34. 10:12:25:33	7. 10:12:28:2 8. 10:12:28:2 9. 10:12:29:4 10:12:29:4 10:12:39:4 10:12:30:2 10:12:30:2 10:12:31:2 10:12:31:2 10:12:31:3 10:12:31:3 10:12:31:3 10:12:31:3

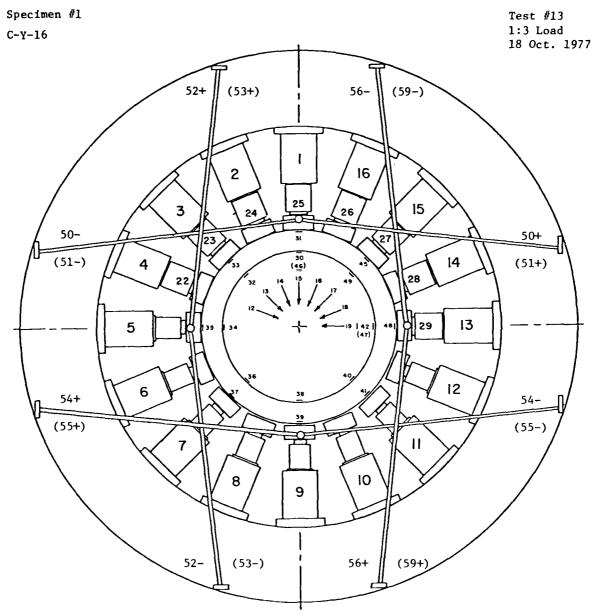
######################################	Š
10 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	278
44444444444444444444444444444444444444	

MAXIMUM LOAD CHANNEL, 25 REACHES A MAXIMUM VALUE AT STEP NUMBER 48

3.2 C-Y-16 MODELS 3.2.1 SPECIMEN #1

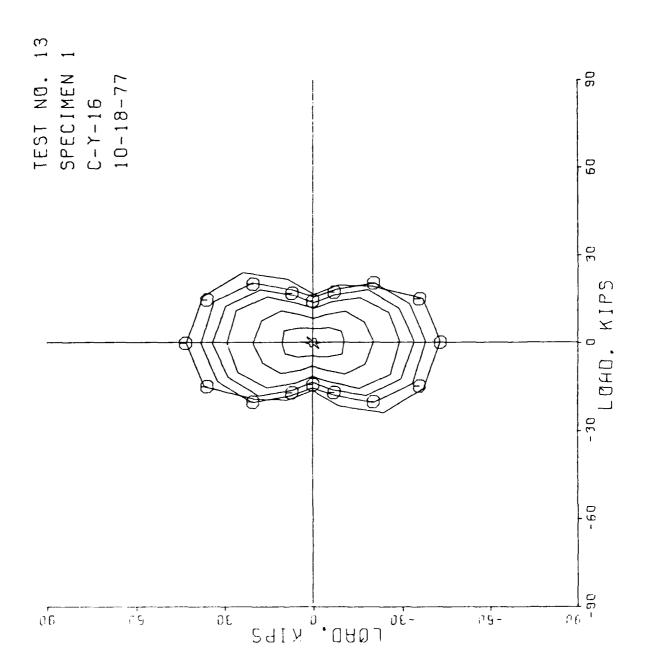
TEST NO. 13
COMPOSITE INTEGRAL LINER
1:3 LOADING RATIO
TESTED 18 OCTOBER 1977

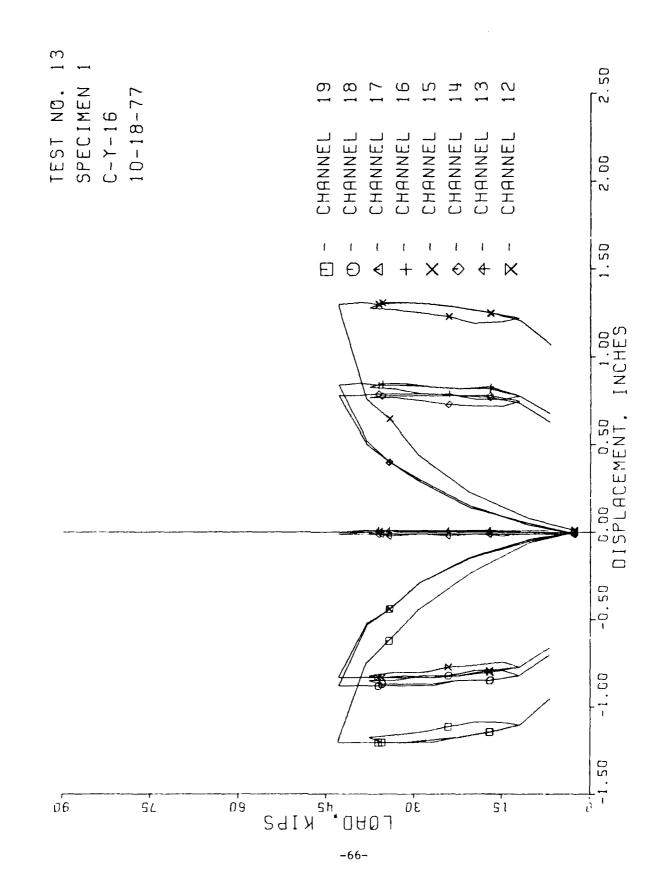
## REACTION FRAME TEST SET-UP

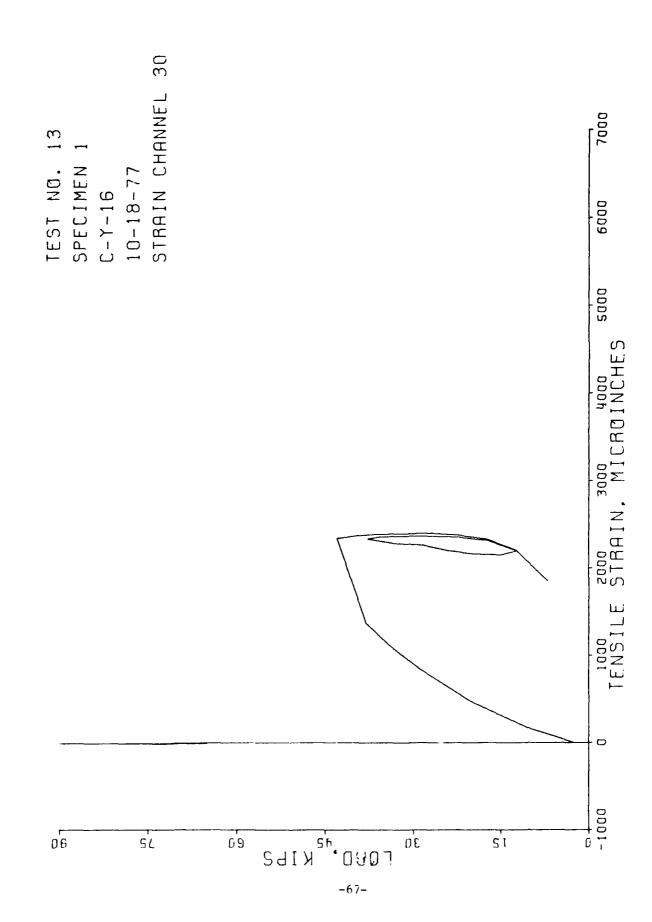


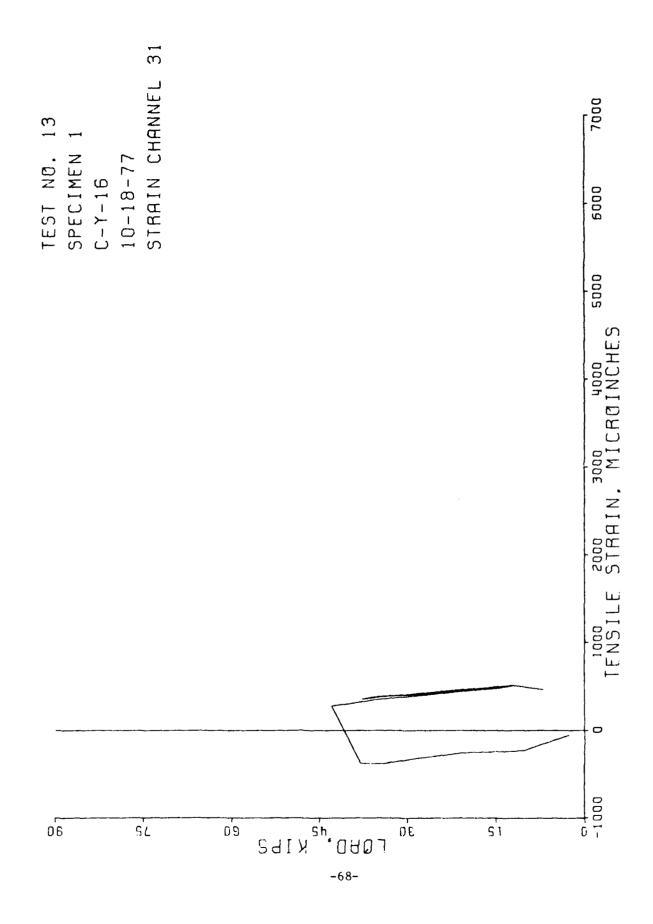
- CH 12-19 Load axis I.D. (Research, Inc. Model 4040).
- CH 22-29 Axial load (Transducers, Inc. Model 693-300K).
- CH 30-42, 45-49 (Ailtech SG 129-6S) Radial pairs 2" from top, except 46-47 2" from bottom. Odd gages 31-45 and 48 on rebar.
- CH 50-56, and 59 (Ailtech SG 129-6S) Polarity indicates rod under tension.

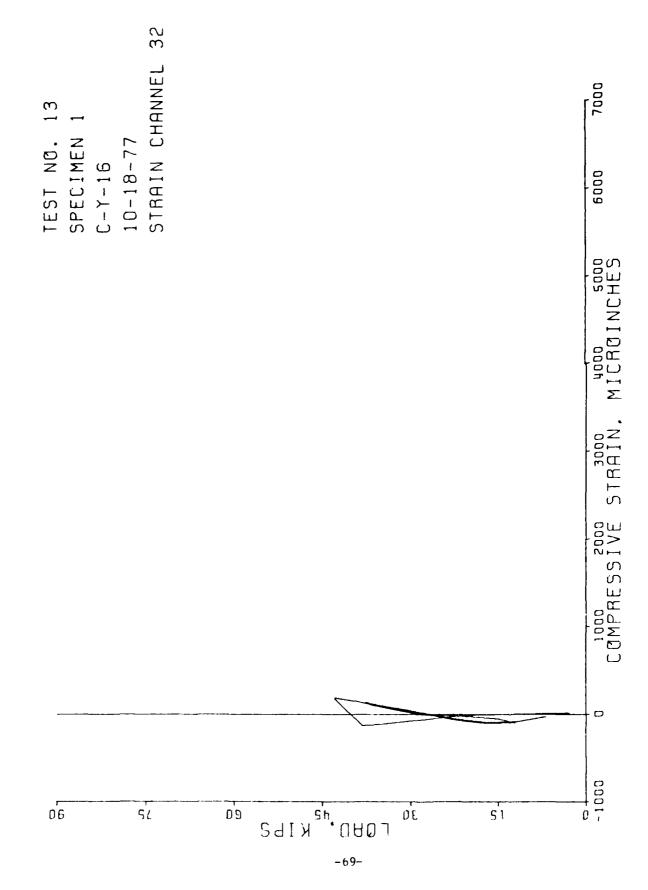
  Lower rod shown (XX).

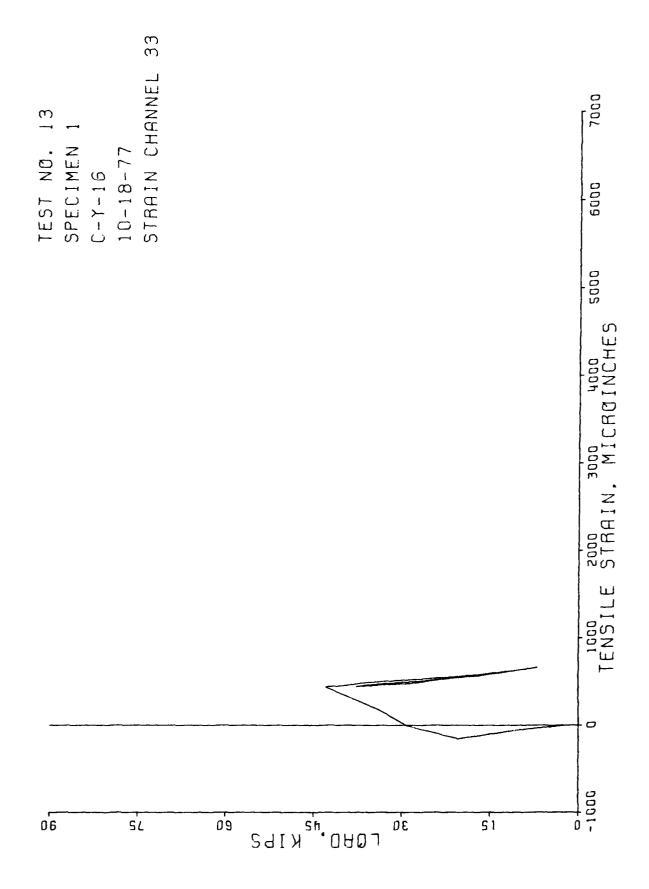


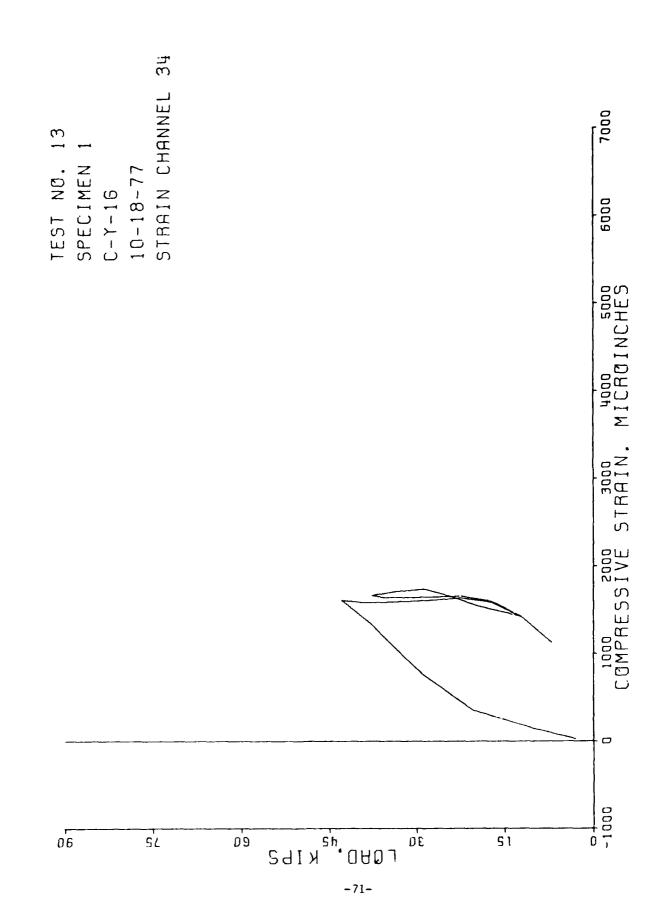


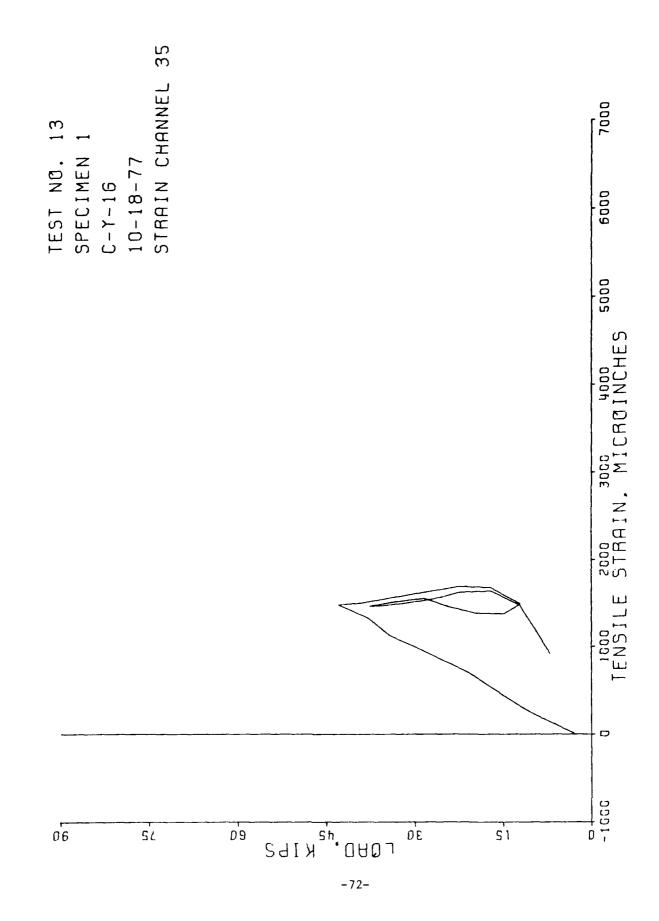


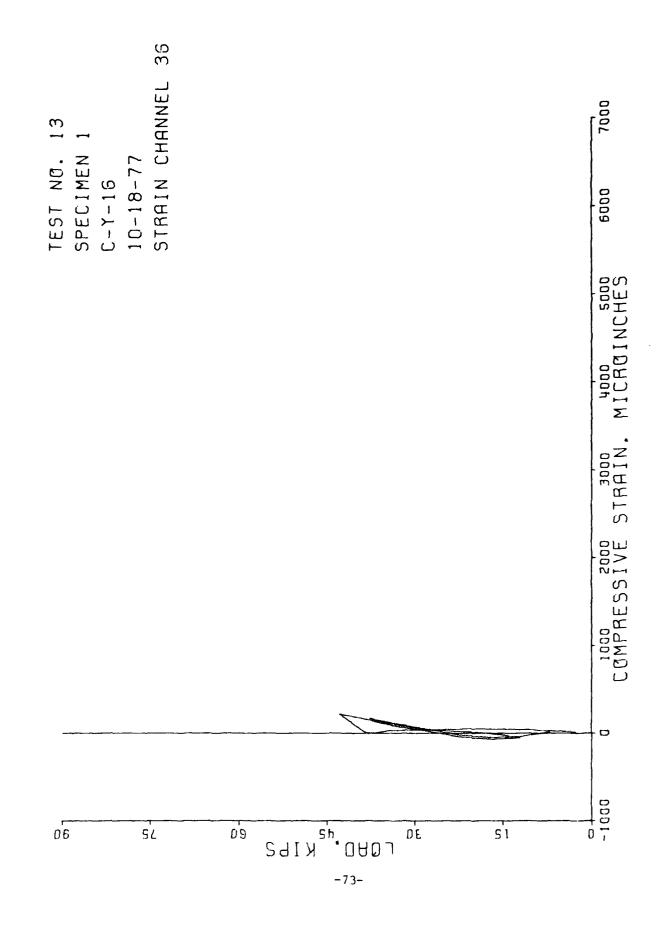


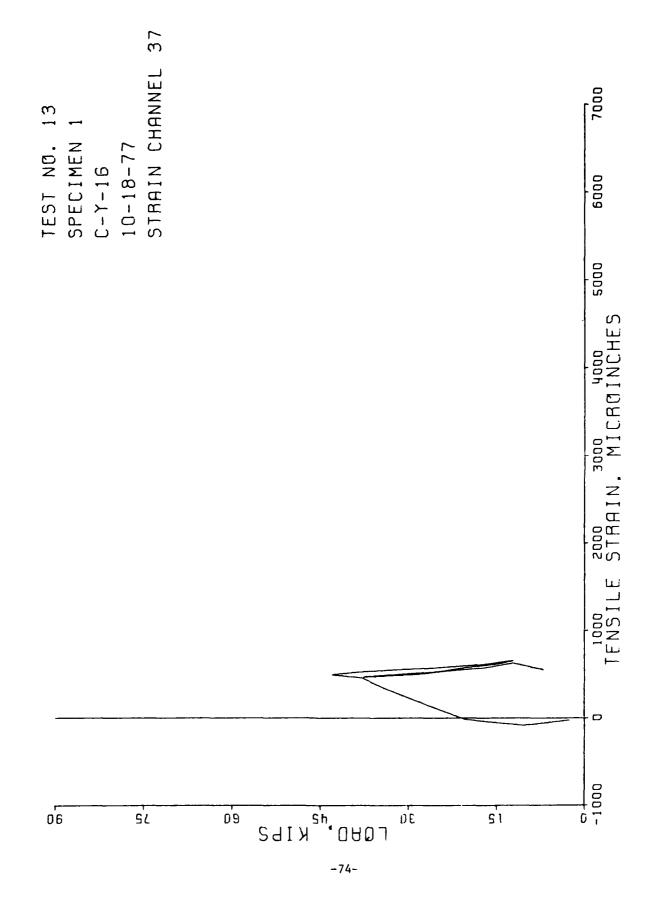


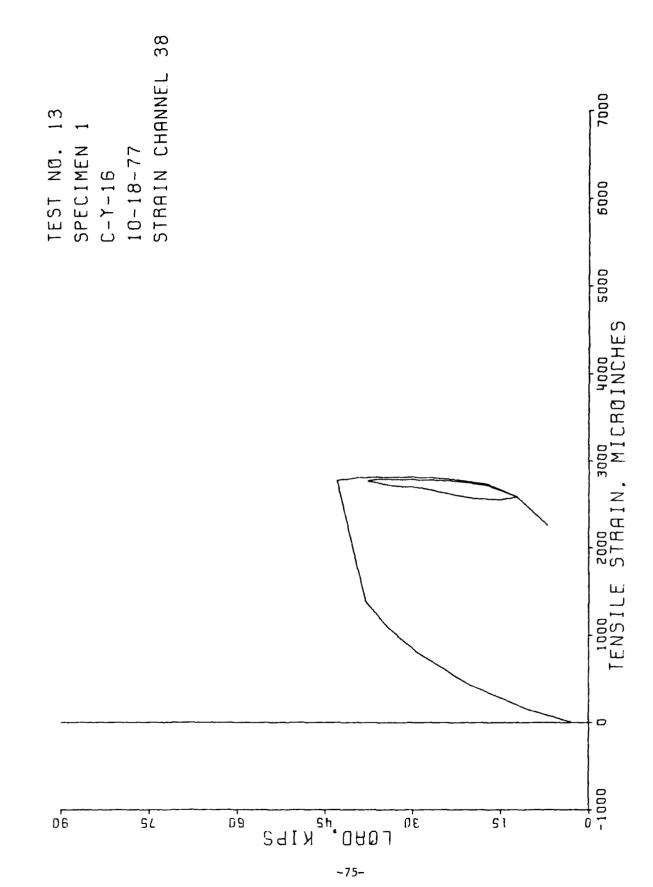


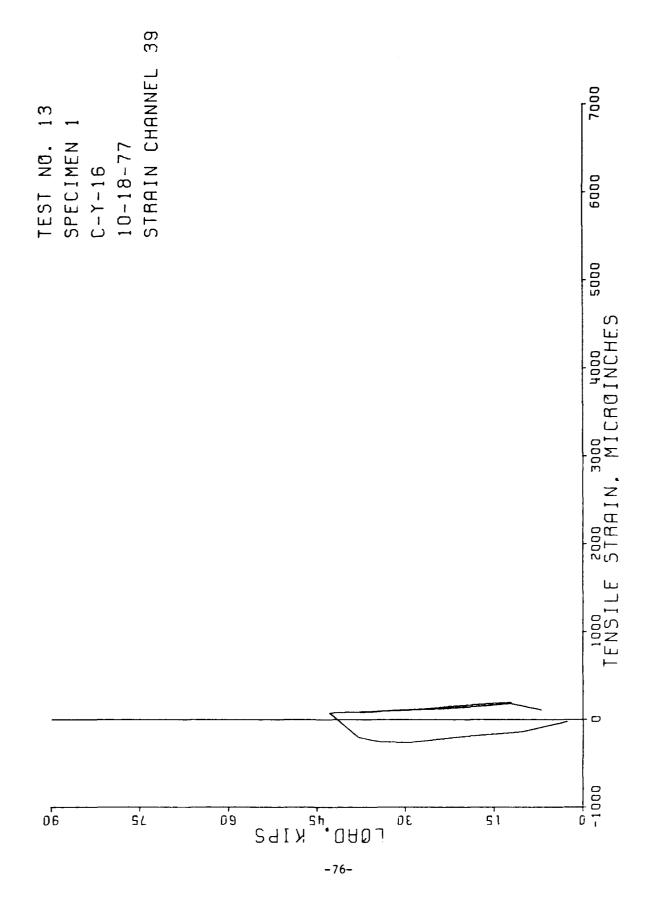


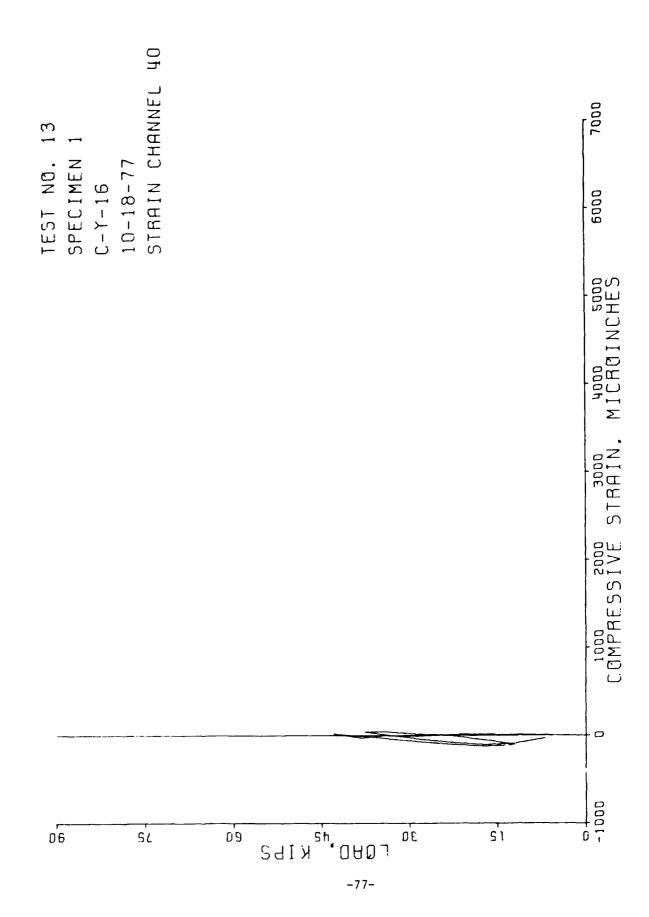


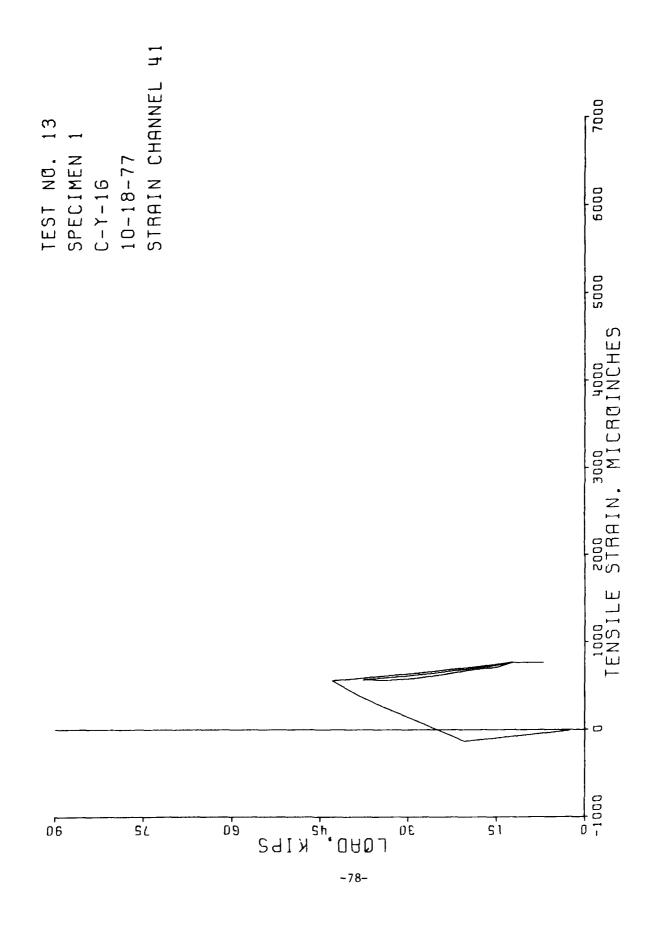


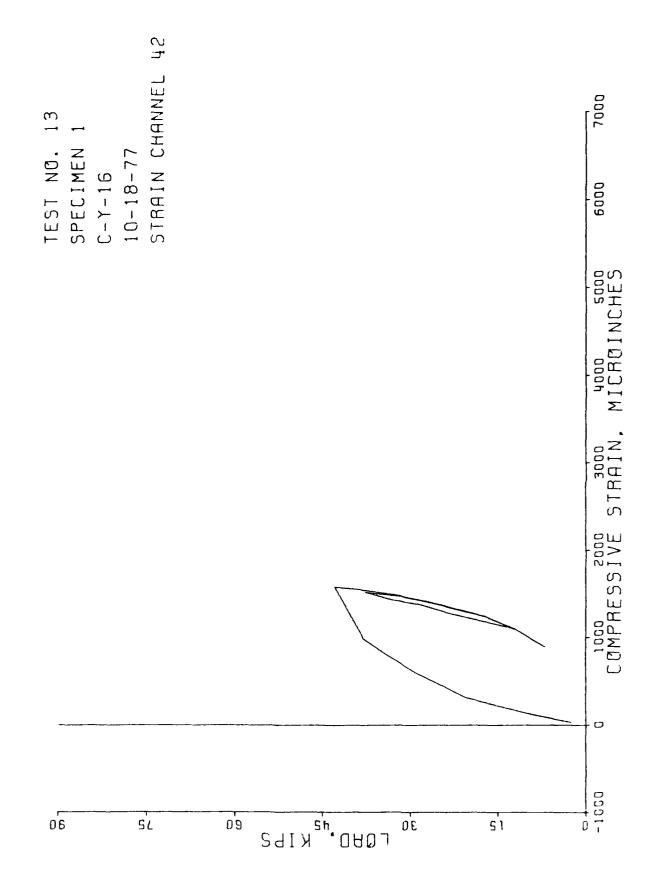


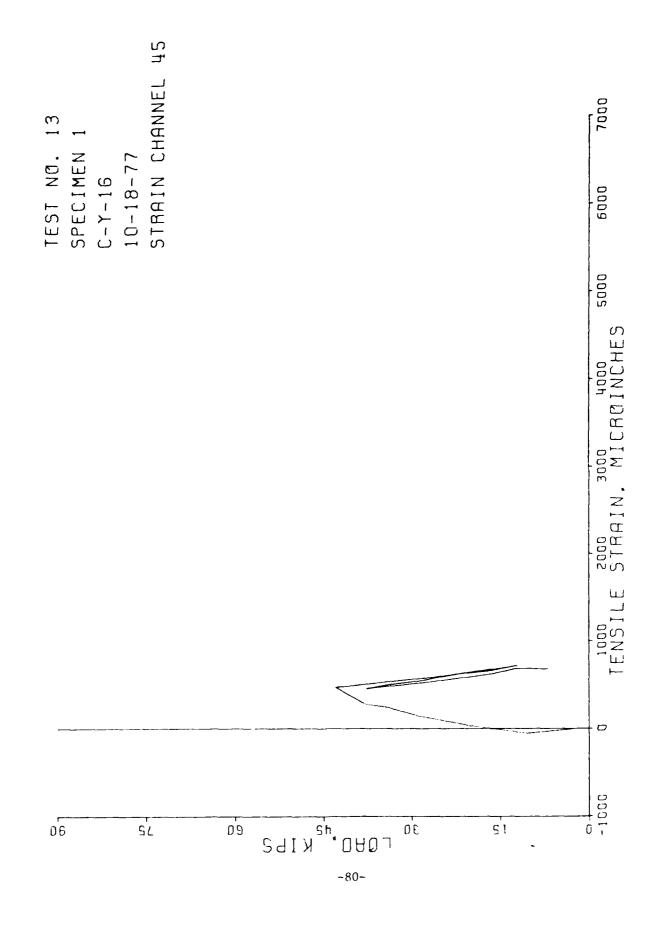


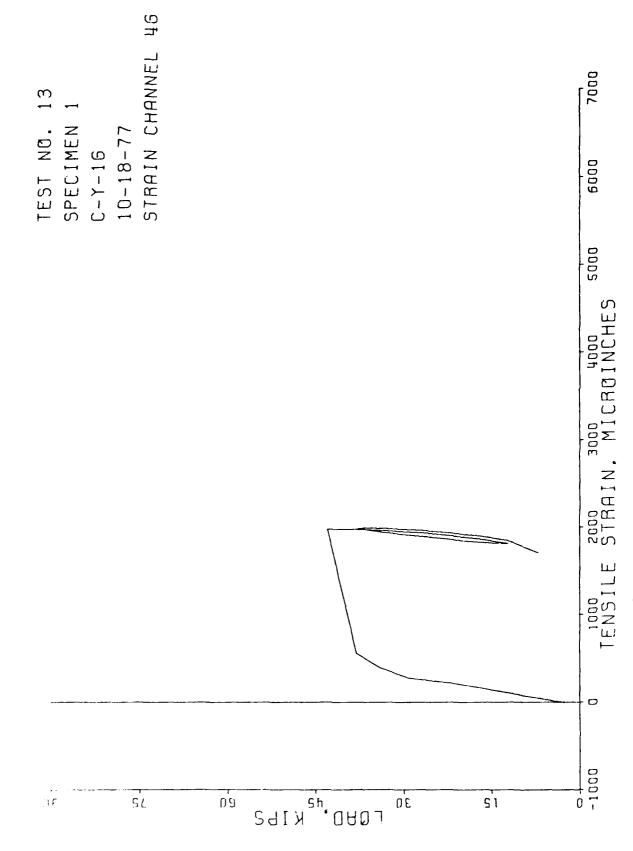


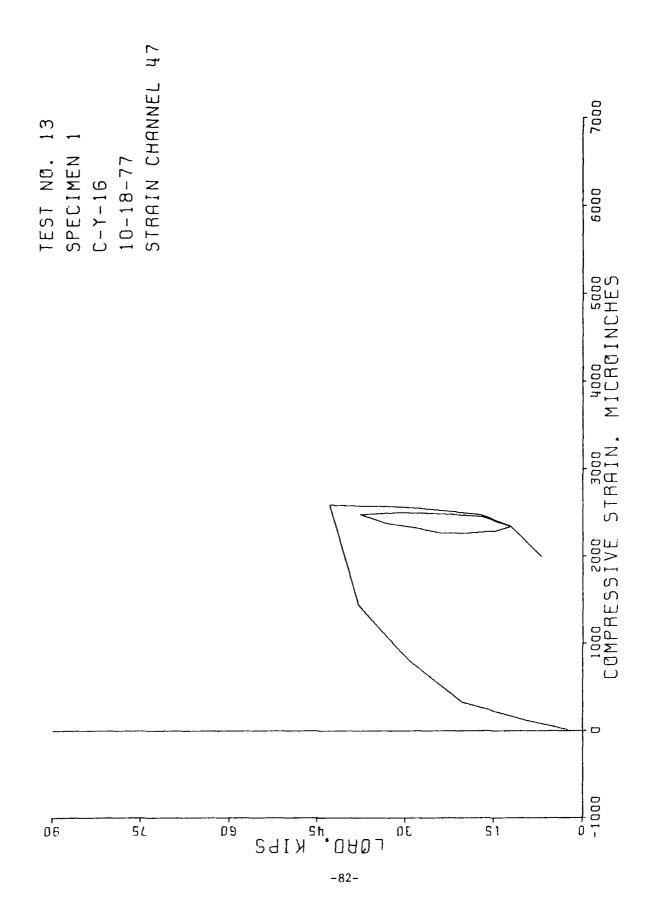


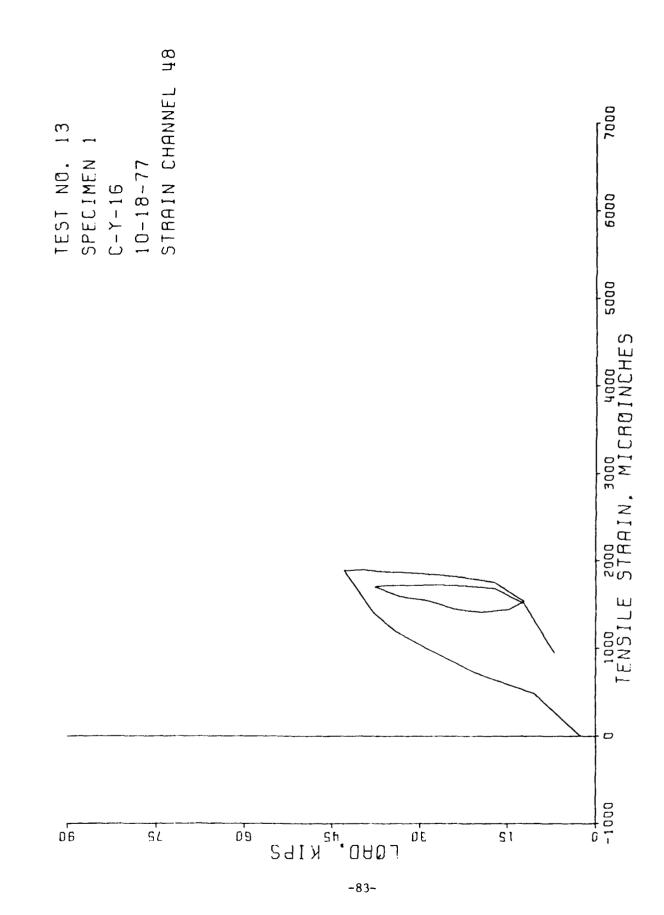


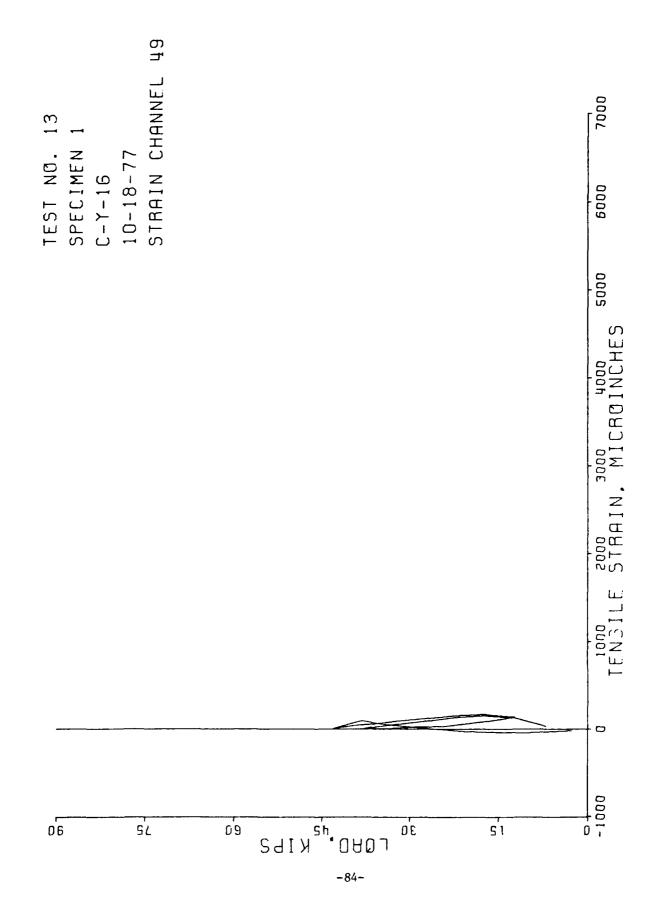












10-18-77			
C-Y-16	8 G	ZEROSHIFT	
T NO. 13 SPECIMEN 1 BER OF INCREMENTS= 27 BER OF CHANNELS= 42	NUMBER OF STRAIN CHANNELS= 18 NUMBER OF DISPLACEMENT CHANNEL NUMBER OF LOSSURE CHANNELS= NUMBER OF PRESSURE CHANNELS= NUMBER OF RODS=	CHANNEL	10 11 11 11 11 12 13 14 14 16 16 16 16 16 16 16 16 16 16 16 16 16

CALIBRATION

STRAIN CHANNEL

	CALIBRATION	00.000000000000000000000000000000000000	CALIBRATION	100000000000000000000000000000000000000	CALIBRATION	111111111111111111111111111111111111111
$\phi$	DISPLACEMENT CHANNEL	119 118 118 113	LOAD CHANNEL	22 22 23 23 23	ROD CHANNEL	ማ ማ ማ ማ ማ ማ ማ ማ ማ ማ ማ ማ ማ ማ ማ ማ ማ ማ ማ

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CH. 32 -14. 000 105. 000 106. 000 1189. 000 -1189. 000 -1189	54.000 89.000 83.000 25.000
1 1 104448000000044444444444444444444444	
CH 2000 CH 200	
CH. 35 238.000 238.000 1123.000 1337.000 1478.000 1538.000 1638.000 1681.000 1681.000 1681.000 1681.000 1681.000 1681.000 1681.000	0000
CH 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	0000
C. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1.	541.000 570.000 624.000 552.000
CH.38 150.000 10082.0000 10083.0000 1392.0000 22812.0000 22812.000 22812.000 22812.000 22812.000 22812.000 22812.000 22812.000 22812.000 22812.000 22812.000 22812.000 22812.000 22812.000 22812.000 22812.000	2764.000 2717.000 2592.000 2263.000
CH. 39 11225.0000 12259.0000 12259.0000 1225.0000 1225.0000 1225.0000 1225.0000 1225.0000 1225.0000 1225.0000 1225.0000 1225.0000 1225.0000 1225.0000 1225.0000 1225.0000	8.00.00 8.00.00
TIME  2. 18:13:50 4. 18:13:50 5. 18:14:16:155 6. 18:14:16:155 10. 18:18:18:18:18 10. 18:18:18:18 11. 18:18:18:18 11. 18:18:18:18 11. 18:18:18:18 11. 18:18:18 11. 18:18:18 11. 18:18:18 11. 18:18:18 11. 18:18:18 11. 18:18:18 12. 18:18:18:18 13:18:18:18:18 14:18:18:18:18 15:18:18:18:18 15:18:18:18:18 15:18:18:18:18 15:18:18:18:18 15:18:18:18 15:18:18:18 15:18:18:18 15:18:18:18 15:18:18 15:18:18:18 15:18:18 15:18:18 15:18:18 15:18:18 15:18:18 15:18 15:18:18 15:1	4. 18:15:15 5. 18:15:15 6. 18:15:17 7. 18:15:18

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CH.12 0.0.050 -0.150 -0.290 -0.520	00.00000000000000000000000000000000000
CH.13 -0.010 0.01 0.010 0.010 0.010	00000000000000000000000000000000000000
CH.14 0.0510 0.150 0.290 0.750	00000000000000000000000000000000000000
CH.15 0.010 0.030 0.230 0.440 0.450	11111111111111111111111111111111111111
- C C H C C C C C C C C C C C C C C C C	00000000000000000000000000000000000000
CH.17	
CH . 1 8	00000000000000000000000000000000000000
H	0.000000000000000000000000000000000000
TIME 188:114:114:150:130:130:130:130:130:130:130:130:130:13	

	CH.2		_•				9700.		8820.	6320.	4550.	1680.	9250.			0	. •	2300.	4800.	7280.	9440.	6870.	<u>-</u>	2010.0	_•	_•	_•	
	CH.23	1480.000	00.0	. 00	00.0	00.0	00.0	00.0	00.0	00.0	.00	00.0	00.0	00.0	00.0	00.	00.0	00.0	00.0	00.0	00.0	.00	00.0	00.0	00.0	9.6	00.0	00.0
,	CH.24	1110.000	0.00	0.00	0.00	0.00	0.00	0.00	00.0	0.00	0.00	00.0	0.00	00.0	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	00.0	00.0	0.00	0.00	0.00	0.00
1	CH.25	2640.000	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00
	CH.26	880.	0650.00	9180.00	8350.00	2330.00	6480.00	0590.00	7520.00	2430.00	8330.00	4320.00	9140.00	5540.00	1410.00	5440.00	7960.00	3040.00	7140.00	0660.00	5700.00	1330.00	00.0	4170.00	8770.00	5110.0	0.0860	0.0
	CH.27	2890.000	00.0	00.0	00.0	00.0	00.0	3.00	00.0	00.0	00.0	00.0	00.0	00.0	00.0	00.0	00.0	00.0	00.0	00.0	3.00	00.0	00.0	00.0	00.0	00.0	00.0	00.0
	CH. 28	490.000	0	0	0	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	0	00	00	00	00	00
	CH. 29	1360.000	640.00	00.060	1590.00	3490.00	5380.00	420.00	4760.00	2100.00	850.00	510.00	740.00	790.00	110.00	340.00	370.00	730.00	1220.00	170.00	4900.00	3060.00	0570.00	760.00	740.00	770.00	180.00	860.00
	TIME	. 18:13:50:	. 18:14:14:5	. 18:14:16:3	. 18:14:20:1	18:14:33:	. 18:14:34:3	18:14:59:1	. 18:14.59:5	. 18:15: 0:4	0. 18:15: 1:2	1, 18:15: 2:1	2. 18:15: 3:2	3. 18:15: 4:5	4. 18:15: 6:1	5. 18:15: 8:4	6, 18:15: 9:2	7, 18:15:10:	8, 18:15:10:3	9. 18:15:11:1	0, 18:15:11:5	1, 18:15:12:5	5:13:4	3, 18:15:14:1	4. 18:15:15:	5. 18:15:15:5	6. 18:15:17:	7. 18:15:18:1

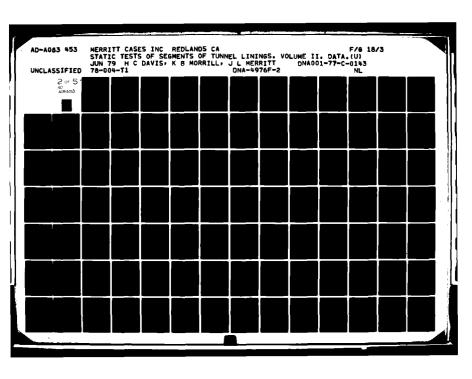
CH.50	-12.812	0.0	ニ	12.812	12.812	25.624	-384.354	-448.413	-499.660	-525.284	-550.907	-550.907	-550.907	-576.531	-525.284	-461.225	-307.483	-217.801	-230.612	-409.978	-486.848	-512.472	-525.284	-550.907	-550.907	-576.531	-435.601
CH.51	64.059	217.801	89.683	64.059	51.247	51.247	-409.978	-499.660	-550.907	-589.343	-614.966	-640.590	-614.966	-589.343	-512.472	-448.413	-243.424	-128.118	-204.989	-474.036	-576.531	-614.966	-627.778	-666.213	-653.402	-627.778	-448.413
CH.52	12.812	蟴.	_	ניח	7	0	•	_	n	u)	N	Γ.	Ψ	۳,	v	_	9	w	9	4	4	^	∞,	_	^	409.978	N
CH.53	38.435	0.0	-89.683	-448.413	-204.649	-884.014	-1652.722	-1524.604	-1306.803	-1127.438	-909.637	-717.461	-576.531	-461.225	-550.907	-730.272	-884.014	-1012.132	-1127.438	-1255.556	-1165.874	-986.508	-819.955	-627.778	-512.472	-409.978	-281.859
CH.54	12.812	5.62	2.81	2.81	2.81	0.0	07.	71.	22.	61.	12.	525.284	38.	50.	12.	35.	56.	53.	79.	45.	35.	61.	99.	50.	50.	κ.	61.
CH.55	51.247	-51.247	12.812	12.812	12.812	12.812	12.812	25.624	12.812	12.812	12.812	38.435	1	153.742		12.812	12.812	12.812	12.812	25.624	12.812	12.812	12.812	25.624	76.871	u 1	243.424
CH.56	25.624	_	v	m	M	m	N	∝	C	_	0	5	5	02	v	99	7	v	7	9	_	•	m	ょ	J	σ	'n
CH.59		٥.	256.23	243.42	69.04	422.78	79.36	02.49	66.55	79.35	04.98		66.55	64.05	89.68	51.24	53.74	230.61	243.42	92.17	140.93	179.36	92.17	92.17	53.74	76.87	5.62
TIME	8:13:5	8:14:14:5	8:14:16:3	8:14:20:1	b:14:33:	8:14:34:3	8:14:59:1	8:14:59:5	8:15: 0:4	8:15: 1:2	8:15: 2:1	:15: 3:2	8:15: 4:5	8:15: 6:1	8:15: 8:4	8:15: 9:2	8:15:10:	8:15:10:3	8:15:11:1	8:15:11:5	8:15:12:5	8:15:13:4	8:15:14:1	8:15:15:	8:15:15:5	8:15:17:	:15:18:1
	-		,,		'n			•	6	10.		12.	13.	14	15.	16.	17.	18	6	50	21.	22.	23	24.	25.	26.	27.

1558.750	591.25	205.00	1635.00	725.00	1678.75	7808.75	4661.25	1552.50	3110.00	4491.25	1227.50	7687.50	0453.75	3312.50	7106.25	0476.25	3477.50	6838.75	4267.50	1511.25	8277.50	4400.00	1102.50	7536.25	010.00
٠.	'n		'n	. 9	7.	•	6	. 0	_	. ~	- ~	せ	S	v	1	. 00	0	0	_	l (V		•	เนา	v	27.

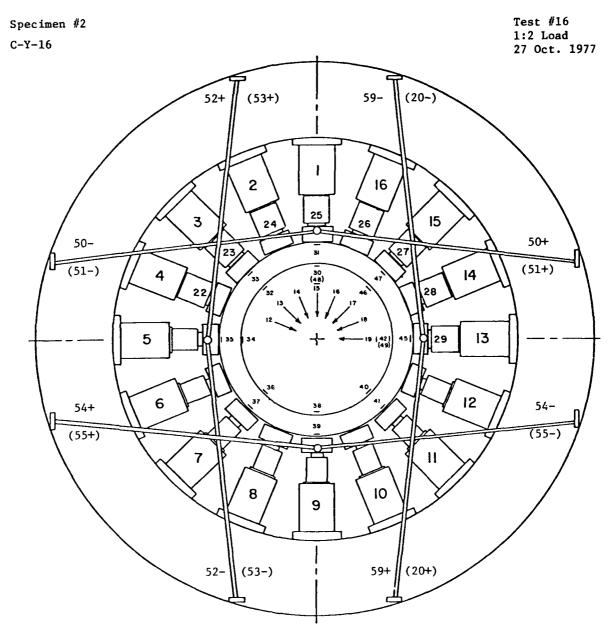
MAXIMUM LOAD CHANNEL, 25 REACHES A MAXIMUM VALUE AT STEP NUMBER 7

## 3.2.2 SPECIMEN #2

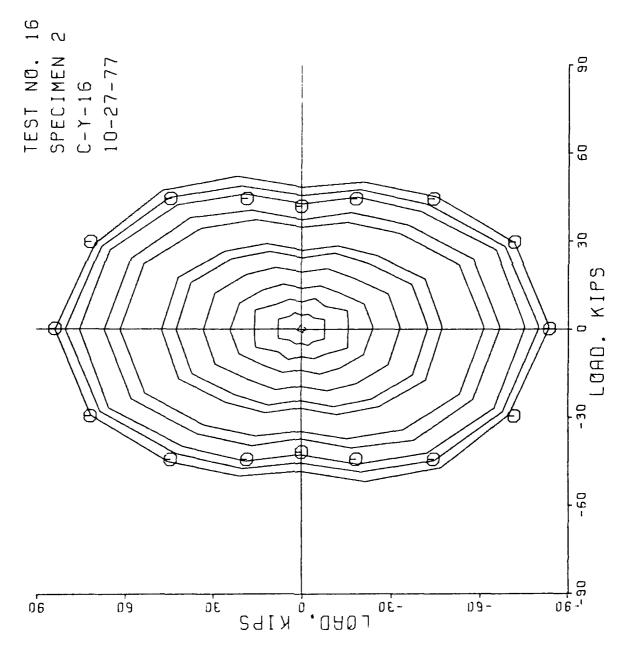
TEST NO. 16
COMPOSITE INTEGRAL LINER
1:2 LOADING RATIO
TESTED 27 OCTOBER 1977

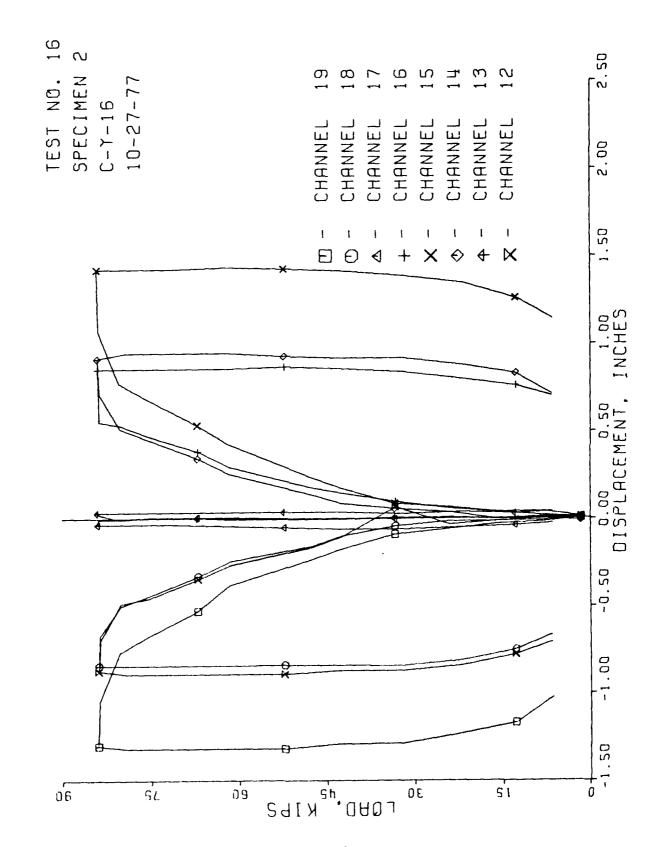


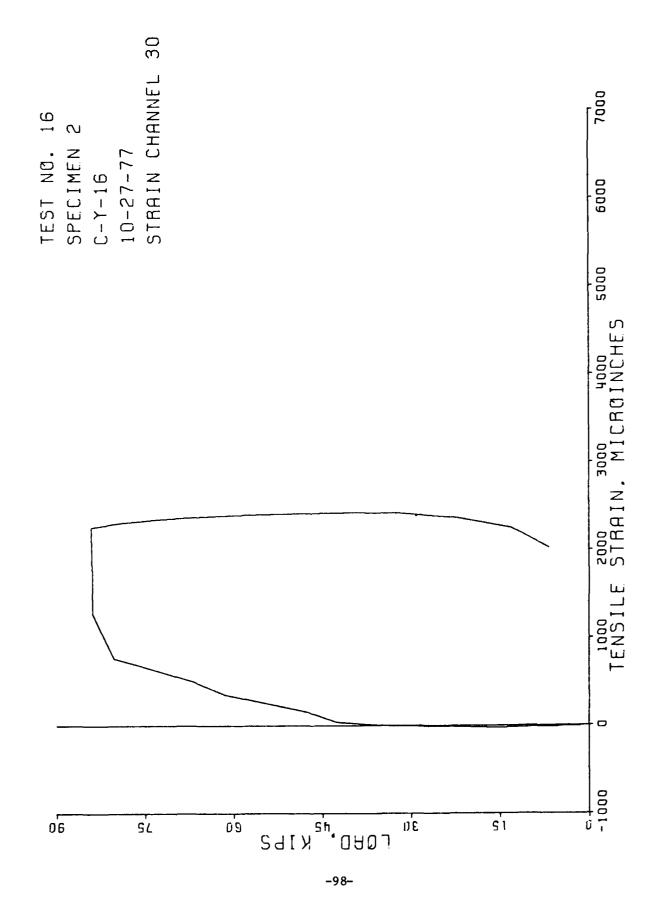
## REACTION FRAME TEST SET-UP

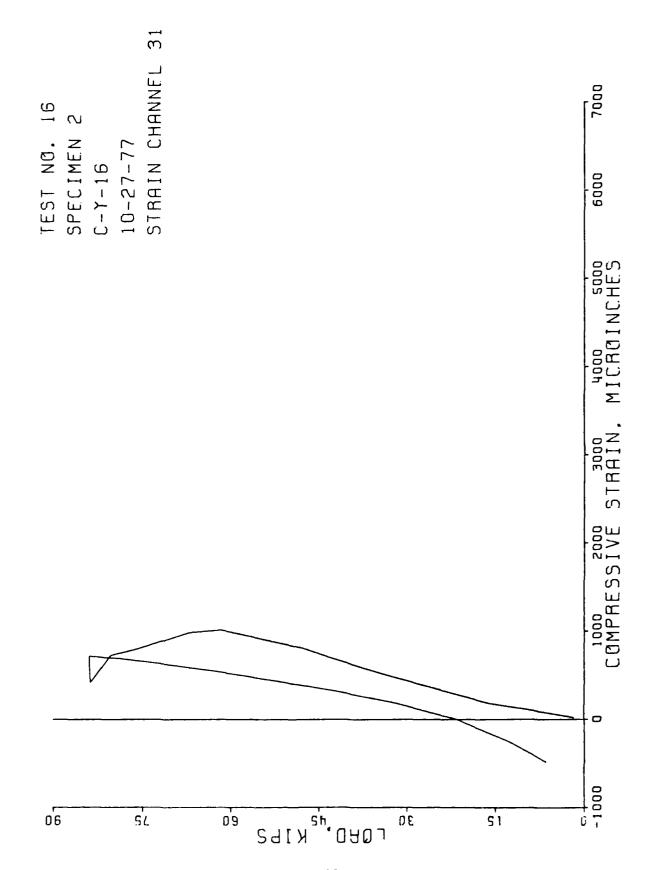


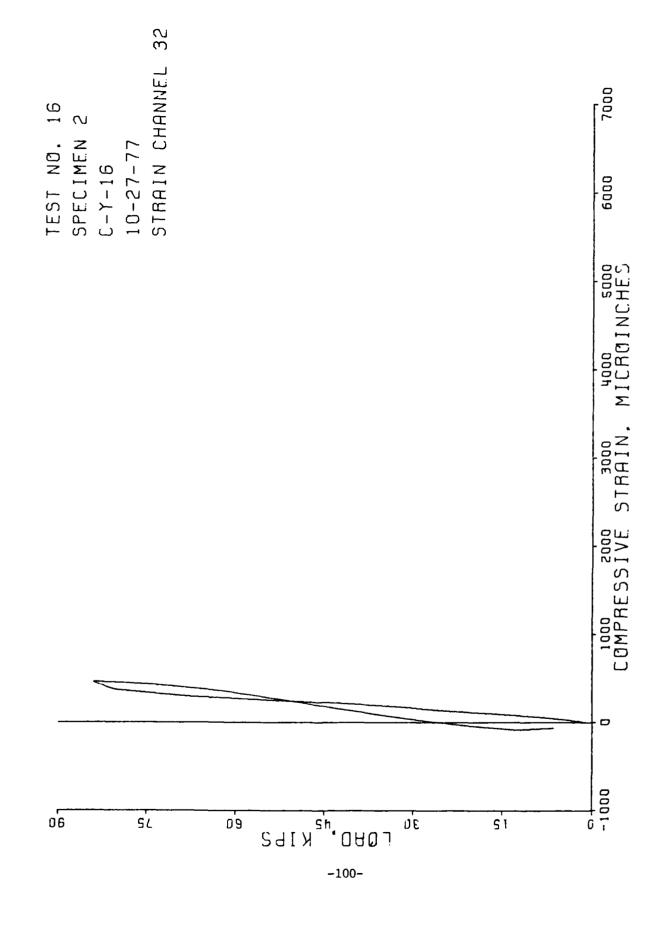
- CH 12-19 Load axis I.D. (Research, Inc. Model 4040).
- CH 22-29 Axial load (Transducers, Inc. Model 693-300K).
- CH 30-42, 45-49 (Ailtech SG 129-6S) Radial pairs 2" from top, except 48-49 2" from bottom. Odd gages 31-47 on rebar.
- CH 20,50-55, and 59 (Ailtech SG 129 6S) Polarity indicates rod under tension. Lower rod shown (XX).

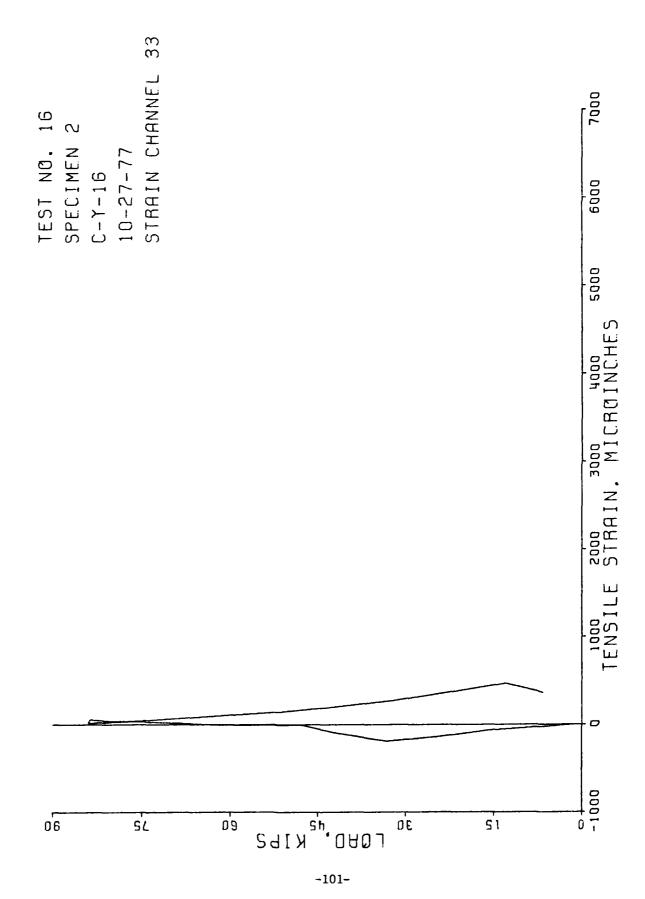


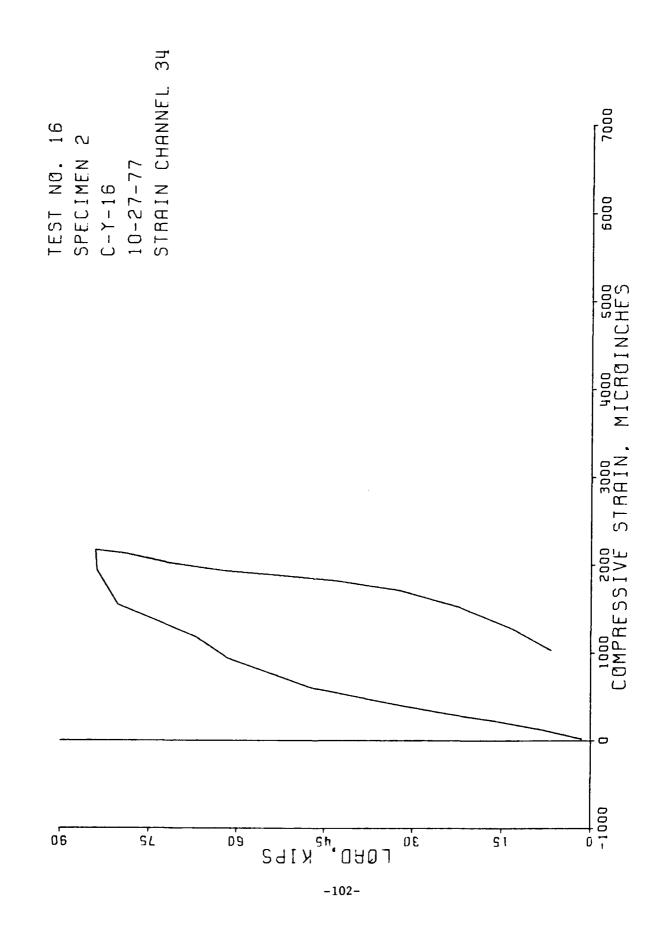


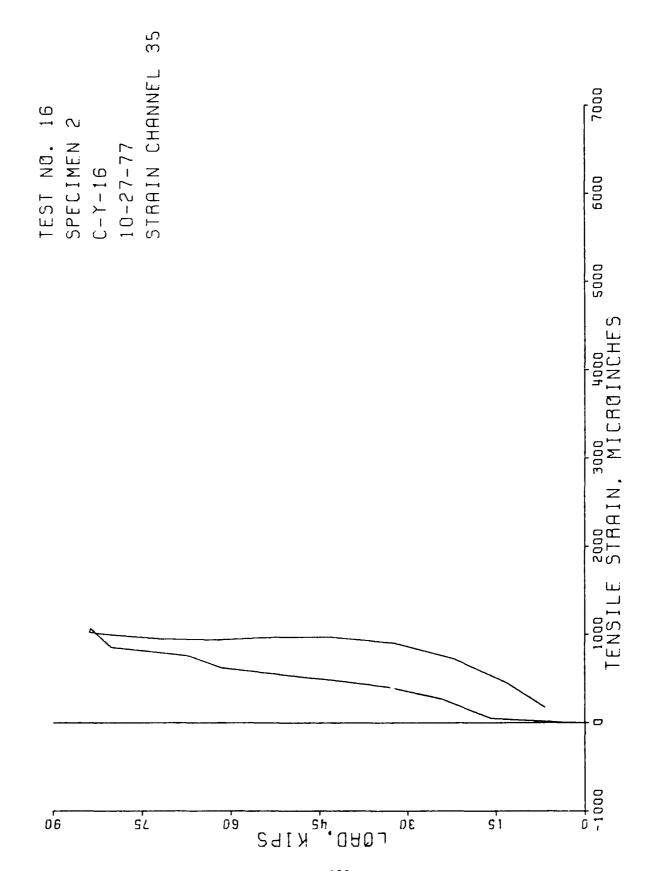


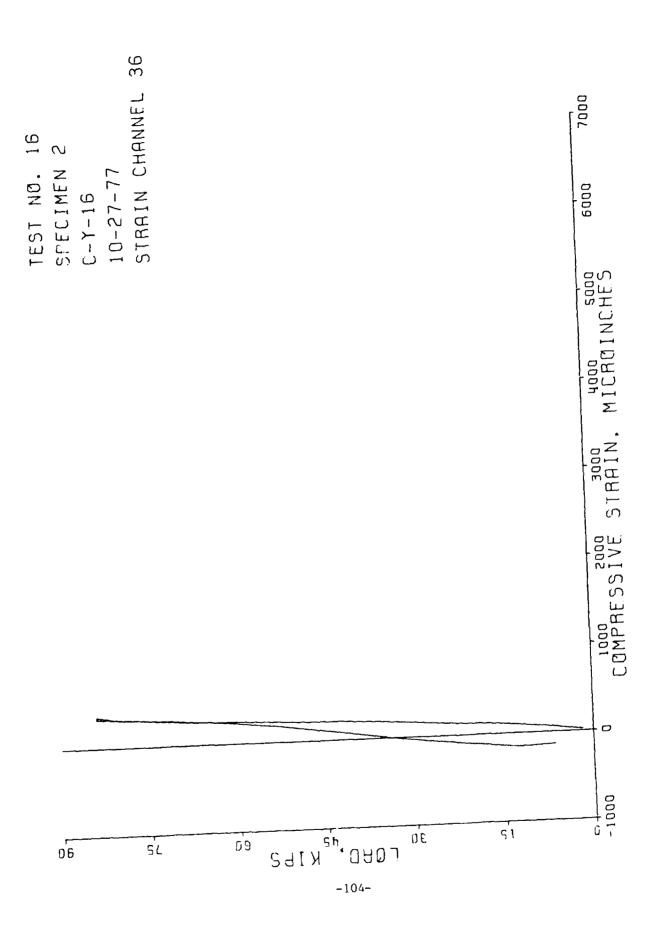


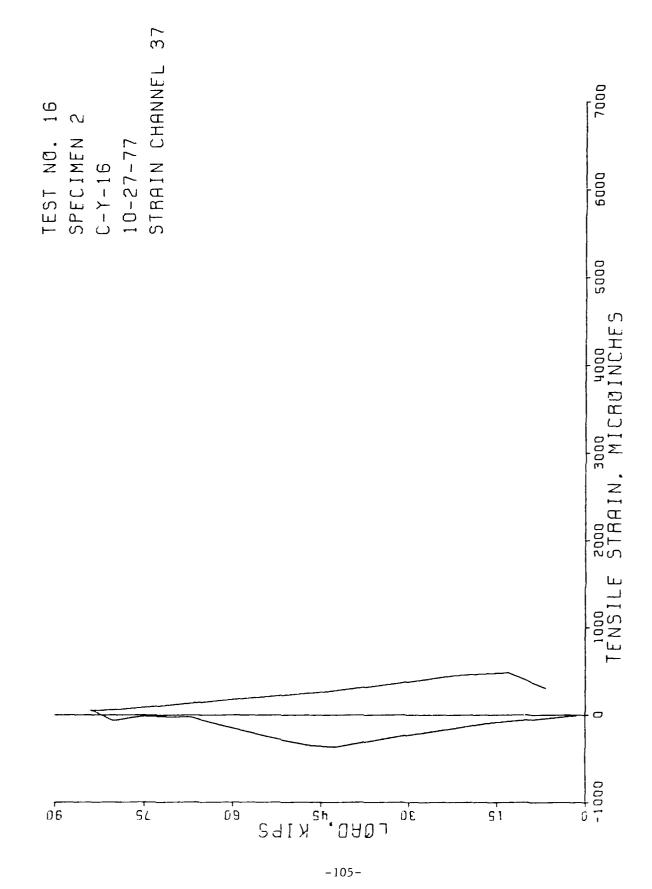


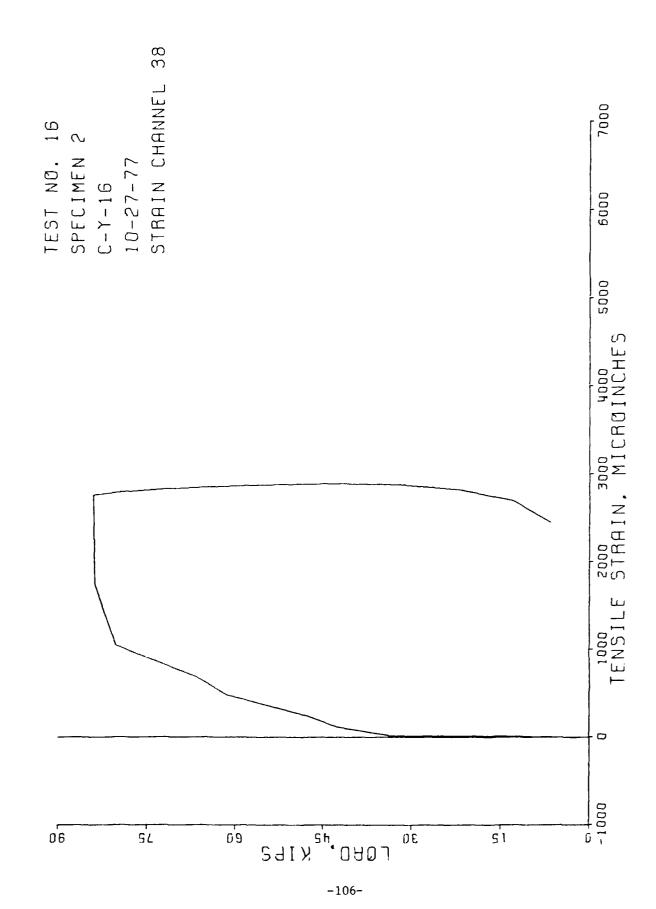


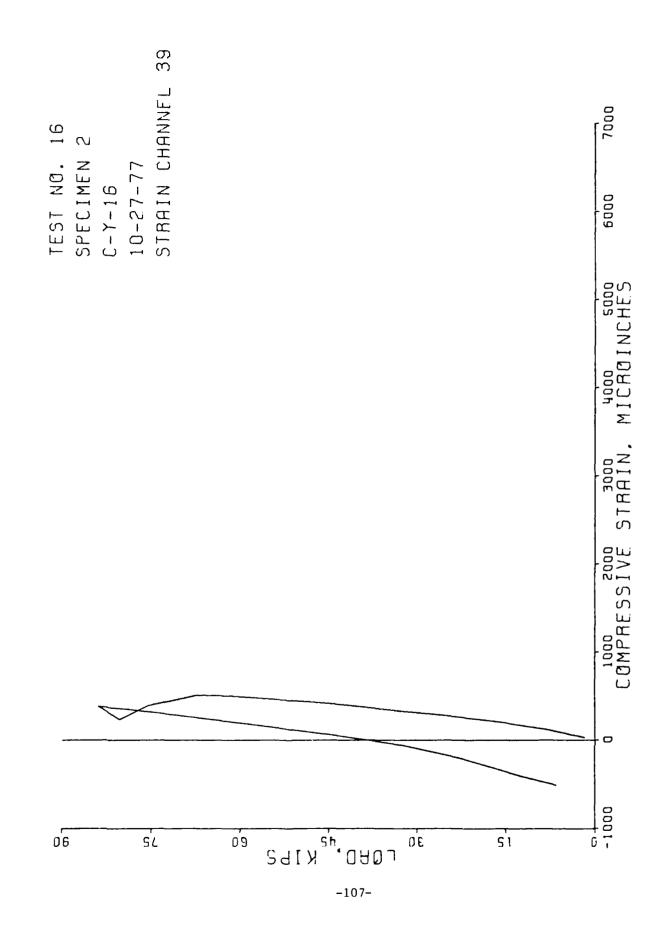


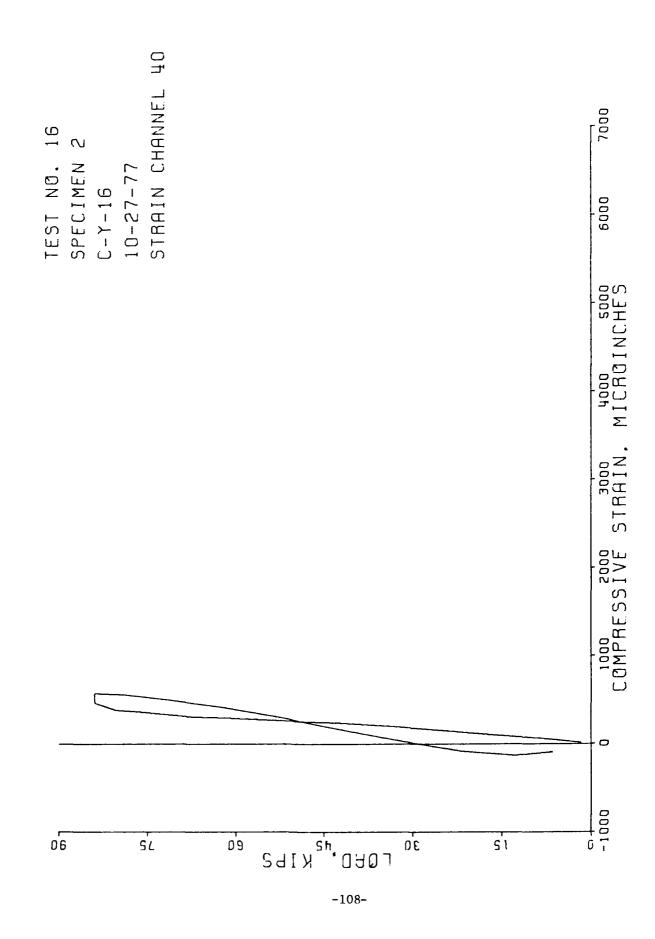


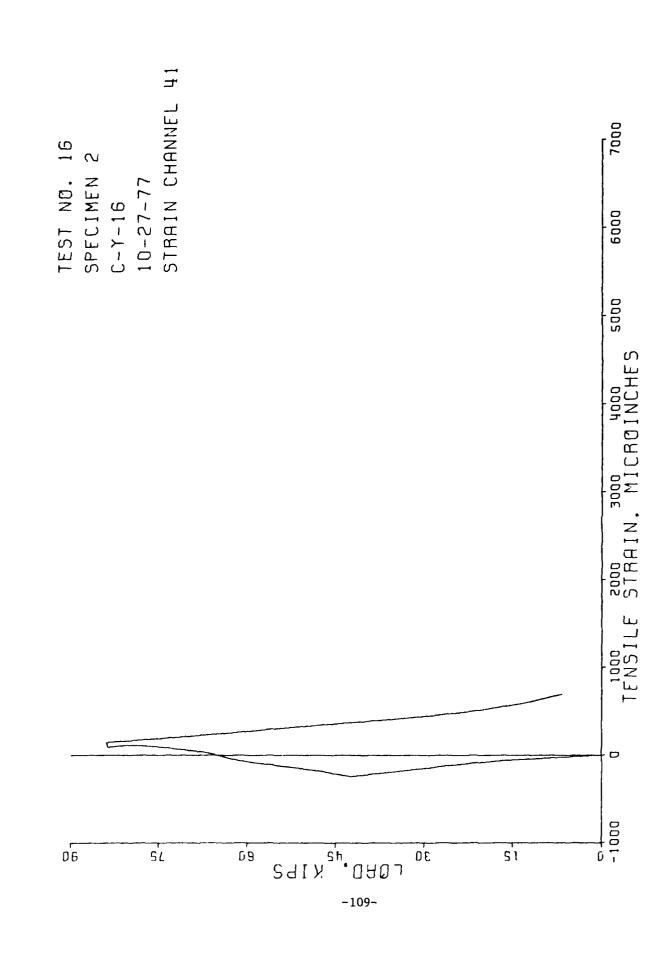


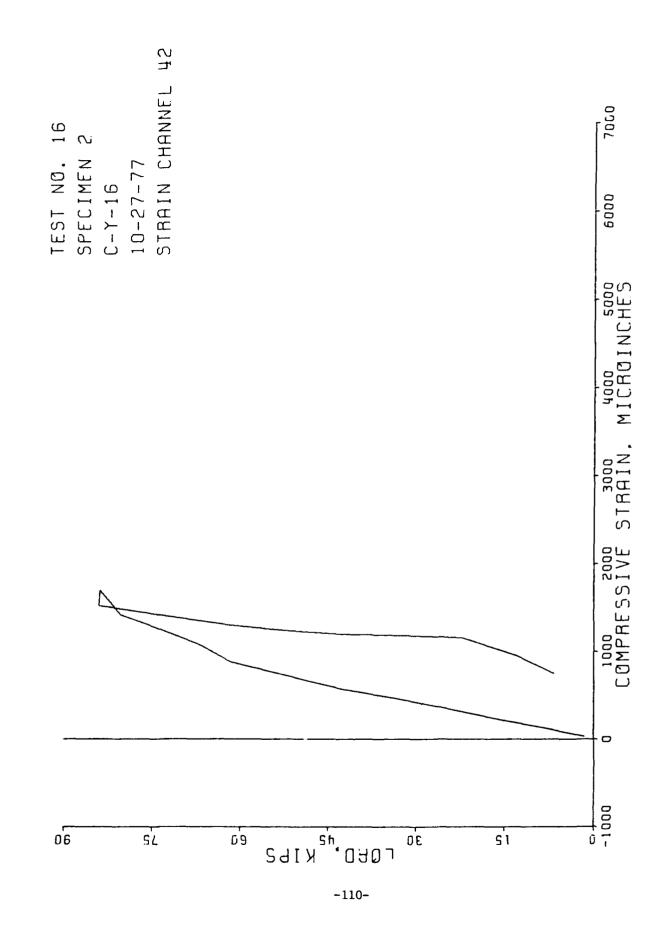


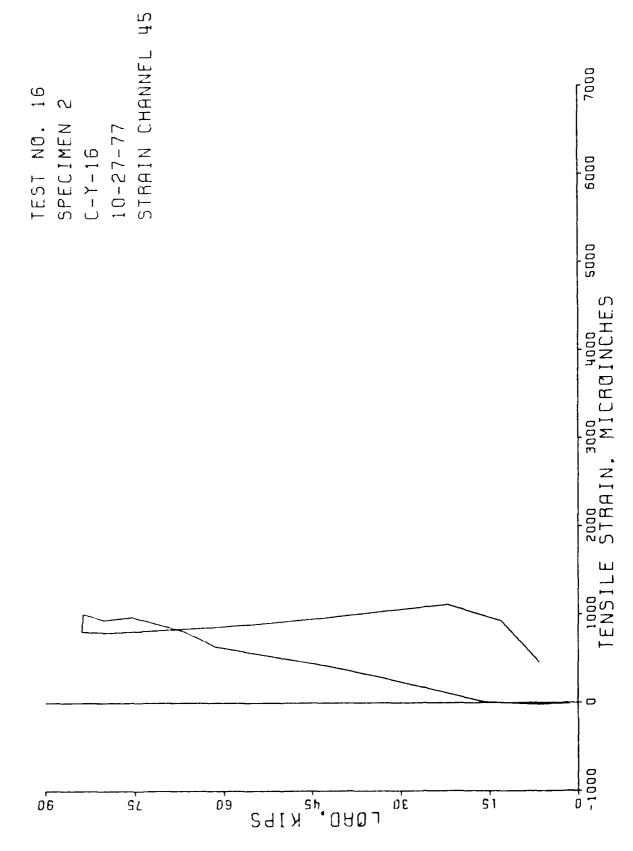


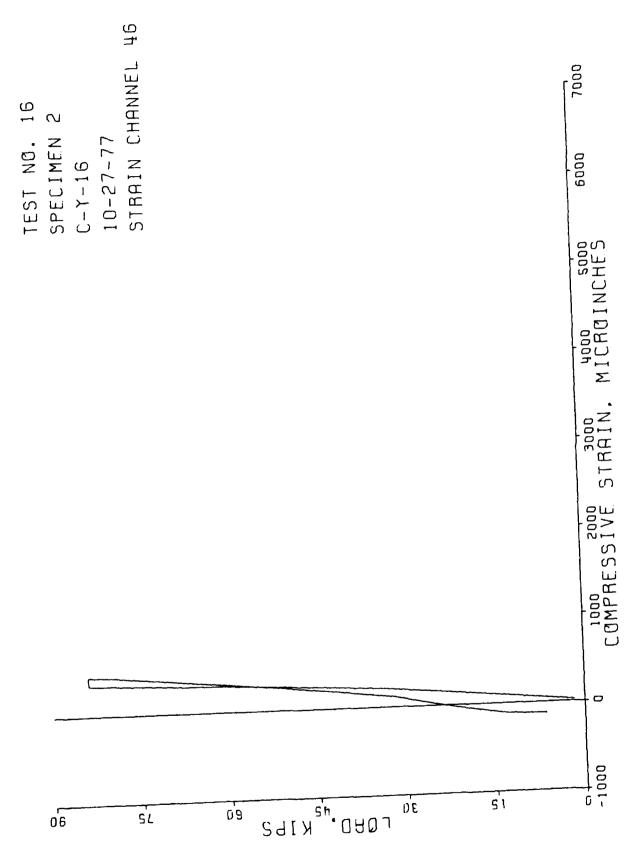


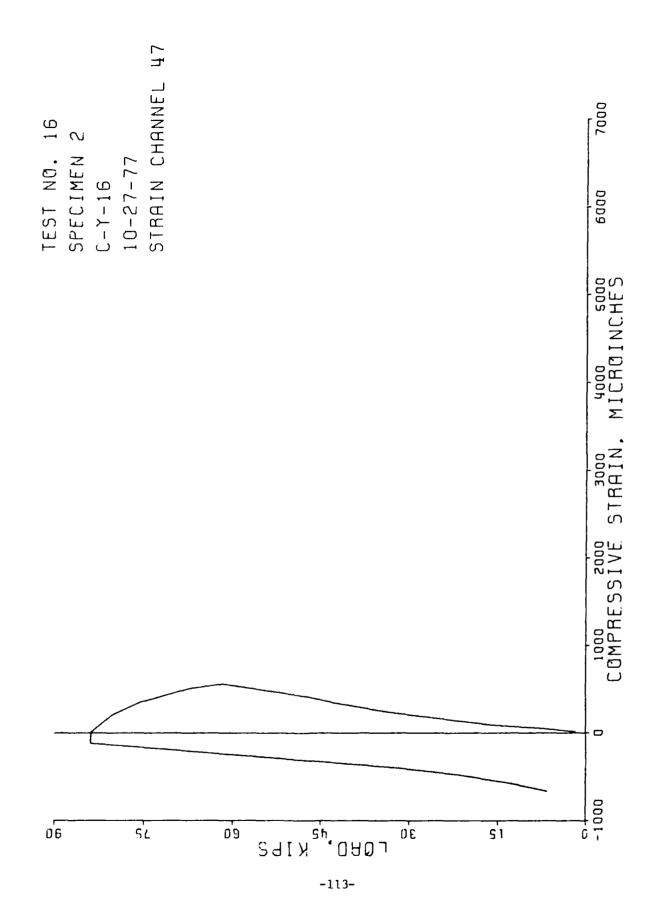


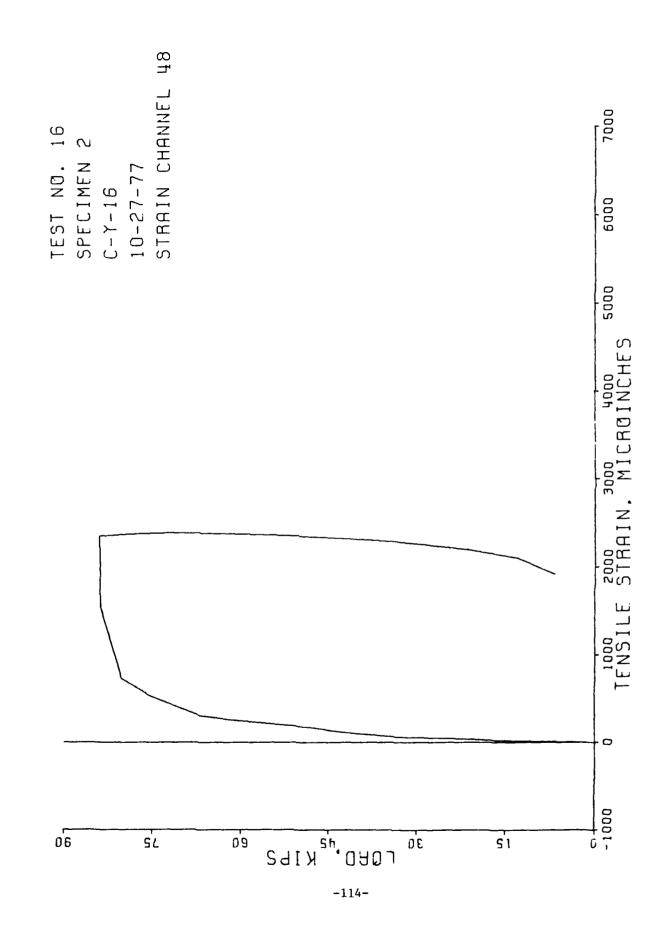


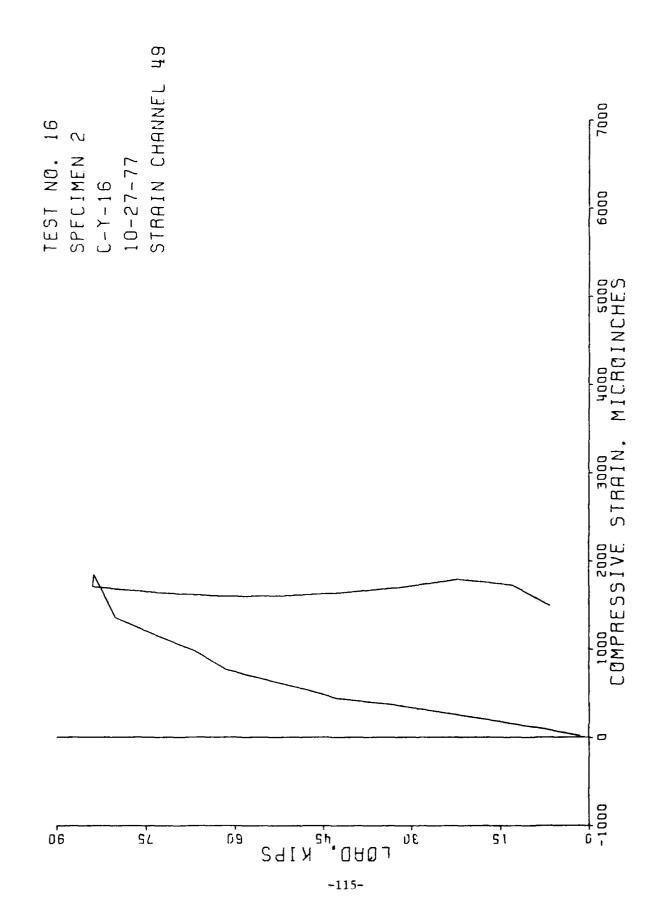












10-27-77			
C-Y-16	••	ZEROSHIFT	
SPECIMEN 2 C	MENTS= 22 B LS= 28 N CHANNELS= 18 ACEMENT CHANNELS= CHANNELS= 8 URE CHANNELS= 0		
TEST NO. 16	NUMBER OF INCRE NUMBER OF STAANN NUMBER OF DISPL NUMBER OF DISPL NUMBER OF LOAD AUMBER OF RESSI	CHANNEL	8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8

CALIBRATION

STRAIN CHANNEL

	CALIBRATION	0.0000000000000000000000000000000000000	CALIBRATION	10.00000000000000000000000000000000000	CALIBRATION	
444444444 $980490000000000000000000000000000000000$	DISPLACEMENT CHANNEL	19 17 16 15 12	LOAD CHANNEL	222289 224 234 234 234	ROD CHANNEL	ουνυνυνο ουνυνισο

CH.40	11111111111111111111111111111111111111	95.000
CH.41	-15.000 -1161.000 -1172.000 -1172.000 -1250.00	693.000
CH.42		-750.000
CH.45	11. 188. 1990 11. 188. 1990 11. 188. 1990 198. 1990 1990 1990 1990 1990 1990 1990 1990	465.000
6H.46	11.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1	123.000
CH.47	11111111111111111111111111111111111111	999
CH.48	22222222222222222222222222222222222222	1913.000
CH.49	11   1   1   1   1   1   1   1   1   1	
TIME	1. 27: 9:31:37 2. 27: 9:37:37 5. 27: 9:42:26 6. 27: 9:45:27 7. 27: 9:45:27 8. 27: 9:45:27 10. 27: 9:56:36 11. 27: 9:56:36 12. 27: 9:56:36 13. 27: 9:56:36 14. 27: 9:59:55 15. 27: 9:59:55 16. 27: 10: 1: 7 17. 27: 10: 2: 19 18. 27: 10: 3:32 18. 27: 10: 3:32 18. 27: 10: 3:32 18. 27: 10: 3:32 19. 27: 10: 3:32 19. 27: 10: 5:56	27:10:10

CHANN

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CH.32	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
CH.33	-3.000 -141.000 -196.000 -90.000 -44.000 -4.0000 -4.000 -4.000 -4.000 -4.000 -4.000 -4.000 -4.000 -4.000 -4.0
CH.34	-22.000 -218.000 -218.000 -218.000 -540.000 -540.000 -1175.000 -1928.000 -1928.000 -2118.000 -2118.000 -1924.000 -1870.000 -1570.000 -1570.000
CH.35	-2.000 22.000 468.000 483.000 483.000 627.000 759.000 825.000 994.000 974.000 975.000 173.000
CH.36	- 28.000 - 117.000 - 1142.000 - 1142.000 - 210.000 - 256.000 - 256
CH.37	-117.000 -1268.000 -1373.0
CH.38	-4
CH. 39	11124. 11124. 12798. 12798. 1279. 12809. 128
TIME	1. 27: 9:31 2. 27: 9:31 3. 27: 9:37 4. 27: 9:37 6. 27: 9:44 7. 27: 9:44 15. 27: 9:56 11. 27: 9:56 12. 27: 9:56 13. 27: 9:56 14. 444

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CH.12	0.010 0.010 0.010 0.001
CH.13	00000000000000000000000000000000000000
CH.14	-0.01 0.00 0.00 0.00 0.00 0.00 0.00 0.00
CH.15	00000000000000000000000000000000000000
CH.16	0.00 0.00 0.00 0.00 0.00 0.10 0.10 0.10
CH.17	0.010 0.010
CH.18	0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0
CH.19	11.00.000.000.000.000.000.000.000.000.0
TIME	11. 27. 27. 27. 27. 27. 27. 27. 27. 27. 27

	CH.22	730.000	20.00	1360.00	6060.00	2410.00	8150.00	0820.00	9410.00	2980.00	8680.00	1510.00	4260.00	9540.00	6830.00	0750.00	4200.00	8830.00	50.00	6320.00	00.0020	50.00	50.00	
	CH.23	1020.000	00.07	20.00	90.06	30.00	90.06	10.00	10.00	00.00	00.00	90.00	00.00	30.00	00.00	20.00	00.00	00.00	00.00	50.00	00.00	20.00	10.00	
	CH.24	4.0	8470.00	6500.00	2520.00	1260.00	0020.00	4770.00	7330.00	2390.00	0550.00	3850.00	7270.00	3490.00	2690.00	7880.00	8540.00	9061.00	30.00	0790.00	0870.00	1560.00	140.00	
	CH.25	009	8020.00	5890.00	4190.00	3330.00	2580.00	7520.00	1600.00	7080.00	5490.00	0240.00	3760.00	3970.00	00.0906	1700.00	2050.00	2200.00	940.00	2060.00	1890.00	2800.00	500.00	
	CH.26	1290.000	8520.00	6920.00	2770.00	1860.00	0750.00	5470.00	8010.00	2790.00	0640.00	3790.00	00.0609	1130.00	8630.00	0170.00	1300.00	2690.00	60.00	6510.00	8140.00	0330.00	60.00	
	CH.27	730.00	6000.000	1790.00	8630.00	6260.00	3770.00	7440.00	8570.00	3620.00	9770.00	3370.00	6770.00	0680.00	8760.00	3470.00	6380.03	9110.00	400.00	4140.00	6540.00	520.00	010.00	
	CH.28	0.00	6000.0009	350.00	510.00	770.00	520.00	500.00	370.00	310.00	300.00	750.00	380.00	050.00	760.00	970.00	590.00	000.000	390.00	410.00	930.00	170.00	0.00	
S — ш	CH.29	0.00	4820.000	00.09	3880.00	9430.00	4270.00	6800.00	4770.00	7310.00	2700.00	5620.00	8470.00	7630.00	6150.00	9430.00	0500.00	1030.00	90.00	1650.00	0460.00	40.00	50.00	
0 A O C H A N	TIME	. 27: 9:3	: 9:37	. 27: 9:39	. 27: 9:42	. 27: 9:44	. 27: 9:45	. 27: 9:47	. 27: 9:50	. 27: 9:53	. 27: 9:56	. 27: 9:56	. 27: 9:57	. 27: 9:59	. 27: 9:59	. 27:10: 1	27:10: 2	. 27:10: 3	. 27:10: 4	. 27:10: 5	. 27:10: 7	. 27:10: 8	. 27:10:10	
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CH.20	204.989 -102.494 -38.435 -12.812 -12.812 -12.65.236 -1511.792 -2331.747 -273
CH.50	64.059 -172.494 -173.365 -244.424 -294.424 -294.483 -192.177 -192.177 -192.177 -192.177 -255.624 -2530.612 -2530.612 -255.624 -255.624 -255.624 -255.624 -255.624
CH.51	220.295 281.859 281.859 115.306 115.306 102.494 102.494 284.241 2544.241 2544.241 2544.241 2544.241 2544.241 2544.241 2544.241 2544.241 2544.241 2544.241 2544.241 2544.241 2544.241 2544.241 2544.241 2544.241 2548.413 1255.556
CH.52	-230.612 -179.365 -1279.365 -1279.365 -1204.989 -358.413 -4599.660 -4599.600 -4599.600 -4599.600 -4599.600 -4599.600 -4599.600 -4599.600
CH.53	64.059 -128.118 -140.930 -166.533 -384.555.284 -525.284 -653.402 -807.143 -1422.109 -1422.109 -1422.109 -1422.109 -1422.250 -871.202 -871.202 -871.202 -871.202 -871.202 -871.202 -871.202 -871.202 -871.202 -871.202 -871.202
CH.54	12.812 25.624 25
CH.55	255 624 1255 624
CH.59	-64.059 -76.871 -230.612 -166.533 -166.553 -166.553 -166.553 -166.553 -166.553 -166.563 -166.563 -166.563 -166.563 -167.494 -167.494 -175.494 -175.494 -175.494 -175.494 -175.494 -175.494 -175.494 -175.494 -175.494 -175.494 -175.494
TIME	1. 27: 9:31:37 3. 27: 9:37:37 4. 27: 9:42:26 5. 27: 9:45:27 7. 27: 9:45:15 8. 27: 9:47:15 9. 27: 9:57:34 9. 27: 9:50:34 10. 27: 9:56:36 11. 27: 9:56:36 12. 27: 9:57:48 13. 27: 9:56:36 14. 27: 10: 2: 19 16. 27: 10: 2: 19 17. 27: 10: 2: 19 18. 27: 10: 2: 19 18. 27: 10: 2: 19 19. 27: 10: 2: 19 20. 27: 10: 5: 56 20. 27: 10: 5: 56 21. 27: 10: 5: 56 22. 27: 10: 6: 56 22. 27: 10: 6: 56 22. 27: 10: 6: 56

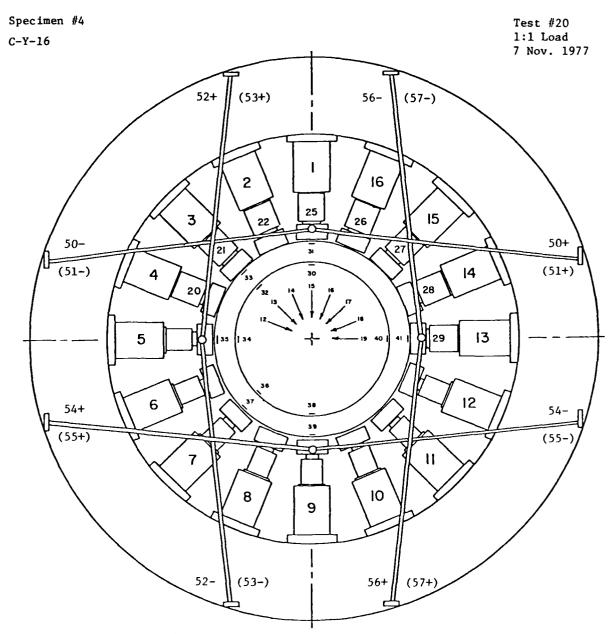
1076.250 6615.000	948.75	6487.50	3718.75	7478.75	8275.00	2540.00	9271.25	2652.50	5850.00	5352.50	2597.50	5998.75	7891.25	9873.75	2432.50	3666.25	5353.75	198.75	193.75
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MAXIMUM LOAD CHANNEL, 25 REACHES A MAXIMUM VALUE AT STEP NUMBER 13

## 3.2.3 SPECIMEN #4

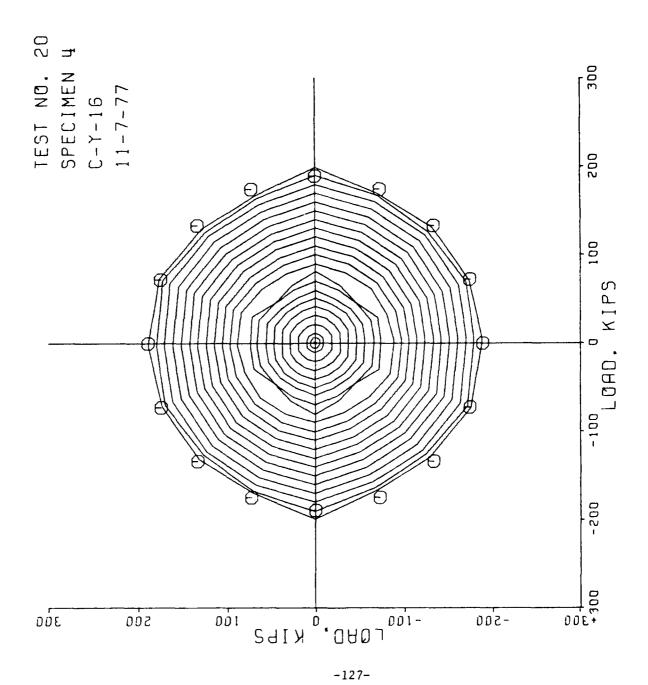
TEST NO. 20
COMPOSITE INTEGRAL LINER
1:1 LOADING RATIO
TESTED 7 NOVEMBER 1977

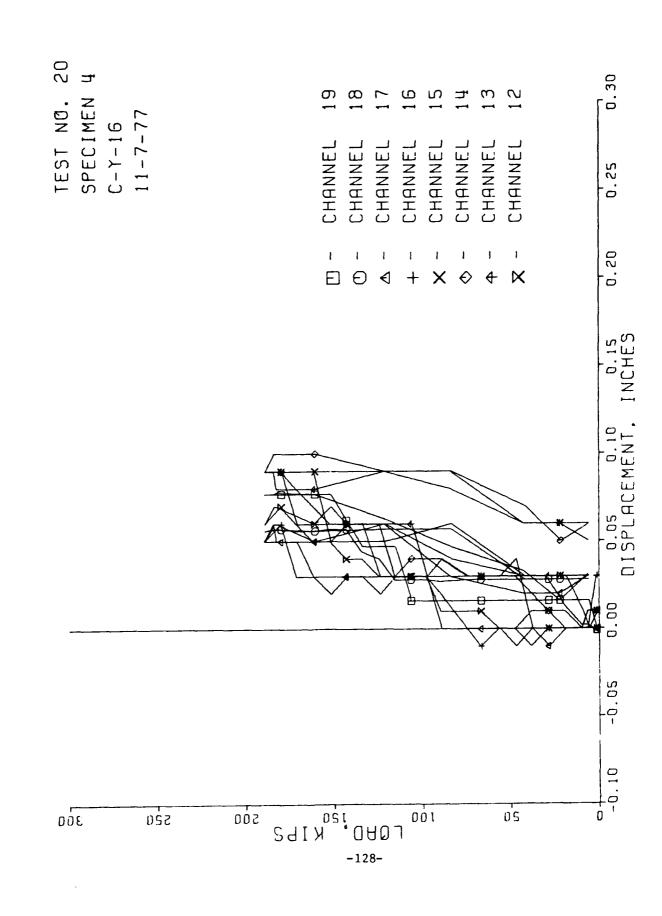
## REACTION FRAME TEST SET-UP

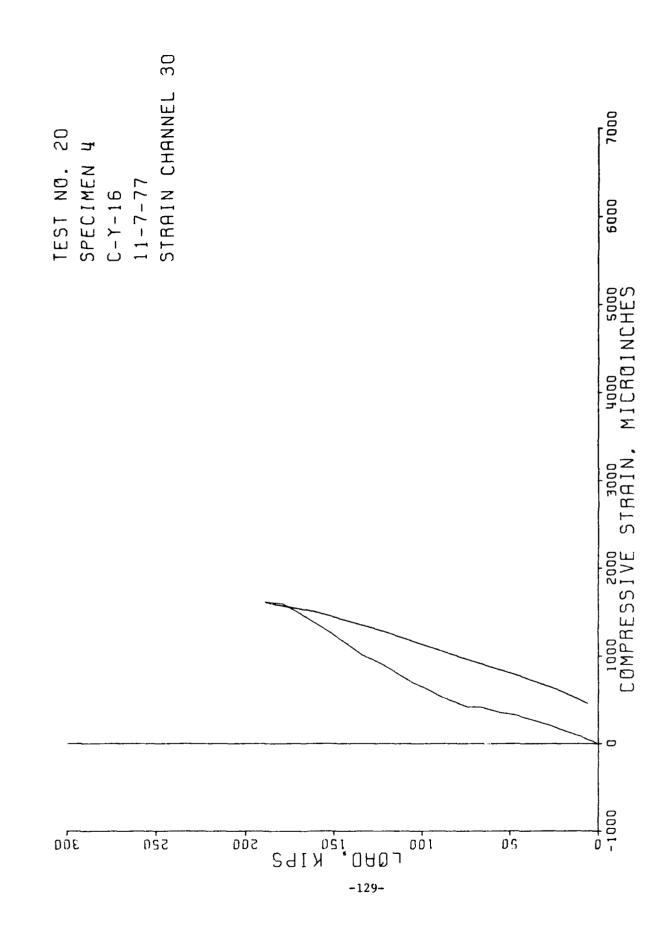


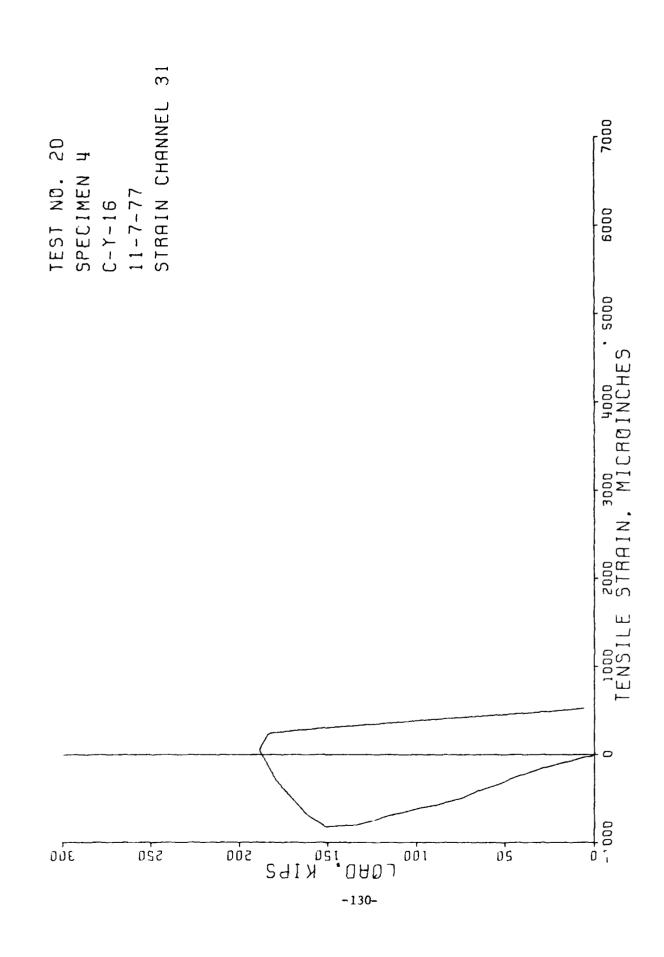
- CH 12-19 Load axis I.D. (Research, Inc. Model 4040).
- CH 20-22, 25-29 Axial load (Transducers, Inc. Model 693-300K).
- CH 30-41 (Ailtech SG 129-6S) Radial pairs 2" from top. Odd gages on Rebar.
- CH 50-57 (Ailtech SG 129-6S) Polarity indicates rod under tension.

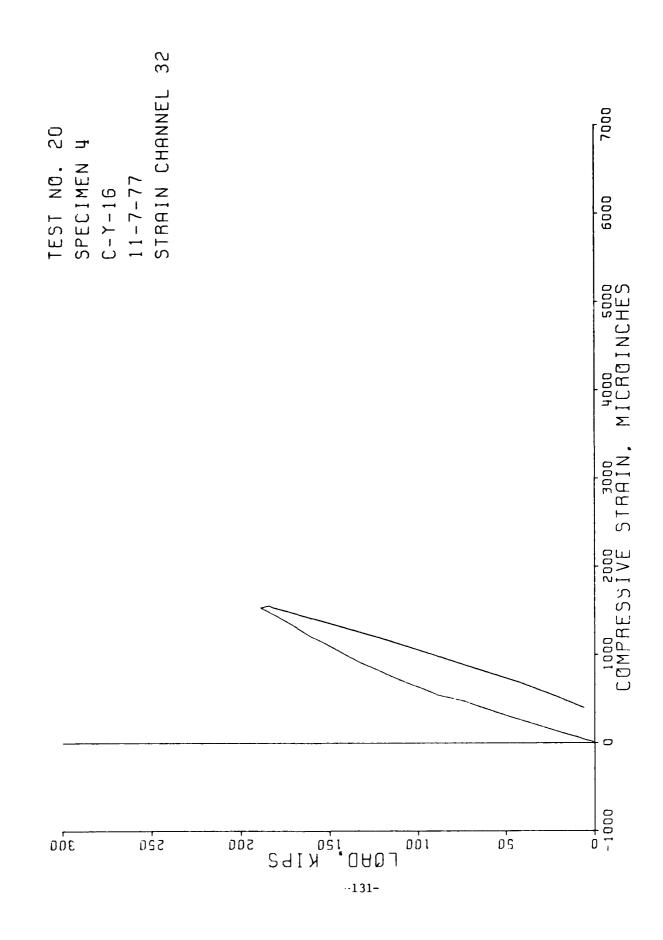
  Lower rod shown (XX).

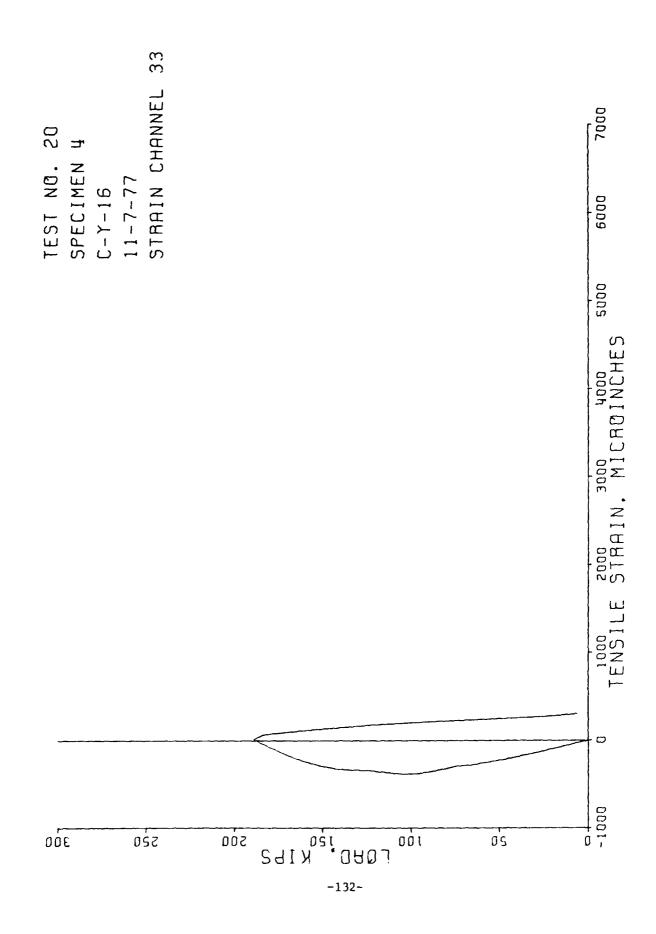


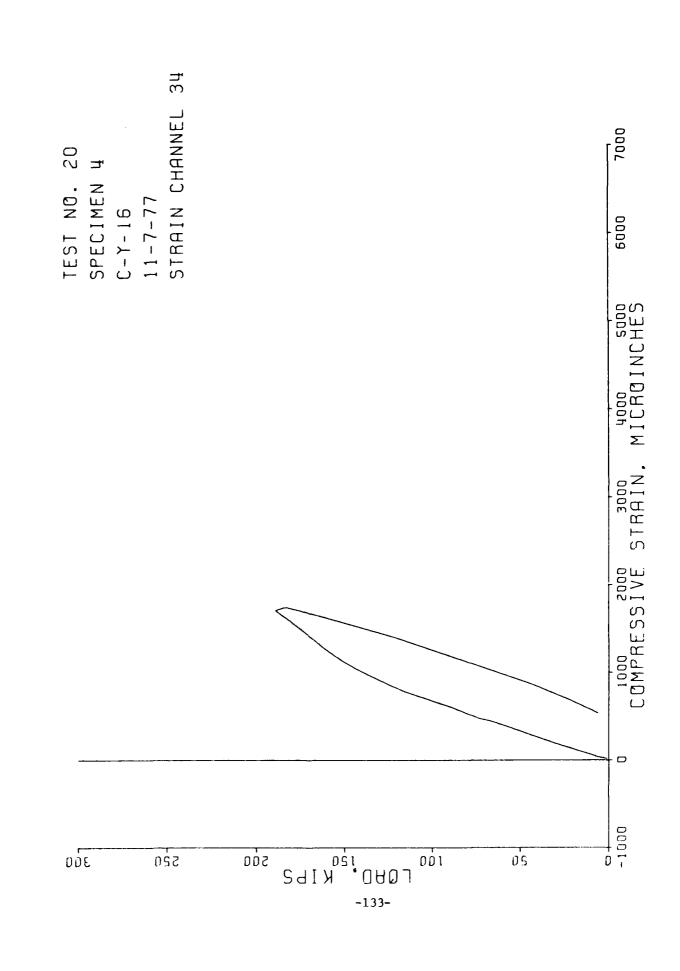


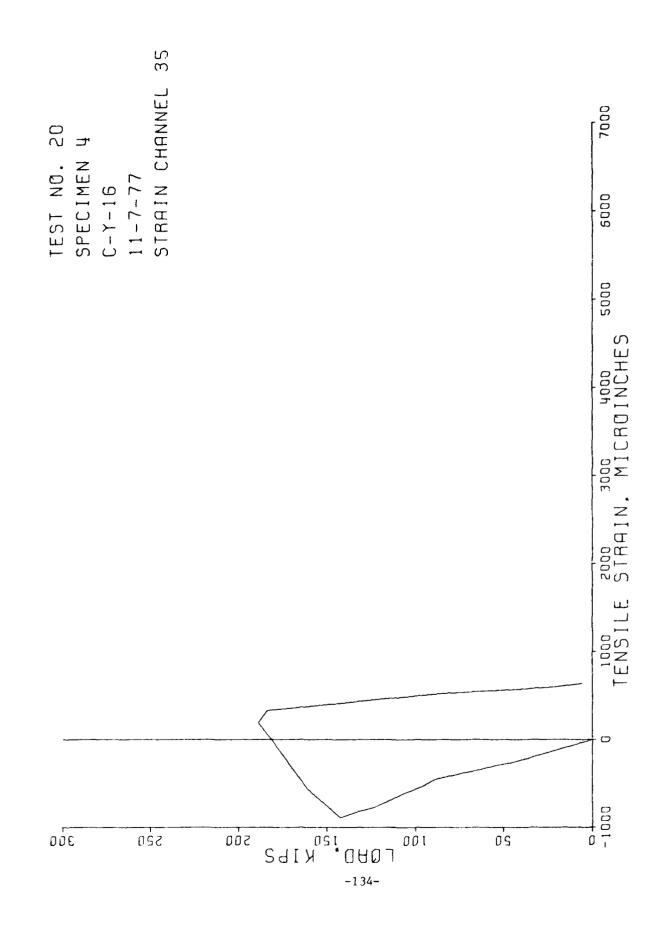


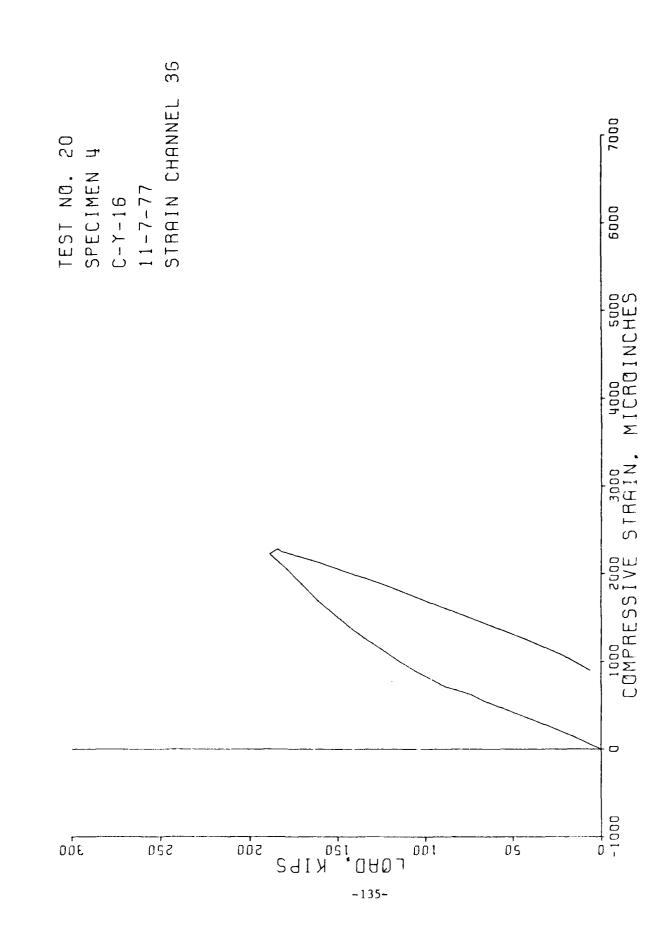


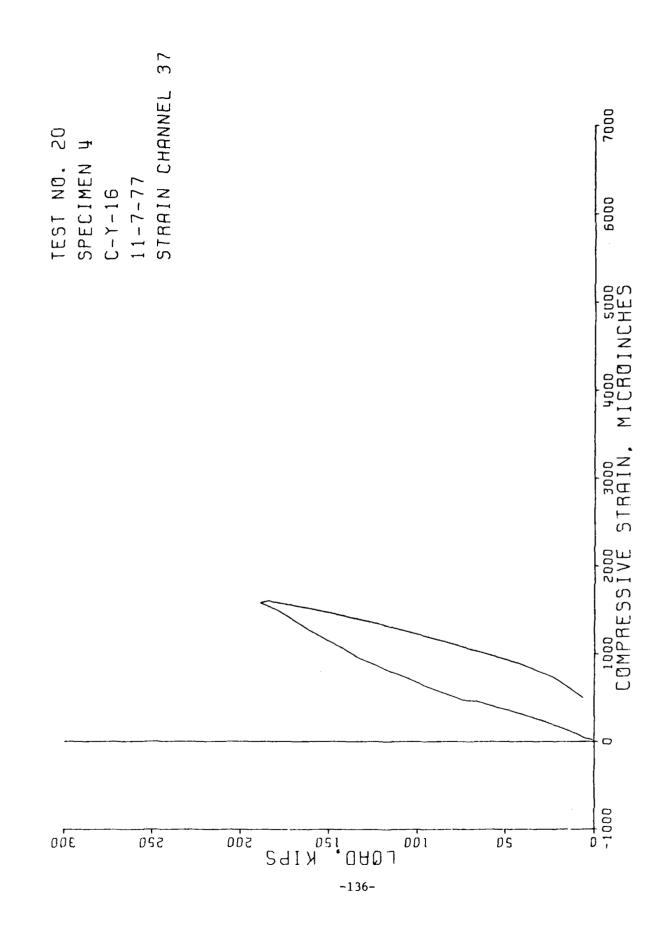


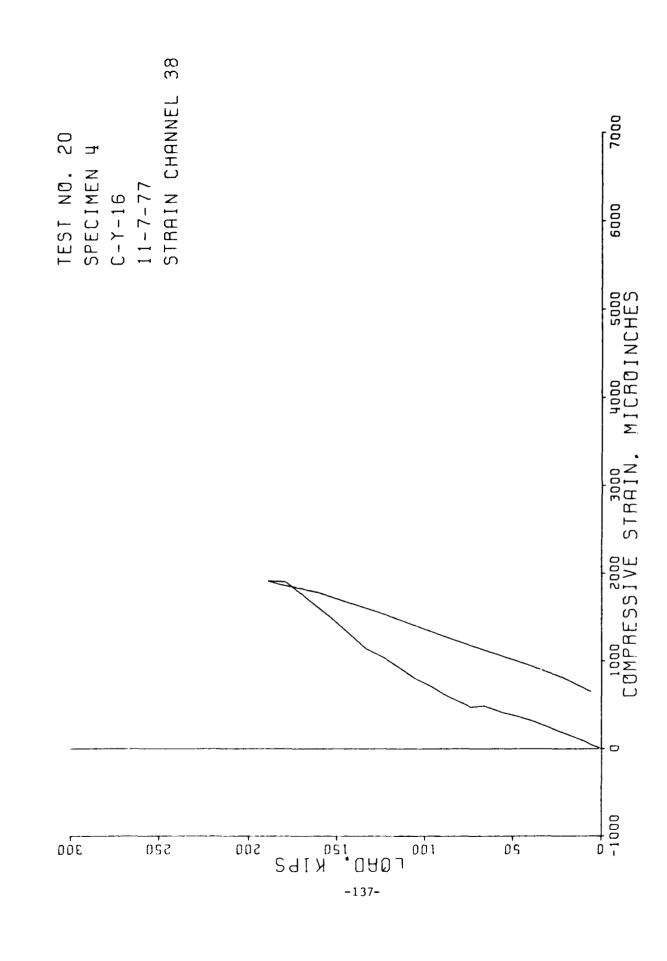


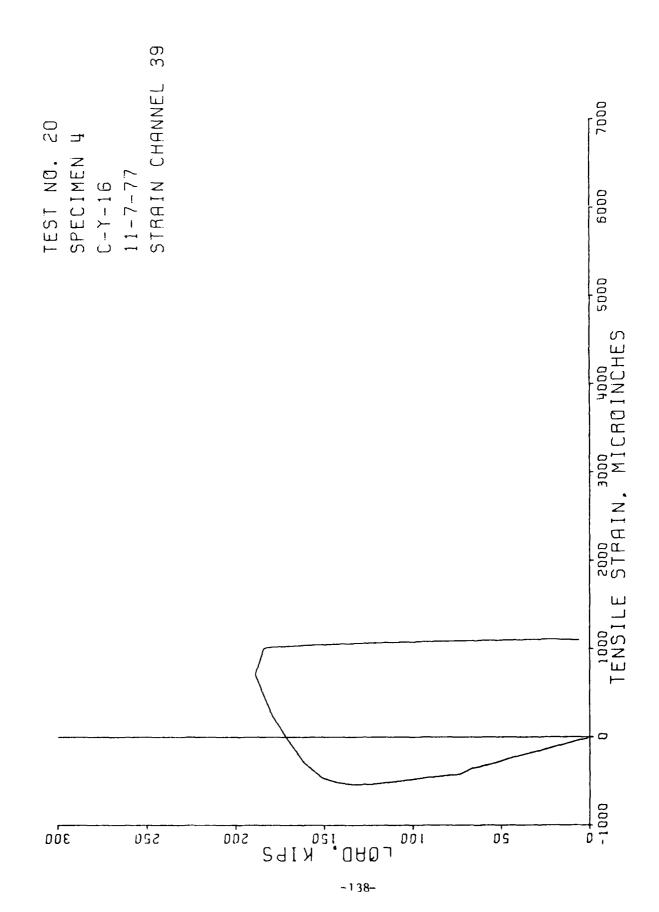


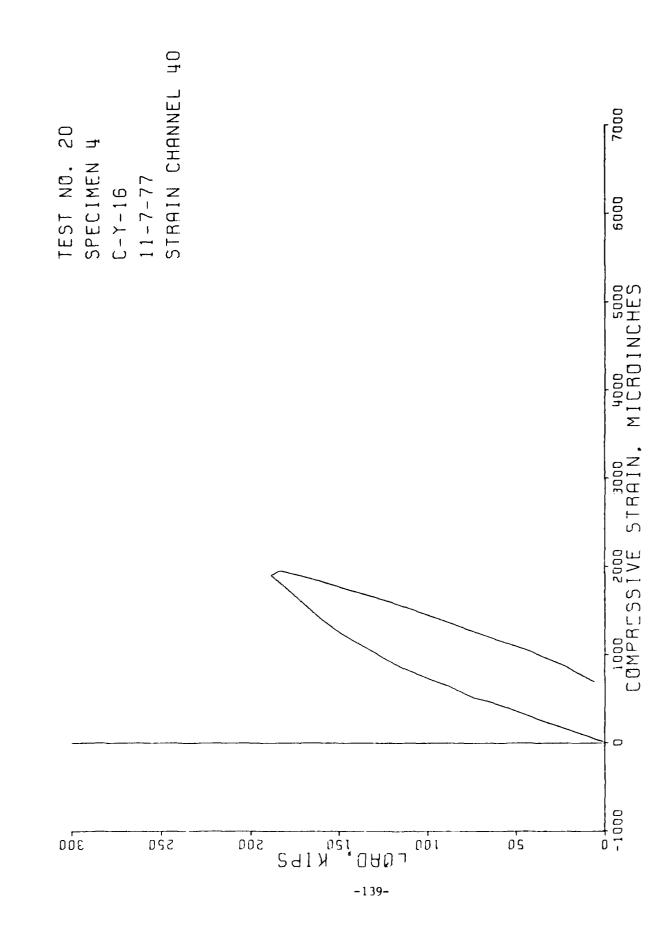


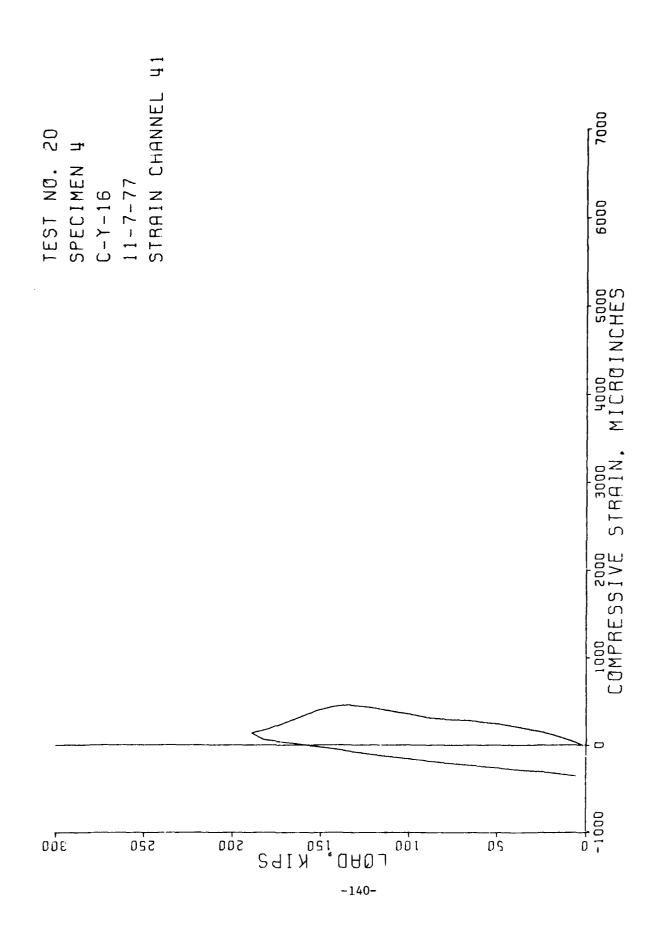












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CH.34	-13.000	5.00	1.00	1.00	182.00	243.00	0.00	376.00	3.00	479.00	7.00	658.00	2.00	781.00	854.00	949.00	1034.00	138.00	1274.00	1431.00	1571.00	1711.00	1743.00	1746.00	1632.00	1405.00	1151.00	861.00	691.00	536.00
CH.35	-5.000	2.00	55.00	10.00	167.00	221.00	63.00	298.00	356.00	378.00	450.00	538.00	90.	697.00	769.00	24.00	886.00	724.00	50.00	293.00	53.00	90.06	30.00	40.00	79.00	61.00	28.00	77.00	01.00	41.00
CH.36	-12.000	8.00	84.00	68.00	248.00	325.00	94.00	465.00	547.00	620.00	716.00	804.00	894.00	1001.00	1118.00	1250.00	1379.00	28.00	1693.00	1878.00	2053.00	2224.00	2286.00	2255.00	2130.00	1859.00	1572.00	1248.00	075.00	897.00
CH.37	-18.000	46.00	84.00	62.00	33.00	295.00	55.00	401.00	463.00	74.00	585.00	650.00	729.00	801.00	77.00	959.00	1068.00	63.00	1278.00	1394.00	1505.00	1587.00	1609.00	1601.00	521.00	343.00	140.00	897.00	31.00	500.00
CH.38	-11.000	5.00	83.00	60.00	236.00	309.00	72.00	417.00	489.00	473.00	618.00	718.00	7.00	930.00	1045.00	146.00	1305.00	1465.00	1619.00	1771.00	1903.00	1917.00	1883.00	873.00	1785.00	525.00	252.00	965.00	815.00	657.00
CH.39	6.00	4.00	55.00	00.90	155.00	201.00	50.00	308.00	354.00	423.00	457.00	475.00	-501.000	520.00	539.00	547.00	522.00	465.00	294.00	34.00	34.00	93.00	998.00	014.00	041.00	066.00	086.00	01.00	110.00	102.00
CH. 40	17.00	43.00	74.00	42.00	206.00	70.00	338.00	408.00	79.00	16.00	653.00	714.00	٥.	64.00	954.00	1069.00	1169.00	82.00	1420.00	1586.00	1745.00	1901.00	1949.00	1950.00	1837.00	1607.00	1342.00	1045.00	875.00	695.00
CH.41	2.00	33.00	61.00	23.00	72.00	12.00	39.00	59.00	86.00	88.00	13.00	49.00	-377.000	10.00	36.00	56.00	34.00	88.00	17.00	46.00	81.00	35.00	73.00	59.00	-6.00	09.00	95.00	3.00	11.00	55.00
TIME	: 8:42:	8:45:5	: 8:43:2	3:44:5	: 8:45:3	8:46:3	: 8:47:3	. 8:48:3	5:65:8 :	5:05:8:	8:51:4	. 8:52:4	7: 8:53:50	: 8:54:5	: 8:55:5	8:56:5	: 8:58:1	: 8:59:1	: 9: 0:2	: 9: 1:2	: 9: 2:2	: 9: 3:2	: 9: 6:2	: 9: 6:5	: 9: 8:1	: 9:10:3	: 9:12:3	5:51:6:	: 9:16:	: 9:17:
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	CH.30	 	146.00	213.00	277.00	51.00	422.00	420.00	537.00	627.00	705.00	815.00	920.00	1008.00	1141.00	1266.00	1384.00	498.00	1599.00	1616.00	1590.00	1583.00	1503.00	1279.00	1027.00	758.00	610.00	460.00
	CH.31 -16.000	00.0	99.00	152.00	209.00	53.00	418.00	492.00	574.00	606.00	651.00	691.00	744.00	799.00	811.00	819.00	689.00	495.00	297.00	47.00	32.00	45.00	91.00	51.00	08.00	67.00	97.00	24.00
	CH.32 -13.000	4.00	122.00	181.00	240.00	56.00	423.00	480.00	552.00	618.00	686.00	762.00	841.00	924.00	1019.00	1120.00	1221.00	337.00	1437.00	1533.00	1562.00	1538.00	1420.00	1195.00	954.00	688.00	534.00	400.00
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	TIME 8:42:	8:42:5	: 8:44:2	: 8:45:3	: 8:46:3	5 :	7:67:8	4:50:4	8:51:4	. 8:52:4	. 8:53:5	: 8:54:5	: 8:55:5	3:95:8:	: 8:58:1	: 8:59:I	: 9: 0:2	: 9: 1:2	: 9: 2:2	: 9: 3:2	: 9: 6:2	9:9:6:	: 9: 8:1	: 9:10:3	: 9:12:3	5:51:6:	: 9:16:	: 9:17:
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DISPLACEMENT CHANNELS

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CH.20	1240.00 5960.00 0100.00	0370.00 0150.00 9500.00	8880.00 910.00	0700.00	96890.00	16460.00	35630.00 45320.00	55010.00 64510.00	3830.00 1070.00 3250.00	78690.00 78790.00	60810.00 21620.00	86920.000 43010.000 22620.000 6030.000
CH.21	1340.00 5530.00 0220.00	9720.00 9360.00 8900.00		4220.00	97140.00	16490.00	35710.00	54960.00 64480.00	3880.00 9130.00 5930	79620.00	60730.00 23410.00	85920.000 43580.000 23240.000 6040.000
CH.22	1960.00 5780.00 0530.00	0360.00 9900.00 9240.00	250.00 840.00	5460.00	96720.00	15960.00	35100.00	54390.00	4020.00 3250.00 7080.00	85920.00	64870.00 25930.00	90510.000 42560.000 21850.000 5240.000
CH.25	960.00 5720.00 9190.00	8660.00 8230.00 7710.00	960.00	4090.00	97410.00	15130.00	33950.00	51800.00	0870.00 9560.00 8910.00	83760.00	60490.00 21310.00	83660.000 42070.000 21850.000 5380.000
CH.26	2100.00 5720.00 0540.00	0740.00	90.00	8080.00	01160.00	19690.00	39190.00	58150.00 67810.00	7950.00 6790.00 6960.00	89740.00	59730.00 21140.00	86244.000 41230.000 21310.000 5060.000
CH.27	1290.00 5660.00 0360.00	0060.00 9690.00 9100.00	110.00 840.00	4210.00 6590.00	96360.00	15610.00 25140.00	34280.0043700.00	53060.00	1520.00 7620.00 3140.00	75190.00	59260.00 23660.00	84400.000 43450.000 23010.000 5120.000
CH.28	1350.00 6360.00 0530.00	0370.00	9000	5090.00	95000.00	14470.00	32980.0042470.00	51860.00 61060.00	7190.00	81700.00	23600.00	85190.000 42000.000 21890.000 4160.000
CH.29	1170.00 6070.00 0920.00	1240.00 1490.00	970.00 550.00	0810.00 9730.00	100580.00	30380.00	50080.00	59790.00 69810.00	9540.00 0070.00	90140.00	60280.00 21080.00	\$1810.000 41550.000 20520.000 4150.000
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CH.50	894. 894. 894. 894. 894. 894. 897. 897. 897. 897. 897. 897. 897. 897	512.47
CH.51	166.553 166.553 166.553 1700.9512 1700.9	- 00
CH.52	- 89.683 - 1.2536.236 - 1.2536.236	5.60
CH.53	1140 1110 1110 1110 1110 1110 1110 1110	384.3
CH.54	115.8 115.8 116.0	86.84
CH.55	1115 1115 1115 1115 1115 1117 1217 1217 1217 1217 1227 1227 1227 1228 1238	58.73
CH.56	1002 1002 1002 1002 1002 1002 1002 1002	. 60
CH.57	1110 1110	.48
TIME	77	9:17:
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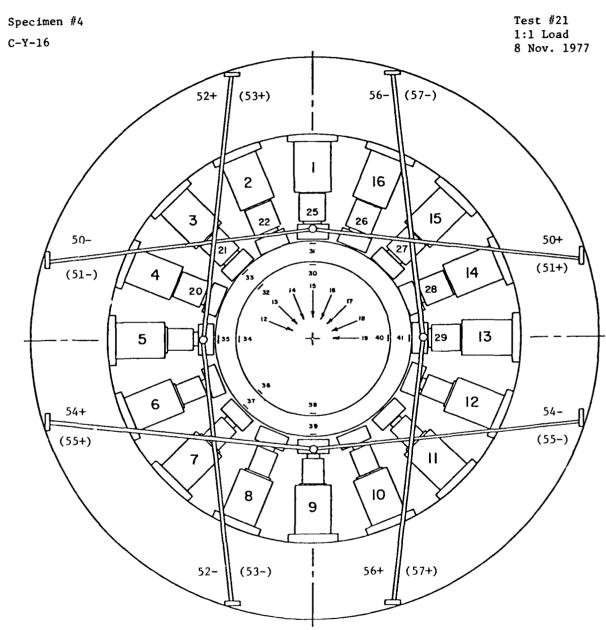
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AXIMUM LOAD CHANNEL, 25 REACHES A MAXIMUM VALUE AT STEP NUMBER 22

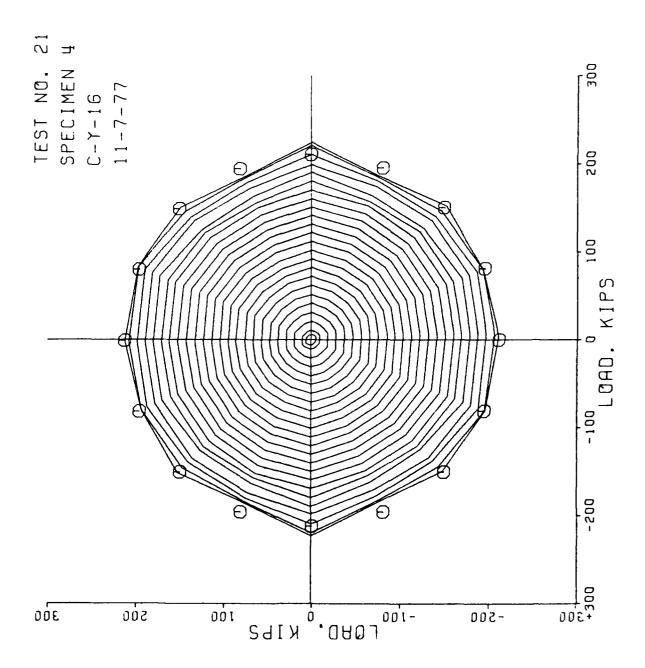
## 3.2.4 RELOAD OF SPECIMEN #4

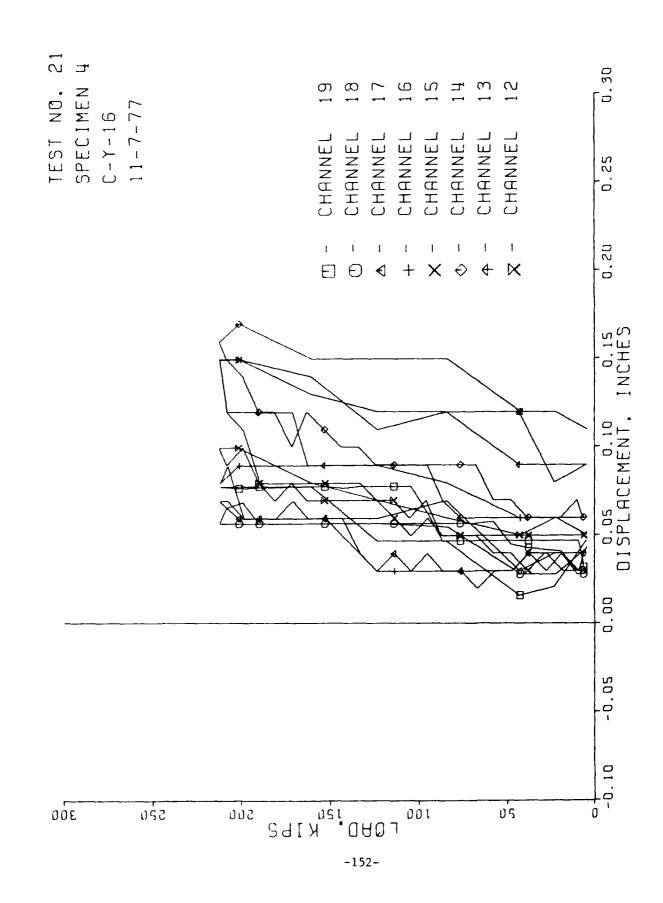
TEST NO. 21
COMPOSITE INTEGRAL LINER
1:1 LOADING RATIO
TESTED 8 NOVEMBER 1977

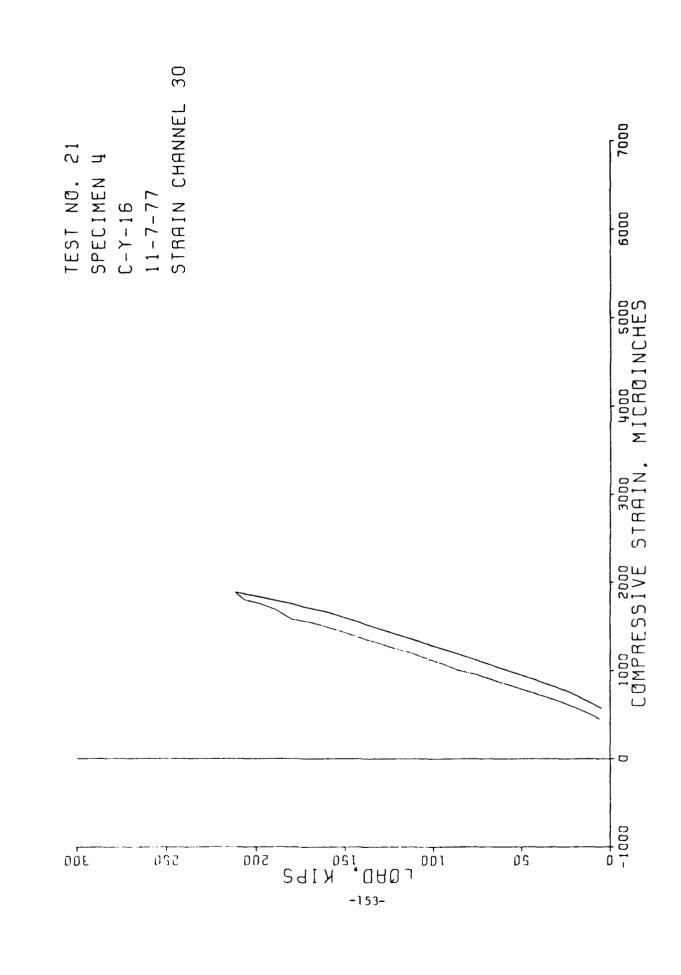
## REACTION FRAME TEST SET-UP

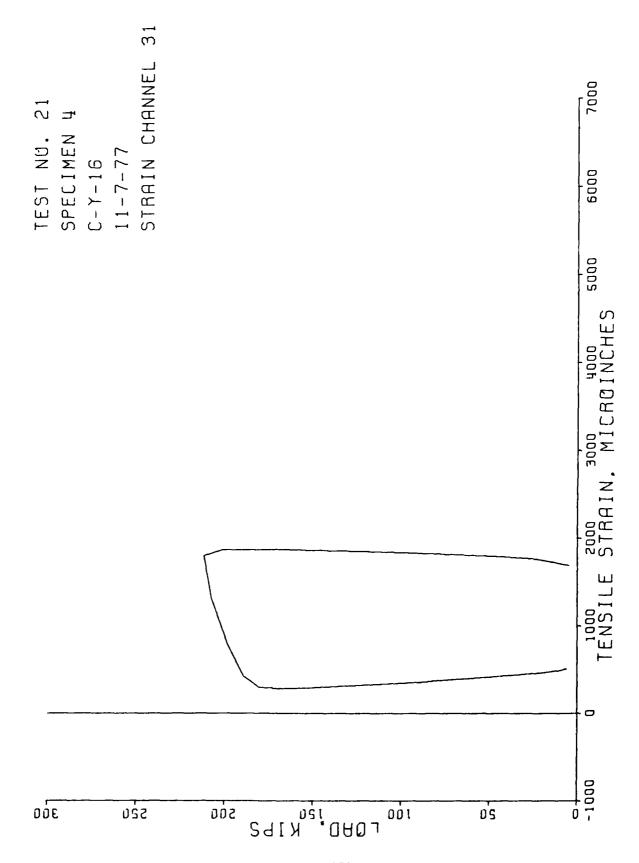


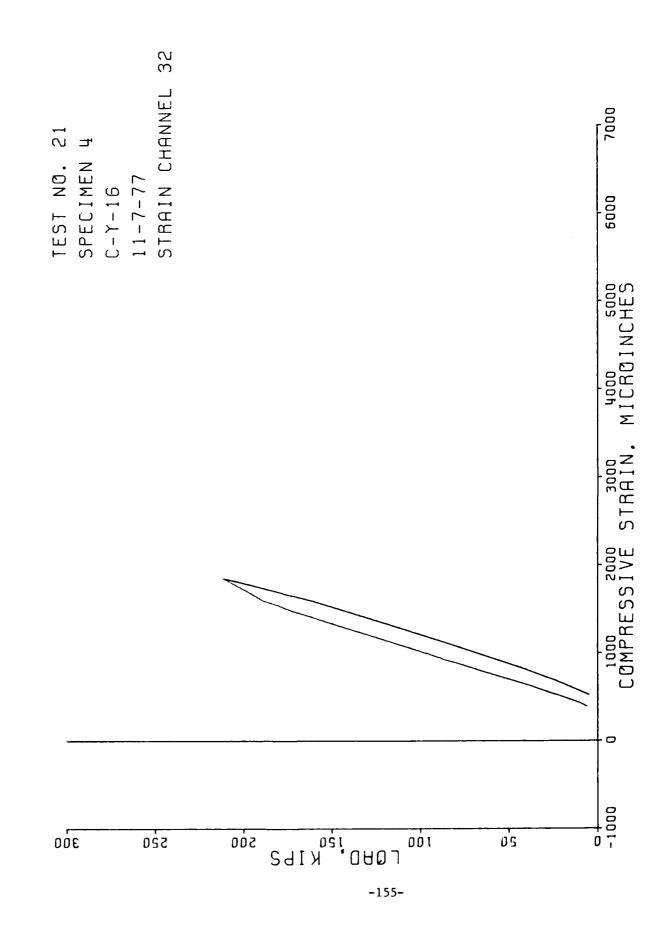
- CH 12-19 Load axis I.D. (Research, Inc. Model 4040).
- CH 20-22, 25-29 Axial load (Transducers, Inc. Model 693-300K).
- CH 30-41 (Ailtech SG 129-6S) Radial pairs 2" from top. Odd gages on Rebar.
- CH 50-57 (Ailtech SG 129-6S) Polarity indicates rod under tension. Lower rod shown (XX).

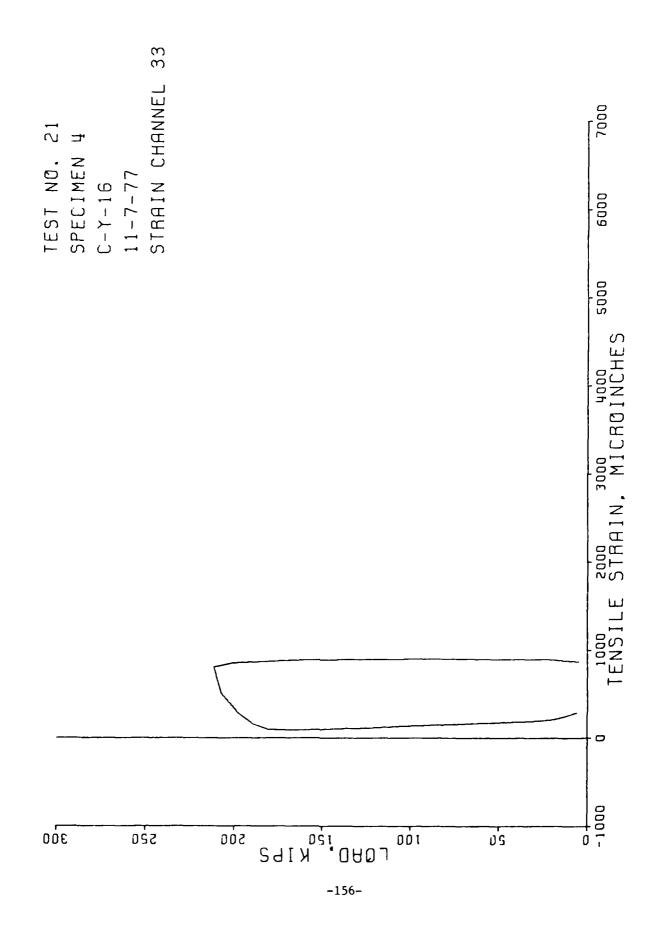


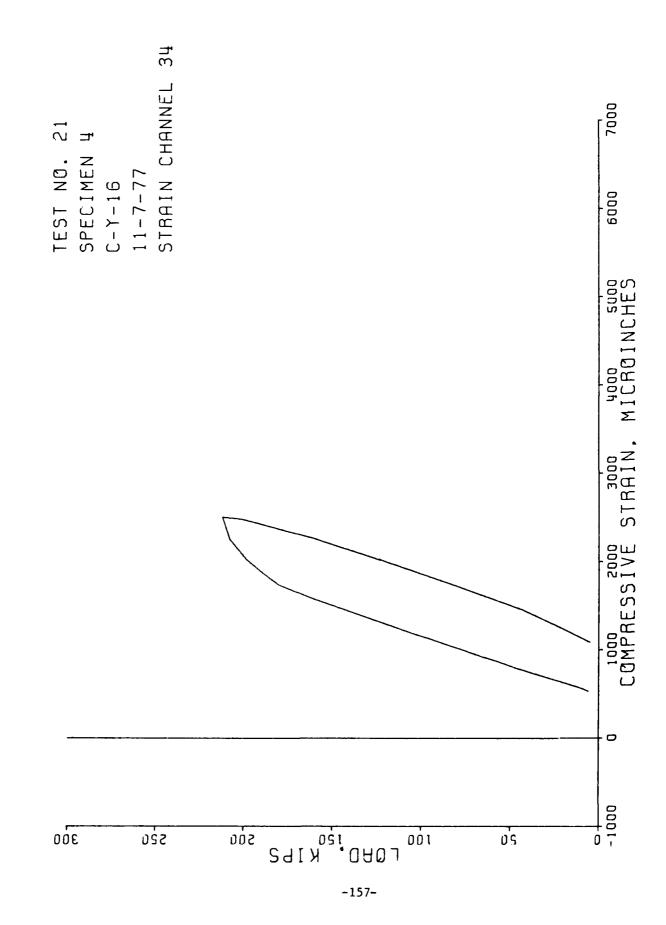


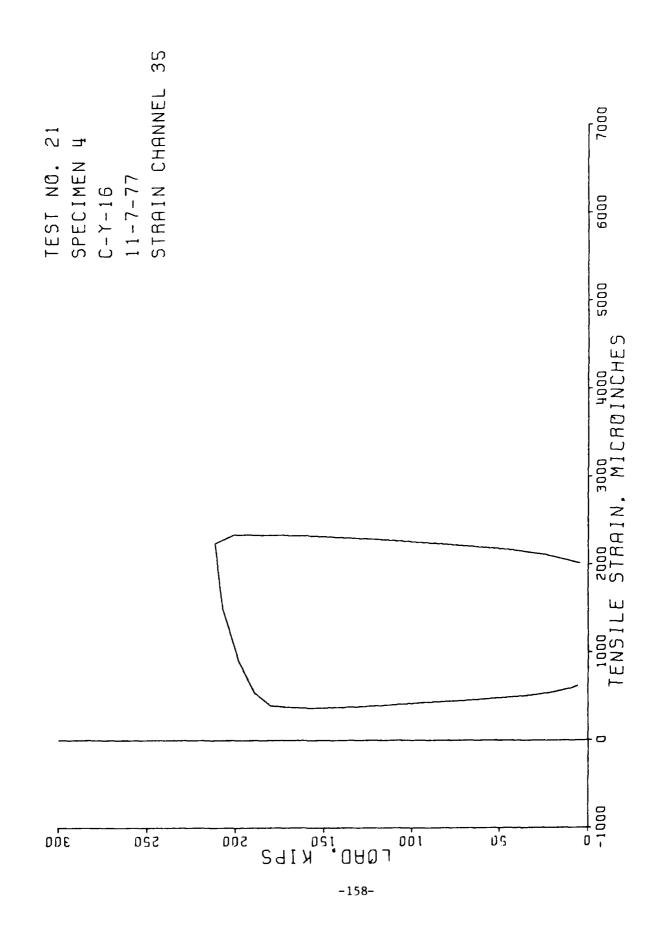


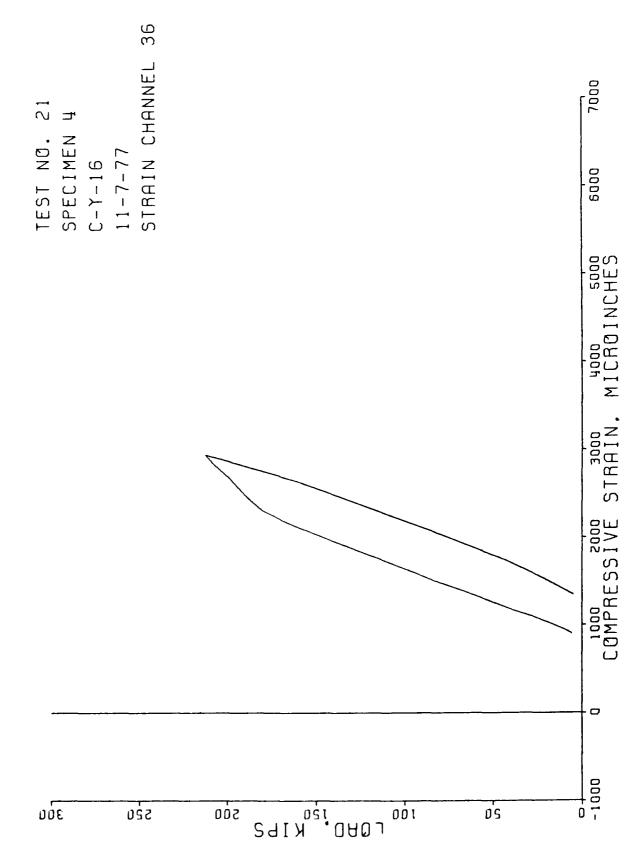


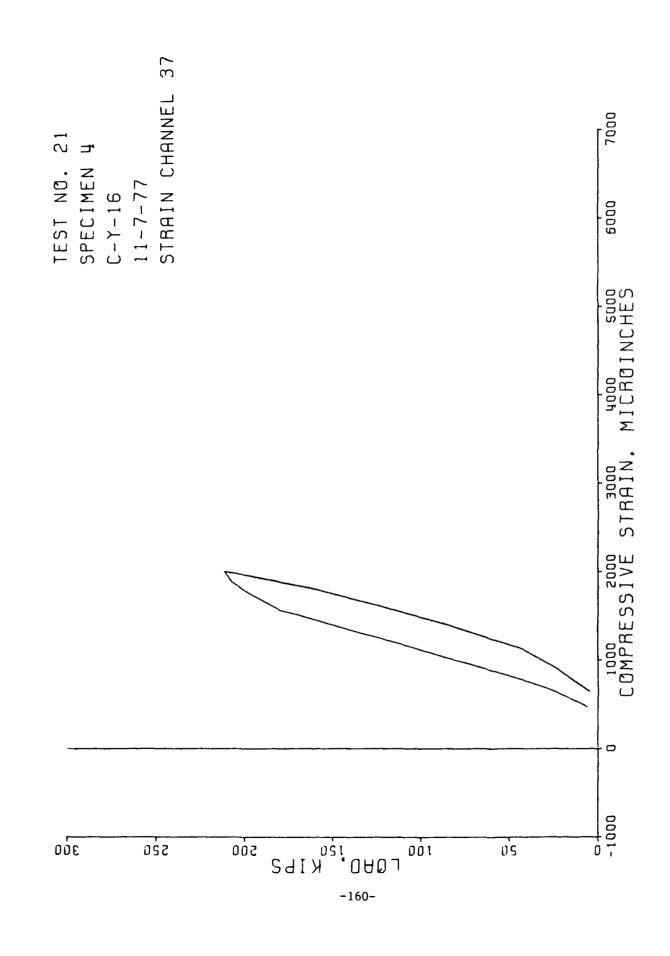


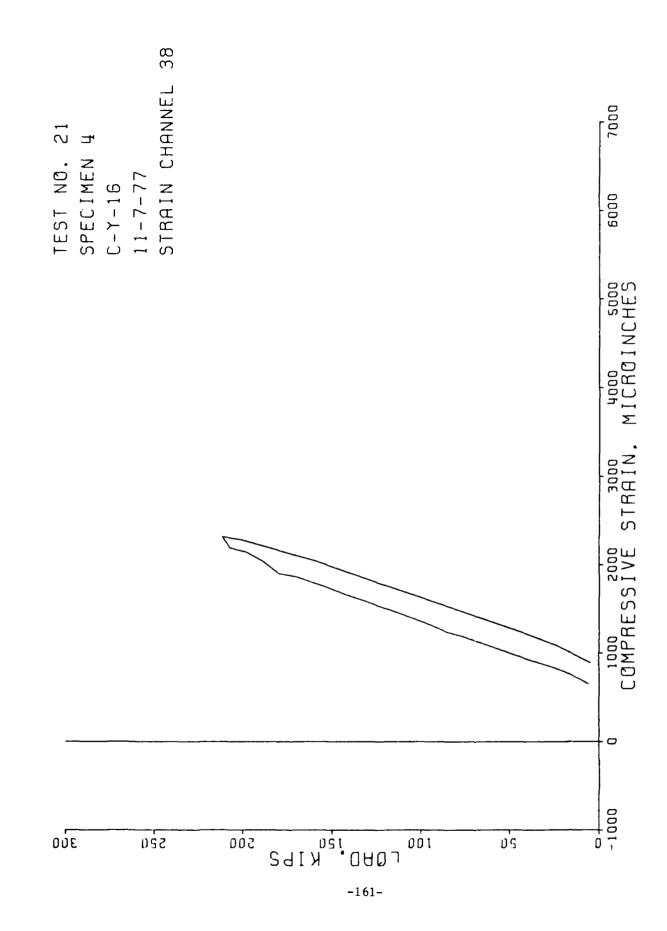


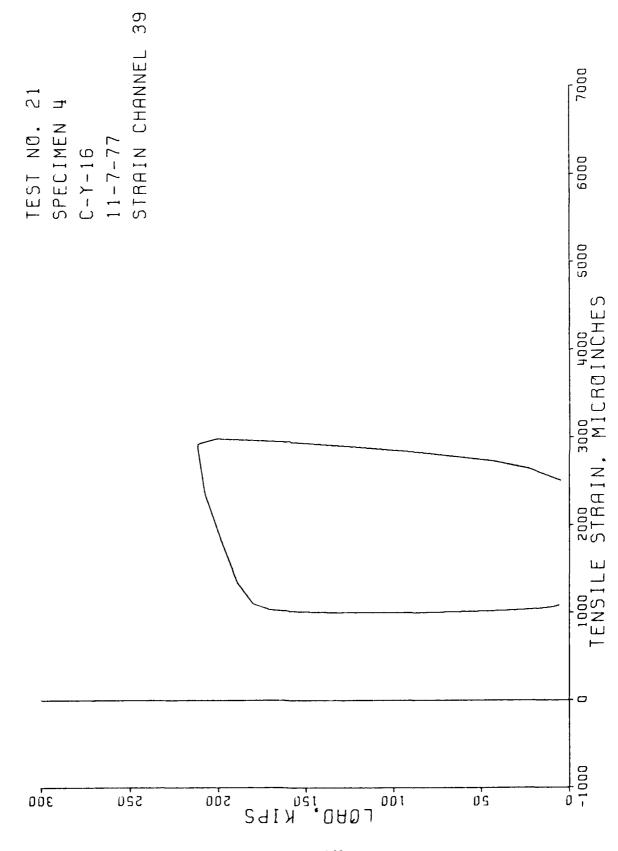


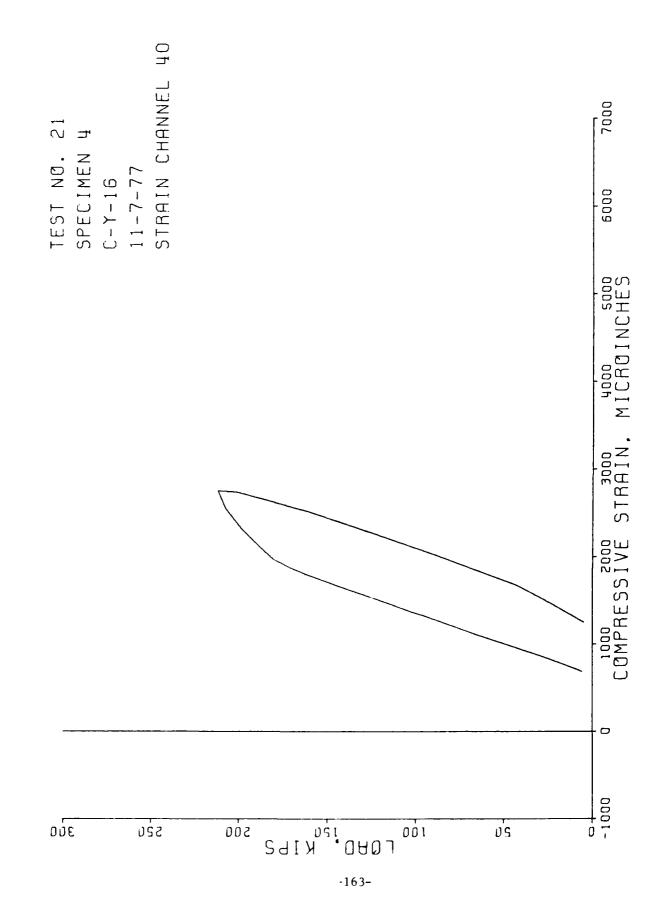


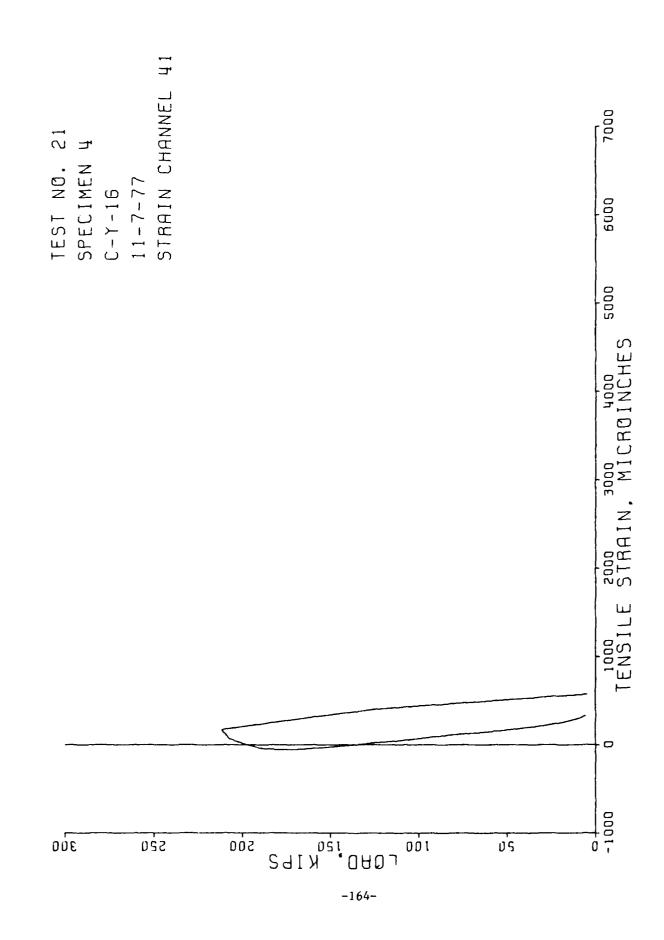












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TEST NO. 2	NUMBER OF NUMBER				

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CH.35	621.000	91.00	48.00	18.00	99.00	83.00	69.00	56.00	45.00	36.00	23.00	09.00	97.00	87.00	77.00	69.00	64.00	64.00	74.00	91.00	37.00	88.00	503.00	235.00	336.00	323.00	286.00	235.00	66.00	106.00	008.00
CH. 36	-898.000	938.00	022.00	095.00	162.00	234.00	310.00	83.00	452.00	525.00	599.00	675.00	749.00	824.00	899.00	976.00	053.00	133.00	208.00	311.00	471.00	668.00	838.00	939.00	882.00	637.00	361.00	065.00	741.00	546.00	343.00
CH.37	-470.000	08.00	93.00	75.00	47.00	07.00	66.00	21.00	976.00	032.00	1086.00	1140.00	195.00	1249.00	1302.00	1355.00	1408.00	1463.00	1513.00	1563.00	1665.00	1765.00	1883.00	2004.00	1971.00	1803.00	1611.00	1397.00	29.00	904.00	652.00
CH. 38	-651.000	90.06	783.00	854.00	14.00	979.00	048.00	1118.00	185.00	1244.00	320.00	392.00	1462.00	530.00	1600.00	1667.00	1738.00	807.00	1865.00	1898.00	041.00	2139.00	2192.00	2313.00	2281.00	2046.00	1787.00	1518.00	233.00	1080.00	890.00
CH.39	1081.000	061.00	041.00	030.00	021.00	015.00	008.00	00.400	000.000	5.00	4.00	3.00	3.00	3.00	5.00	9.00	005.00	015.00	032.00	102.00	346.00	813.00	356.00	918.00	985.00	945.00	890.00	823.00	2.00	646.00	505.00
CH.40	-683.000	7.00	5.00	3.00	9.00	3.00	1052.00	7.00	1185.00	1260.00	1319.00	1381.00	1449.00	1519.00	1584.00	1655.00	1724.00	1796.00	1867.00	1961.00	2123.00	2305.00	2541.00	2745.00	2732.00	2503.00	2255.00	1979.00	1673.00	1458.00	1248.00
CH.41	331.000	98.00	54.00	22.00	98.00	76.00	56.00	36.00	18.00	03.00	00.1	00.0	00.1	.000	. 00	14.00	1.00	45.00	53.00	6.00	38.00	5.00	70.00	68.00	06.00	17.00	06.00	62.00	<u>.</u>	50.00	68.00
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MAXIMUM LOAD CHANNEL, 25 REACHES A MAXIMUM VALUE AT STEP NUMBER 24

## 3.2.5 SPECIMEN #3

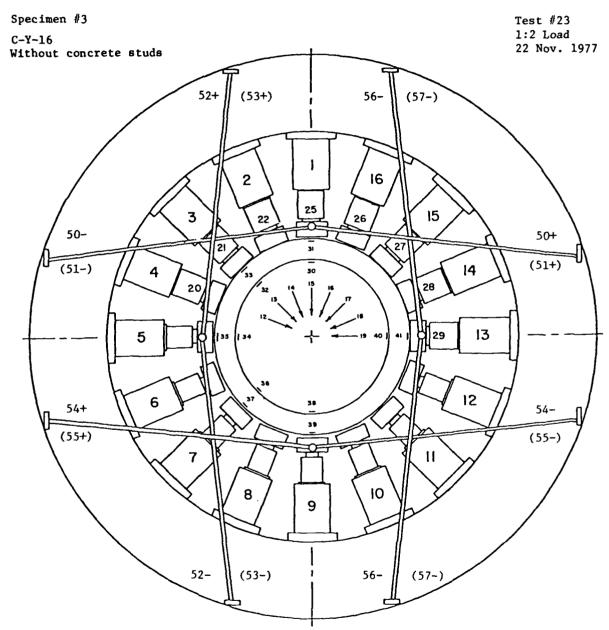
TEST NO. 23

COMPOSITE INTEGRAL LINER WITHOUT CONCRETE STUDS

1:2 LOADING RATIO

TESTED 22 NOVEMBER 1977

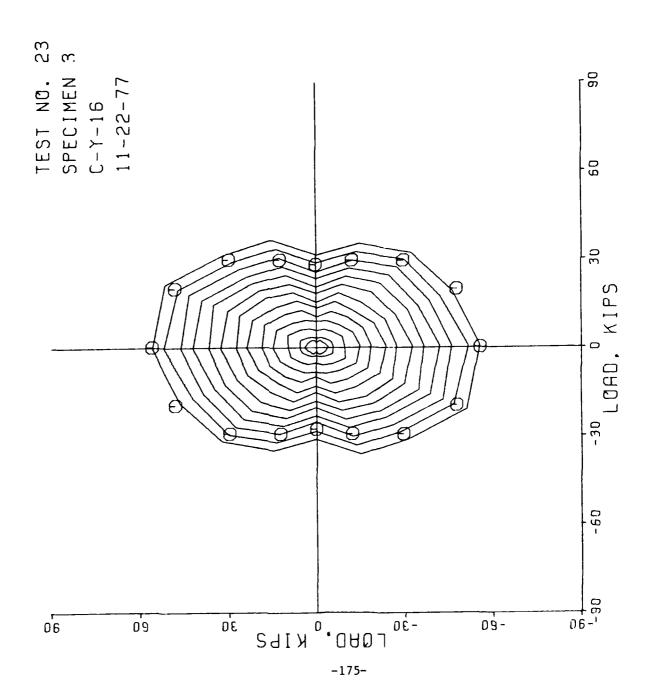
## REACTION FRAME TEST SET-UP

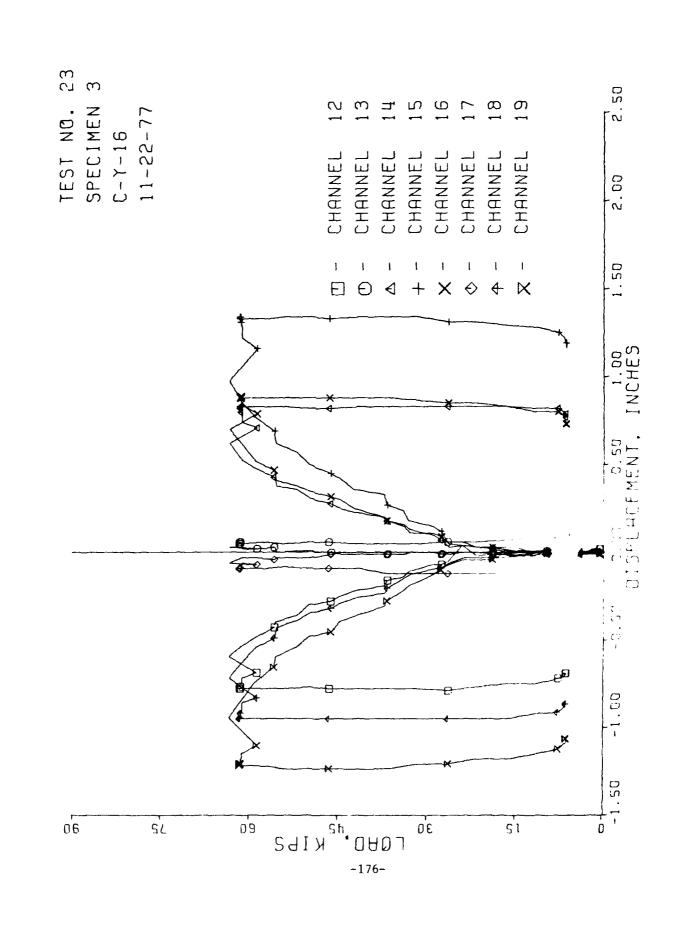


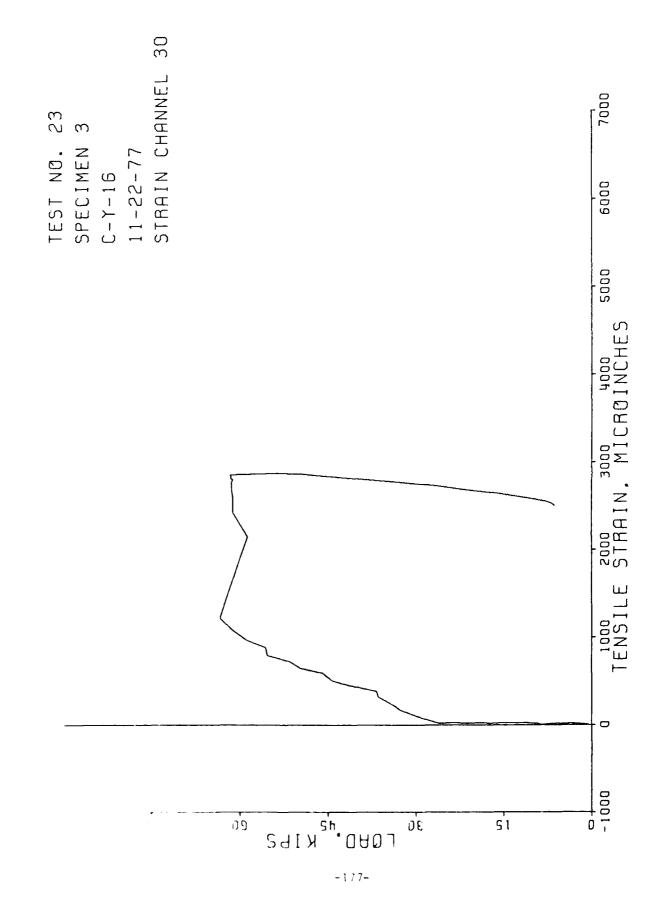
CH 12-19 Load axis I.D. (Research, Inc. Model 4040).

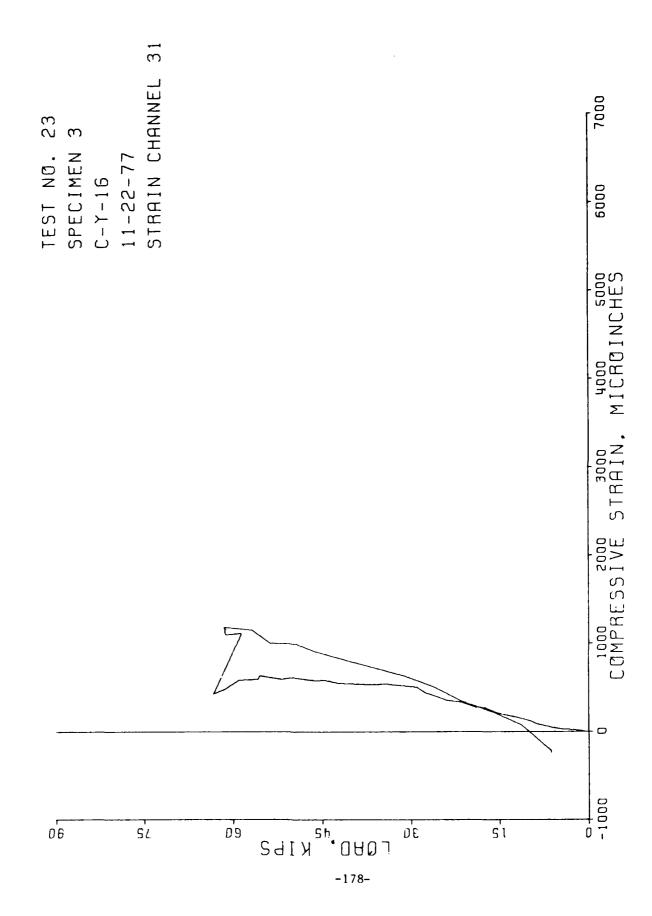
CH 20-22, 25-29 Axial load (Transducers, Inc. Model 693-300K).

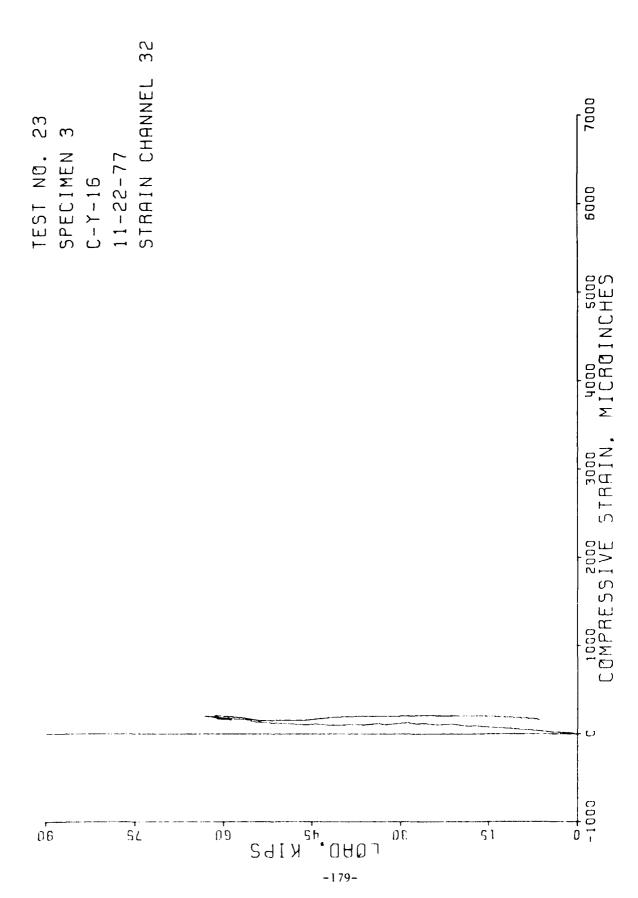
CH 30-41 (Ailtech SG 129-6S) Radial pairs 2" from top. Odd gages on Rebar. CH 50-57 (Ailtech SG 129-6S) Polarity indicates rod under tension. Lower rod shown (XX).

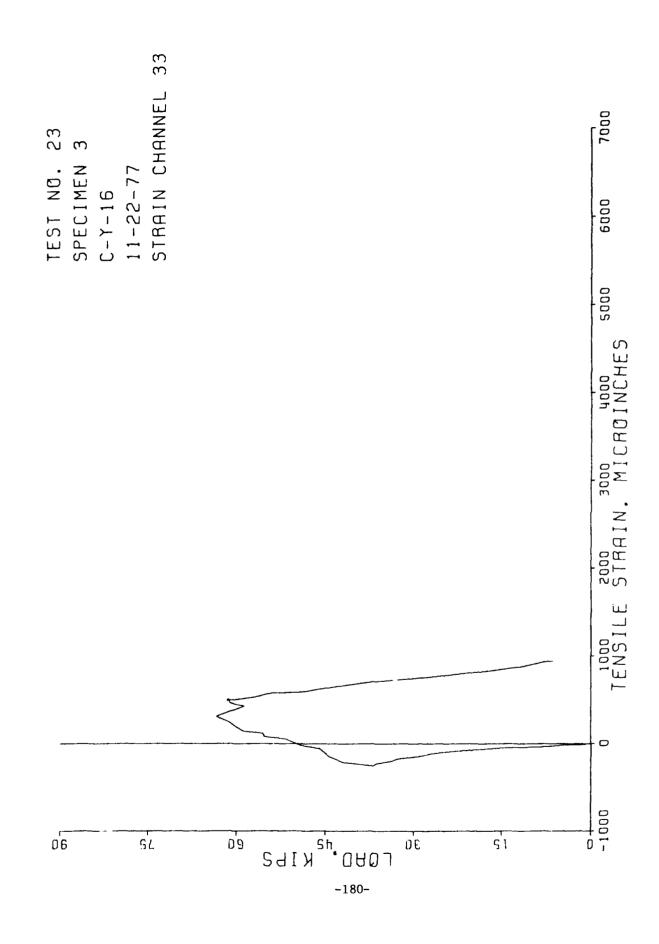


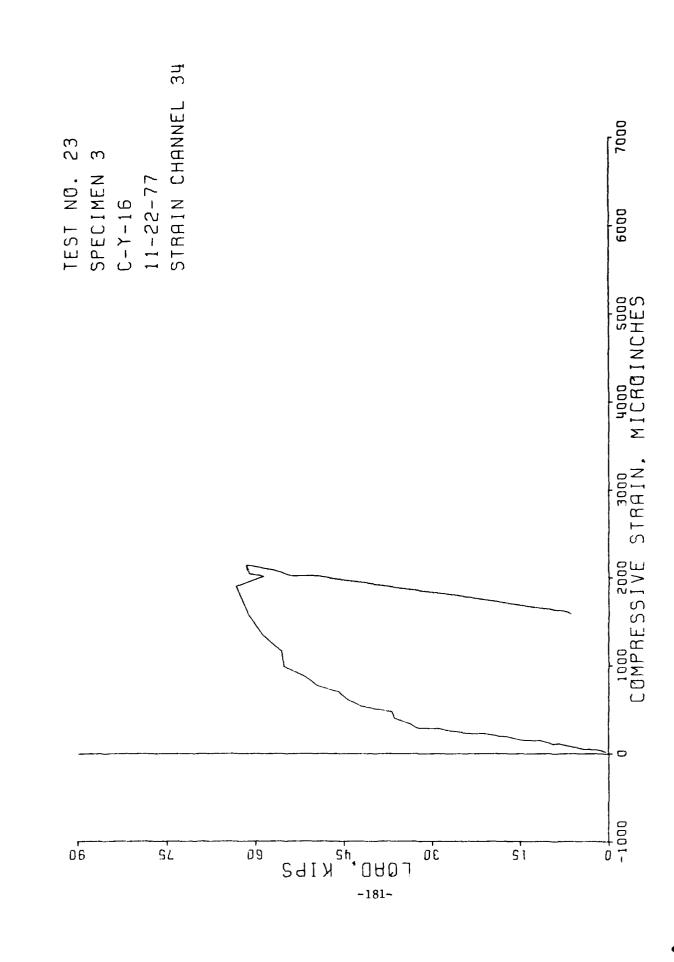


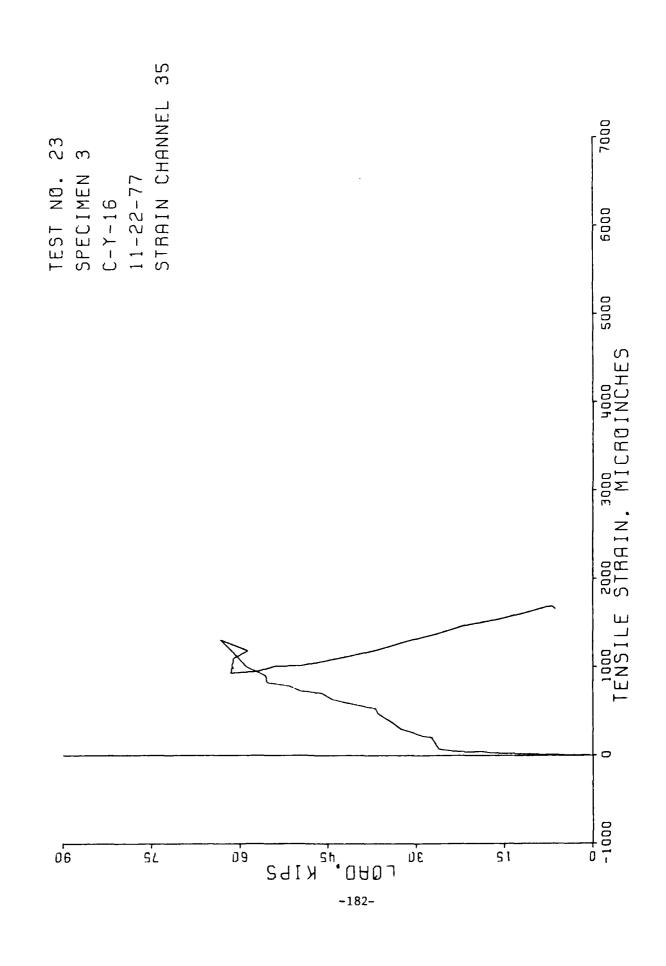


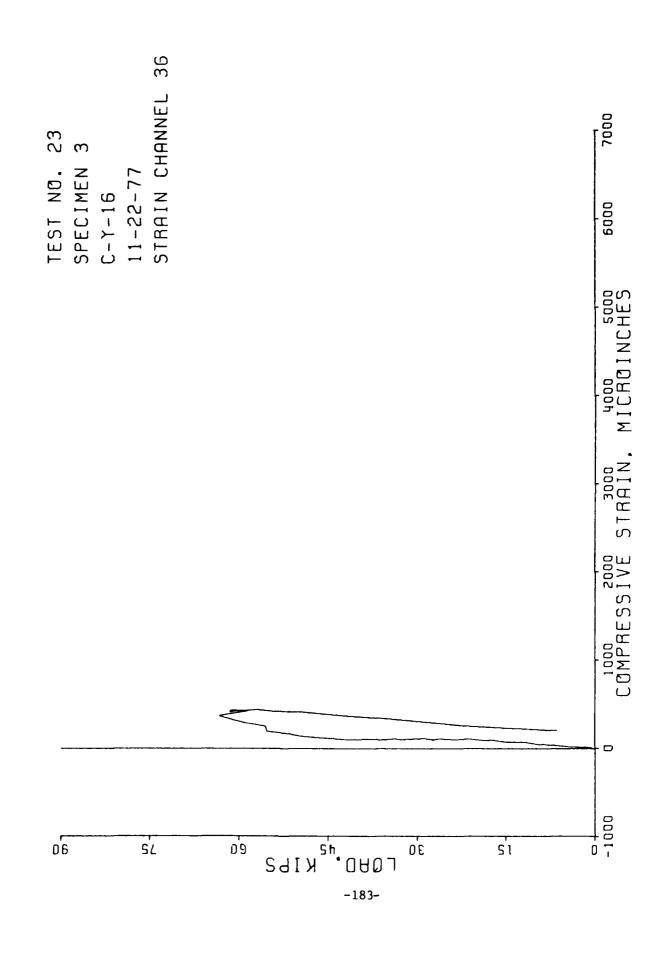


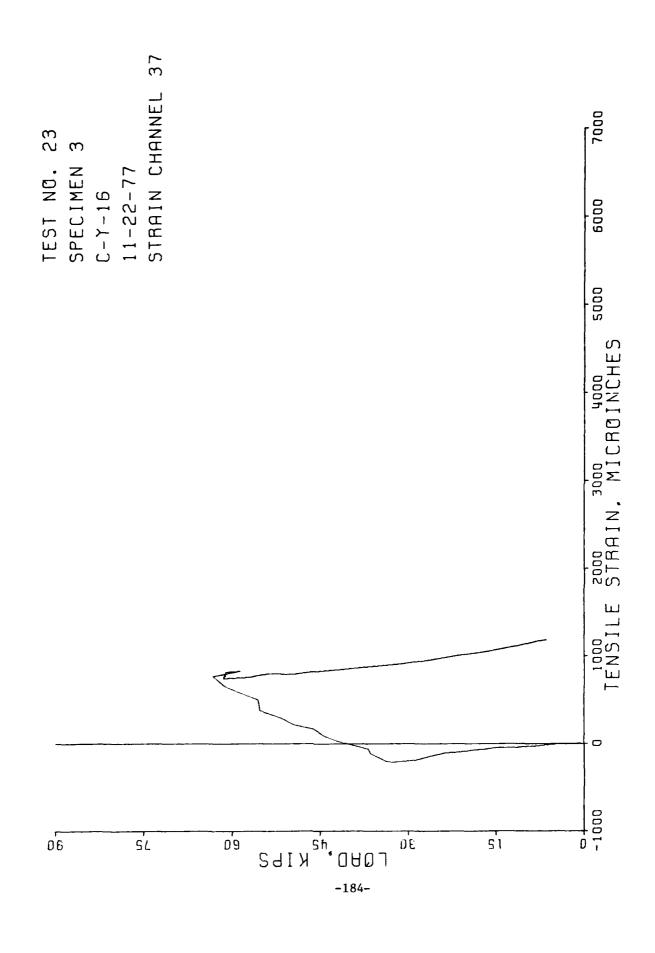


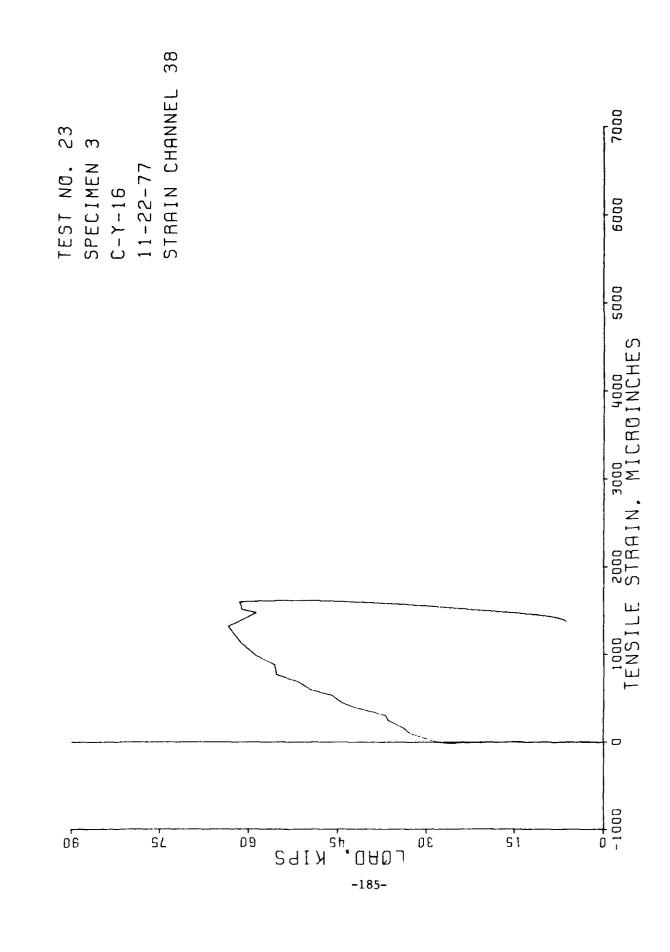


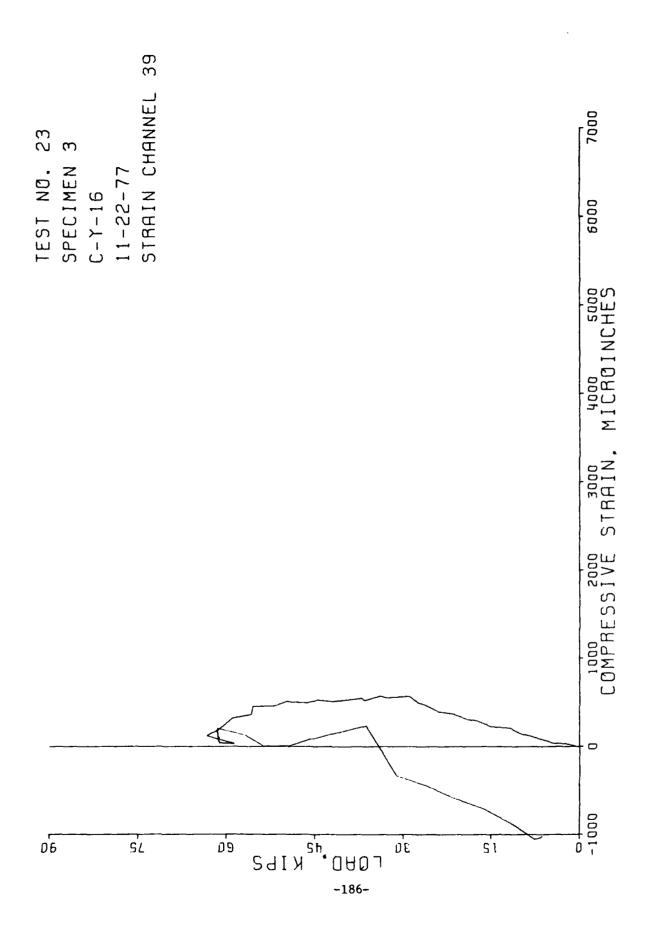


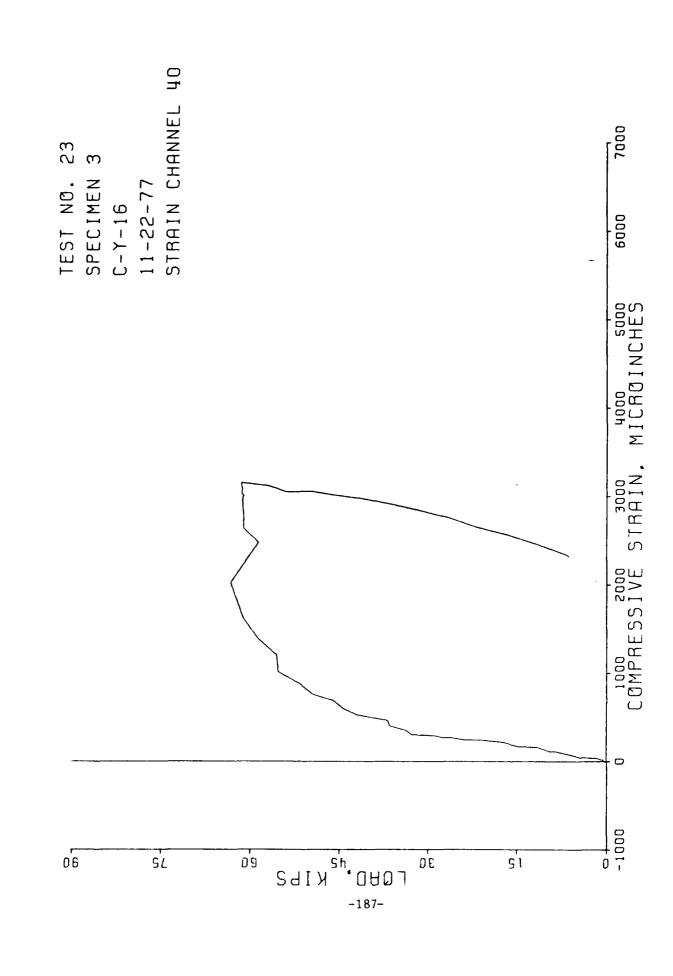


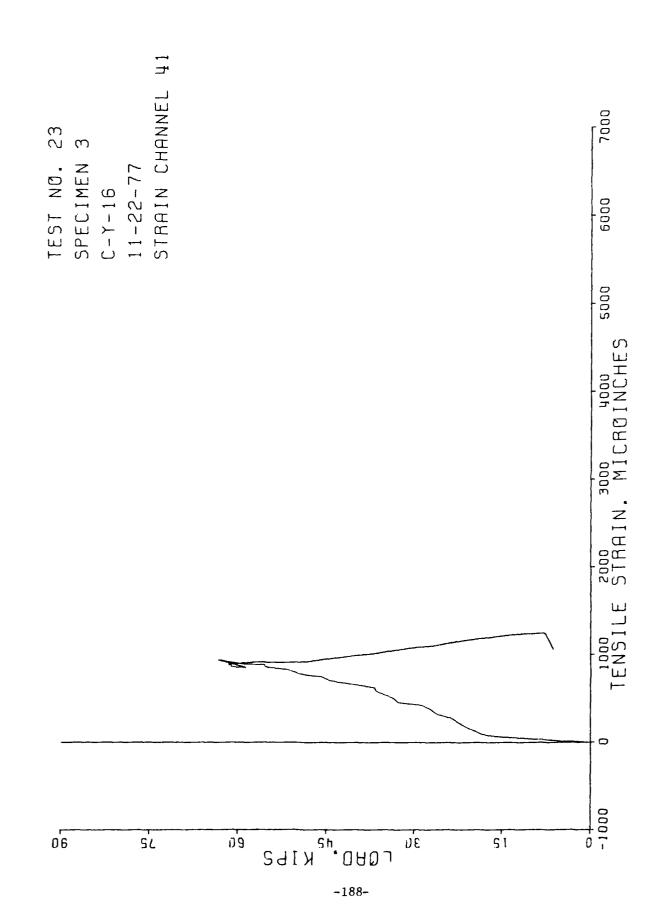






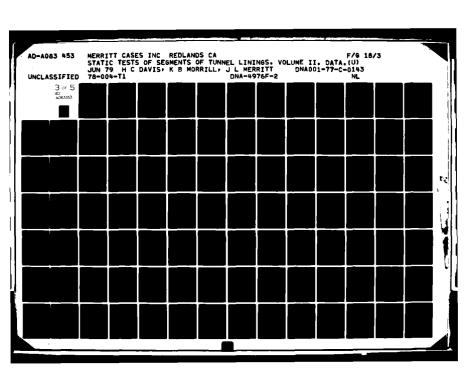






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MAXIMUM LOAD CHANNEL, 25 REACHES A MAXIMUM VALUE AT STEP NUMBER 32

58. 46010.000 60. 38011.250 61. 38011.250 62. 38011.250 63. 2755.000 64. 23792.500 65. 19996.250 66. 15201.250 67. 12201.250 68. 8117.500 69. 5110.000 70. 4462.500 74. 4487.500 75. 4487.500

## 3.3 COMPLIANT LINER 3.3.1 SPECIMEN #10

TEST NO. 25

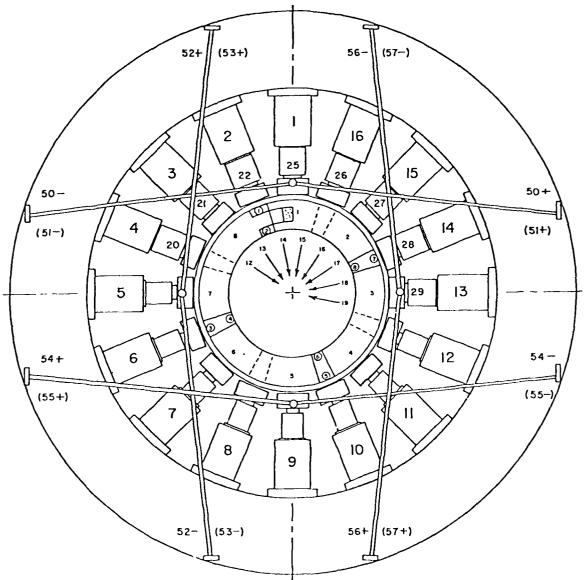
COMPLIANT LINER

1:1 LOADING RATIO

TESTED 15 DECEMBER 1977

## REACTION FRAME TEST SET-UP



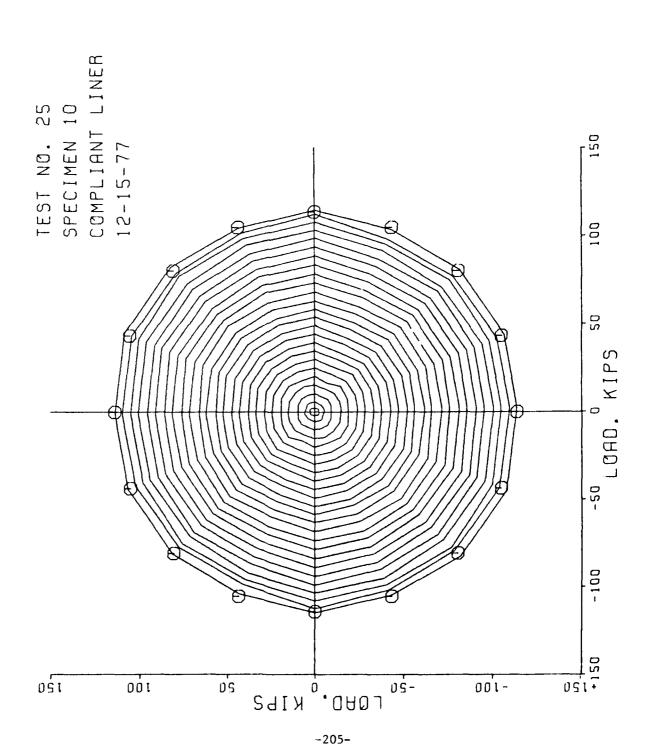


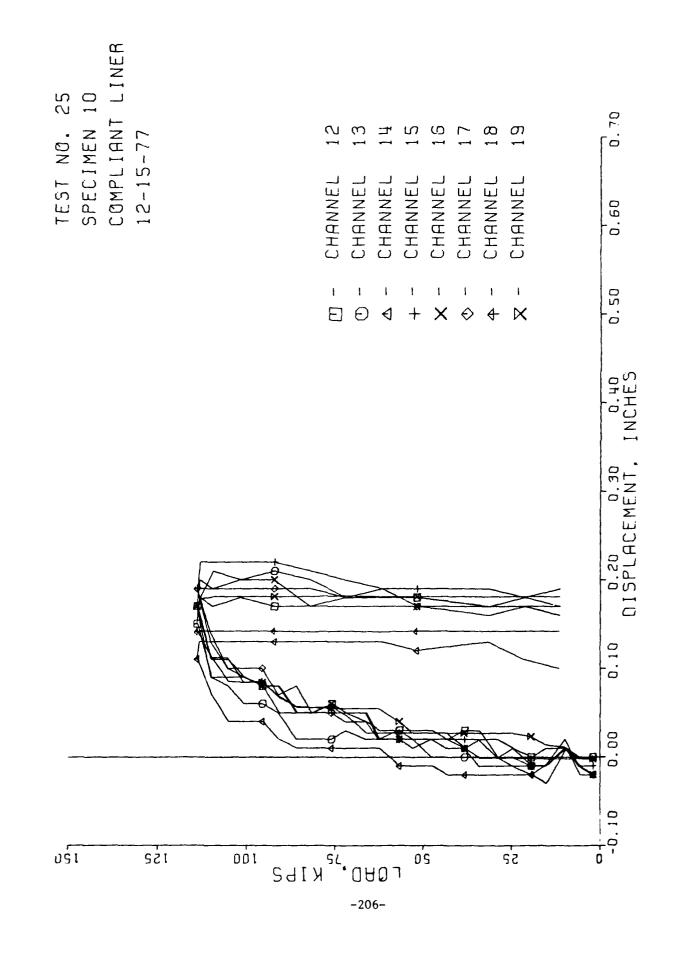
CH 12-19 Load axis I.D. (Research, Inc. Model 4040).

CH 20-22, 25-29 Axial load (Transducers, Inc. Model 693-300K).

CH 50-57 (Ailtech SG 129-6S) Polarity indicates rod under tension. Lower rod shown (XX).

Dial Gages ① - ⑧ measure circumferential gap width at the top.





COMPLIANT LINER 12-15-77	∞	EROSHIFT		CALIBRATION	000000000000000000000000000000000000000	CALIBRATION	110.0000000000000000000000000000000000
TEST NO. 25 ' SPECIMEN 10 COM	NUMBER OF INCREMENTS= 36 NUMBER OF CHANNELS= 24 NUMBER OF STRAIN CHANNELS= NUMBER OF DISPLACEMENT CHANNELS= NUMBER OF LOAD CHANNELS= NUMBER OF PRESSURE CHANNELS= NUMBER OF RODS=	CHANNEL ZER	55 55 55 55 55 55 56 57 56 57 56 57 56 57 56 57 56 57 56 57 58 57 58 57 58 57 58 57 58 57 58 57 58 57 58 57 58 57 58 57 58 57 58 58 58 58 58 58 58 58 58 58 58 58 58	DISPLACEMENT CHANNEL	11111111111111111111111111111111111111	LOAD CHANNEL	29 28 26 25 22 21

10.000 CALIBRATION 1.000 1.000 1.000 1.000 1.000 1.000

20 ROD CHANNEL 57 55 54 53 53 50

CH.19		ΣŢ.
CH.18		<b>-</b>
CH.17	1	. 16
CH.16	00000000000000000000000000000000000000	. 16
CH.15	0.000000000000000000000000000000000000	. 19
CH.14	00000000000000000000000000000000000000	. 10
INELS CH.13	0.000000000000000000000000000000000000	. 17
E N T C H A N CH.12	0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0	. 17
DISPLACEME	1. 15:14 3. 15:14 4. 15:15 6. 15:15 7. 15:15 8. 15:15 10. 15:15 10. 15:15 11. 15:15 11. 15:15 12. 15:15 13. 15:15 14. 15:15 15. 15:15 16. 15:15 17. 15:15 18. 15:15 18. 15:15 19. 15:15 19. 15:15 22. 15:15 23. 15:15 24. 15:15 25. 15:15 26. 15:15 27. 15:15 28. 15:15 28. 15:15 29. 15:15 20. 15	6. 15:16: 7:3

CH.20	1850.00 5200.00 9570.00 4320.00	7580.00 6640.00 1850.00 5820.00	5240.00 0420.00 0460.00 4660.00	89540.000 93830.000 93830.000 103330.000 112270.000 112270.000 11260.000 103470.000	4660.00 4540.00 4530.00 4110.00 3580.00 3200.00
CH.21	2300.00 5370.00 0240.00 5120.00	9880.00 9880.00 9030.00 8460.00	8220 2850 2850 2850 1771 1890 1890 1890 1890	91410.000 97240.000 97240.000 106570.000 106540.000 114390.000 112410.000 102870.000 92090.000	2700.00 3530.00 3410.00 3280.00 3100.00 2180.00
CH.22	2910.00 5380.00 0060.00 5120.00 9770.00	9300.00 9300.00 8620.00 3550.00 3010.00	7550.00 2140.00 2180.00 7450.00	92120 96470 101440 10540 110540 115060 11350 1105010 97030	7040.00 6610.00 6010.00 5200.00 3630.00 2040.00
CH.25	1900.00 5720.00 9440.00 5200.00	8770.00 8770.00 8100.00 3220.00 7430.00	6610.00 2350.00 6050.00 1740.00 1480.00	909/00 95480.000 100660.000 105820.000 113690.000 112590.000 109350.000	1960.00 2030.00 1680.00 1660.00 1310.00 1270.00
CH.26	2970.00 2500.00 2790.00 2790.00	100.000 130.000 170.000 170.000	250.00 250.00 270.00 270.00 250.00	94510.000 98870.000 103900.000 112970.000 117280.000 115080.000 1101090.000	910.00 1020.00 1920.00 1770.00 1630.00 1950.00
CH.27	2780.00 6130.00 0640.00 5400.00	4840.00 9920.00 4510.00	9240.00 9780.00 3900.00 3100.00	93095 98760 102470 102470 111690 111690 1113320 111340 92160	2410.00 3180.00 3240.00 3120.00 3160.00 2990.00
CH.28	2090.00 0260.00 5580.00 9340.00	4650.00 4590.00 8970.00 4090.00	7760.00 7760.00 7550.00 3470.00 7810.00	92880.000 97170.000 106650.000 108900.000 113030.000 118620.000 108690.000	4470.00 4890.00 4720.00 4060.00 3090.00 2510.00
CH.29	5360.00 5680.00 0270.00 5200.00	9890.00 9890.00 9450.00 9240.00	88550 88550 88550 88550 88550 88550 88550 88550 88550 88550	93640.000 93770.000 103730.000 107730.000 114580.000 112270.000 109640.000 94930.000	4770.00 4060.00 3740.00 2940.00 2270.00 2220.00
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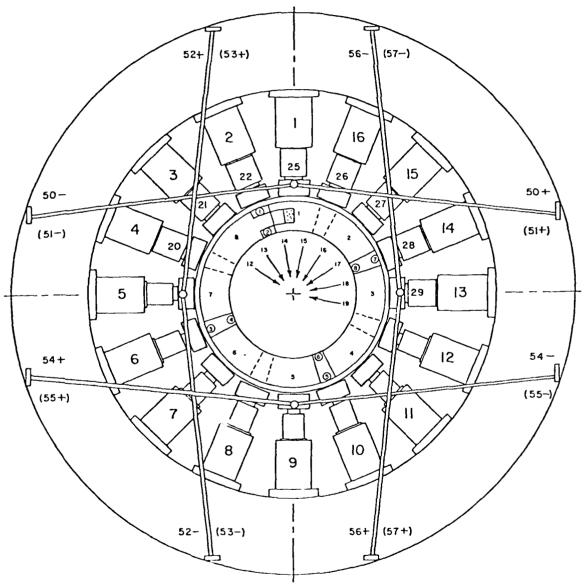
MAXIMUM LOAD CHANNEL, 25 REACHES A MAXIMUM VALUE AT STEP NUMBER 25

## 3.3.2 RELOAD OF SPECIMEN #10

TEST NO. 26
COMPLIANT LINER
1:1 LOADING RATIO
TESTED 19 DECEMBER 1977

## REACTION FRAME TEST SET-UP



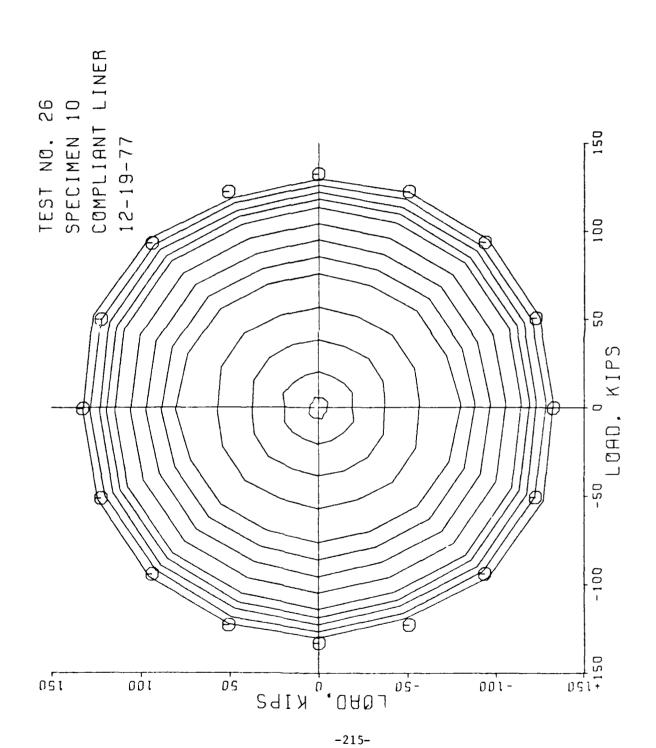


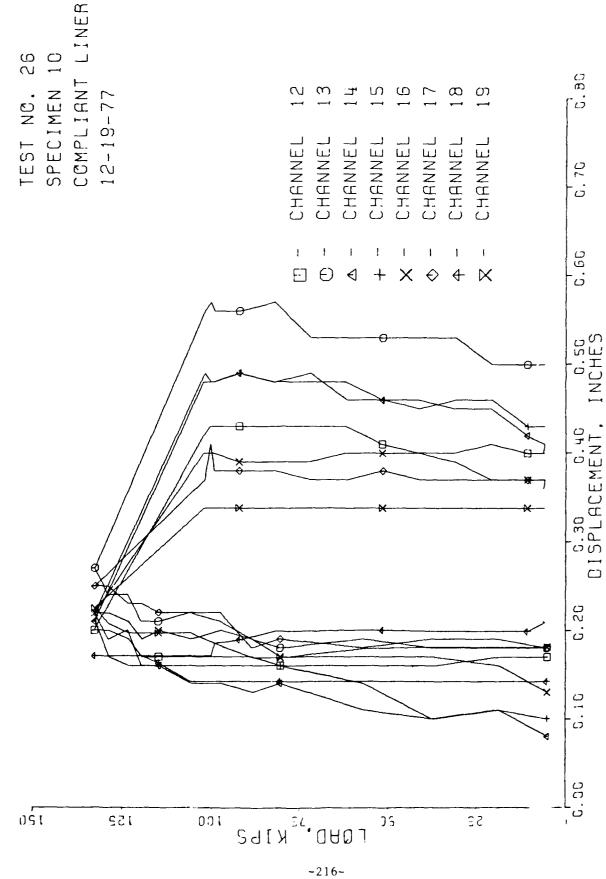
CH 12-19 Load axis I.D. (Research, Inc. Model 4040).

CH 20-22, 25-29 Axial load (Transducers, Inc. Model 693-300K).

CH 50-57 (Ailtech SG 129-6S) Polarity indicates rod under tension. Lower rod shown (XX).

Dial Gages 1 - 8 measure circumferential gap width at the top.





ANT LINER 12-19-77		IFT		CALIBRATION	000000000000000000000000000000000000000	CALIBRATION	000000000000000000000000000000000000000
COMPLIANT	ω ο	ZER0SH]					
EST NO. 26 SPECIMEN 10	UMBER OF INCREMENTS= 27 UMBER OF CHANNELS= 24 UMBER OF STRAIN CHANNELS= 0 UMBER OF DISPLACEMENT CHANNEL UMBER OF PRESSURE CHANNELS= UMBER OF RESSURE CHANNELS= UMBER OF RODS= 8	CHANNEL	55 50 50 50 50 50 50 50 50 50 50 50 50 5	DISPLACEMENT CHANNEL	112 114 116 118	LOAD CHANNEL	22 22 22 1

-218-

CH.19				www
CH.18	~~~		0.171 0.171 0.171 0.185 0.188 0.200 0.199	~00
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СН.14	80.1.1	46444	00000000000000000000000000000000000000	42.4.
CH.13	88.5.	222223	00000000000000000000000000000000000000	.500
СН.12	71.0		00000000000000000000000000000000000000	444
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CH.20	6170 52820 52820 52820 645850 645850 645860 645860 64580 64580 64580 64580 64580 64580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580 65580	
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CH.51	0.0	-153.742	-371.542	-435.601	-563.719	-653.402	-755.896	+284.0.4	94	-1037.756	15	-1306.803	0.0	0.0	12.812	25.624	64.059	153.742	269.048	409.978	589.343	884.014	17	1242.744	13	1204.309
CH.52	550.907	1204.309	1332.427	1806.463	1857.711	1960.205	2126.758	2344.559	2408.618	2600.795	2959.525	3536.056	1793.652	1896.146	1960.205	1601.475	1217.121	922.449	704.649	499.660	294.671	102.494	-51.247	-589.343	-1101.814	-1101.814
CH.53	-38,435	2.8	4.05	3.43	4.05	4.05	9.68	5.55	0.61	8.73	2.47	$\sim$	1.02	0.41	7.91	5.07	3.49	2.22	3.76	3.11	5.60	0.91	3.12	8.25	7.07	2.69
CH.54	102 435	.16	9.02	2.76	56 · t	3.06	3.99	5.48	2.10	3.35	3.25	5.78	1786.85	1889.34	2.16	1633.10	1248.75	0761.91	0223.81	9634.46	3.25	8.30	4.30	3.18	7.96	5.14
CH.55	192.177	i o	409.2	601.4	844.8	9.866	152.3	293.3	318.9	357.3	395.8	σ.	815.1	904.8	930.5	738.3	430.8	033.6	585.2	0.650	457.8	791.6	920.4	754.5	9.866	011.4
CH.56	204.989				050		293	5		813	947		148	392	507	084	559	129	675	219	740	176	497	408	619	639
CH. 57	153.742	35	.77	.59	.27	.95	.82	012.13	.81	191.49	268.36	.67	9365.42	9749.77	929.14	9467.91	8904.19	353.28	7763.94	7123.35	6431.52	5675.62	4791.60	3318.25	254.87	2229.25
TIME	9: 9:	9: 9:11:2	9: 9:13:1	9: 9:15:	9: 9:16:5	9: 9:18:4	9: 9:20:3	9: 9:23:5	9: 9:25:3	9: 9:28:5	9: 9:32:1	9: 9:35:4	9: 9:38:2	9: 9:41:	8: 9:44:2	9: 9:46:1	9: 9:48:	9:65:6 :6	9: 9:51:3	9: 9:53:3	9: 9:55:1	9: 9:56:2	9: 9:58:	9: 9:59:3	9:9:1:1	9: 9: 3:

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NUMBER 13 STEP REACHES A MAXIMUM VALUE AT 25 LOAD CHANNEL, MAXIMUM 3.4 C-X-9 MODELS 3.4.1 SPECIMEN #5

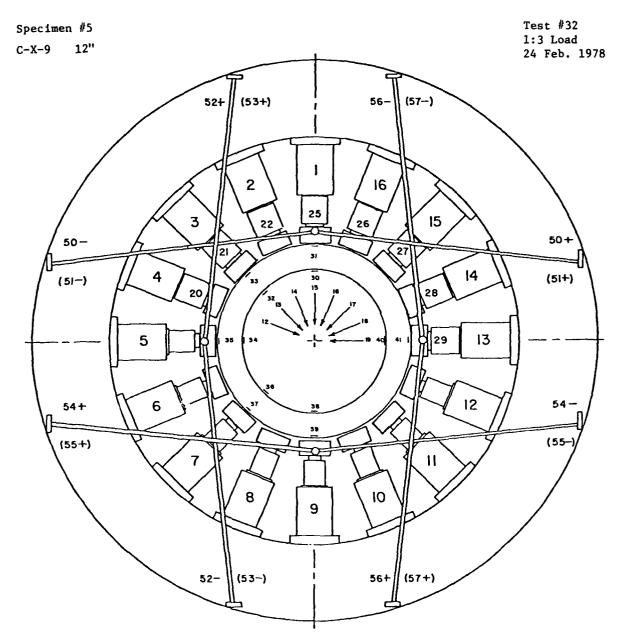
TEST NO. 32

COMPOSITE INTEGRAL LINER

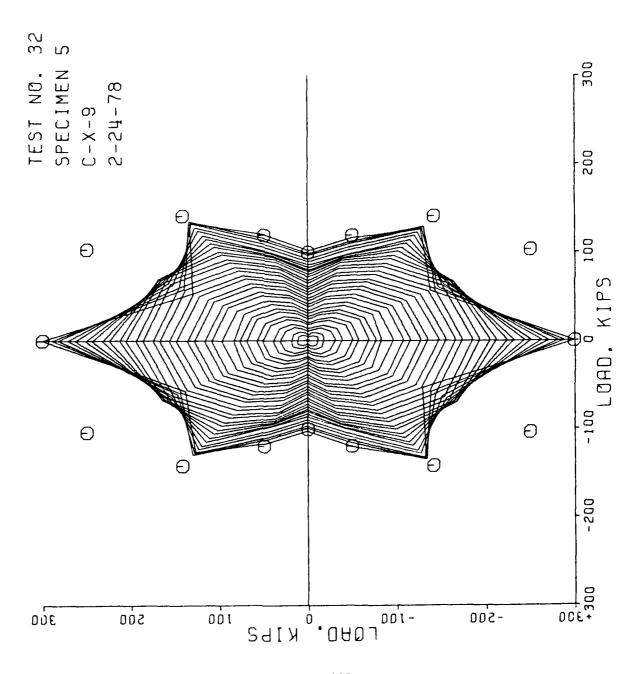
1:3 LOADING RATIO

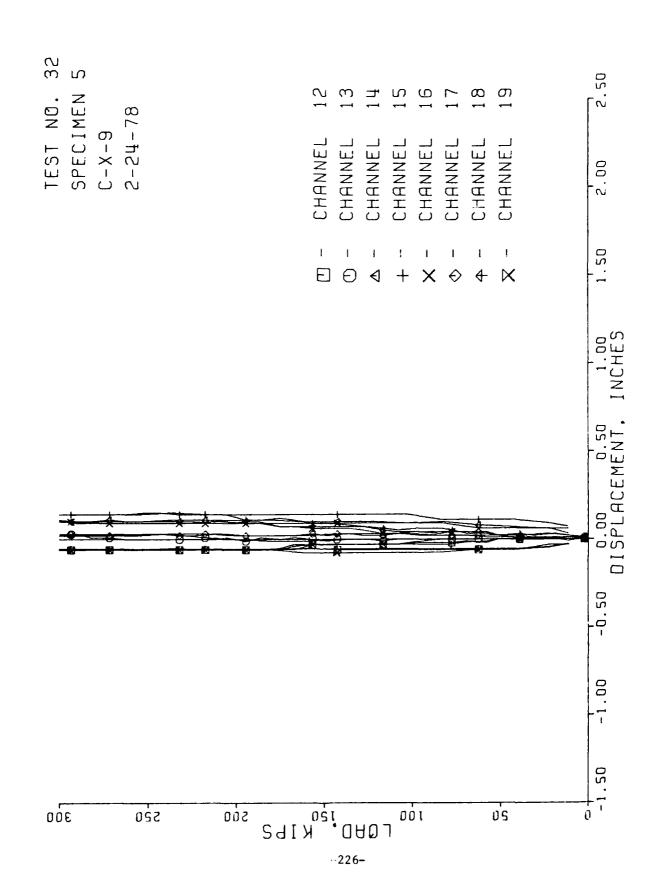
TESTED 24 FEBRUARY 1978

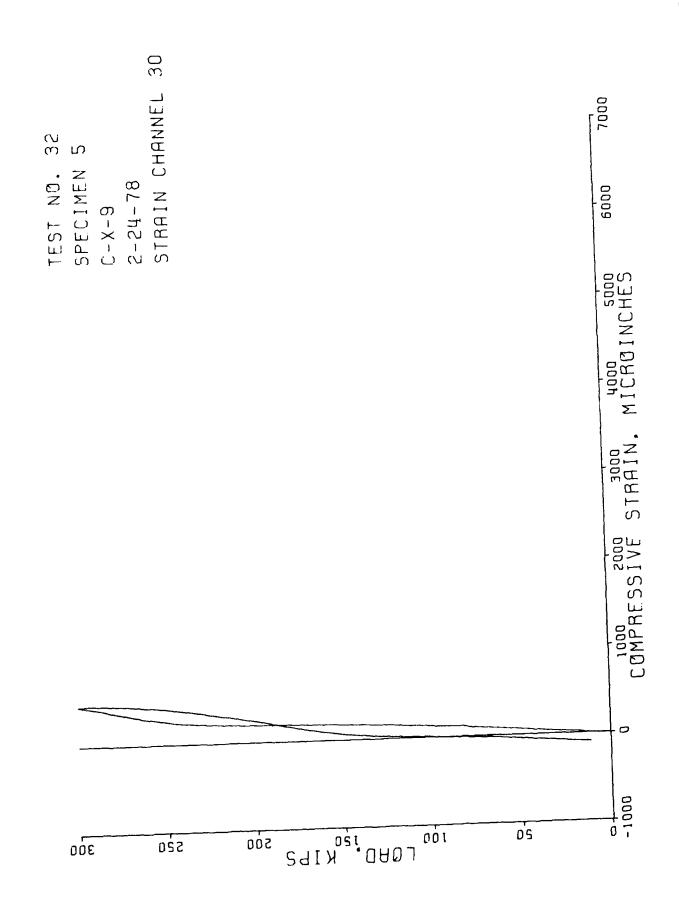
## REACTION FRAME TEST SET-UP

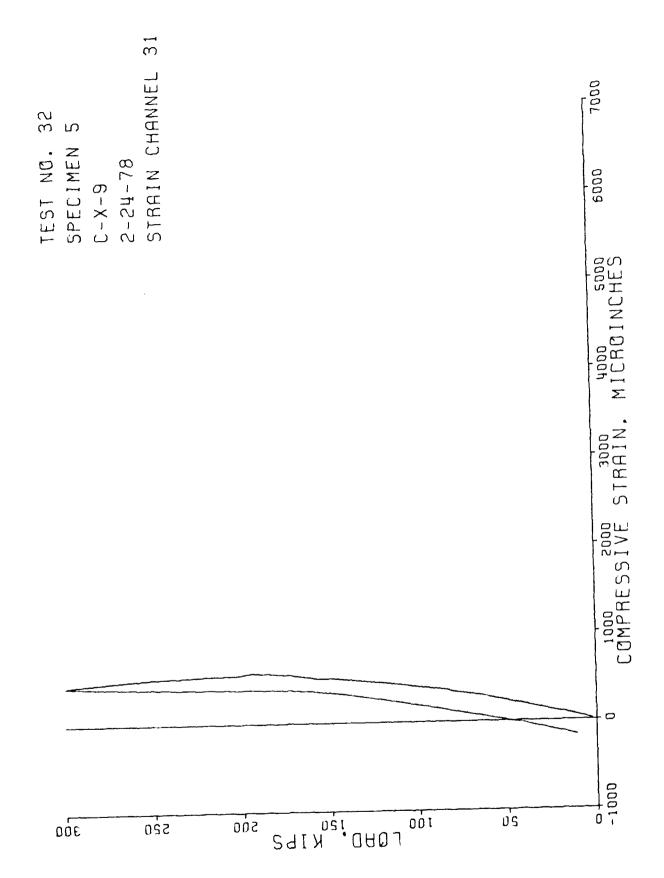


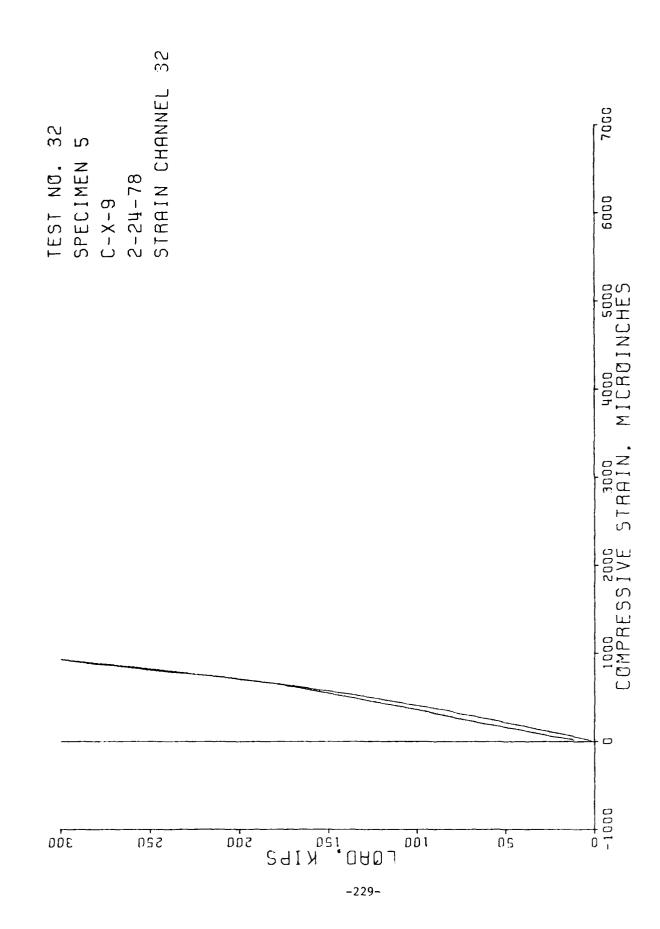
- CH 12-19 Load axis I.D. (Research, Inc. Model 4040).
- CH 20-22, 25-29 Axial load (Transducers, Inc. Model 693-300K). CH 30-41 (Ailtech SG 129-6S) Radial pairs 3" from top. Odd gages on Rebar
- CH 50-57 (Ailtech SG 129-6S) Polarity indicates rod under tension. Lower rod shown (XX).

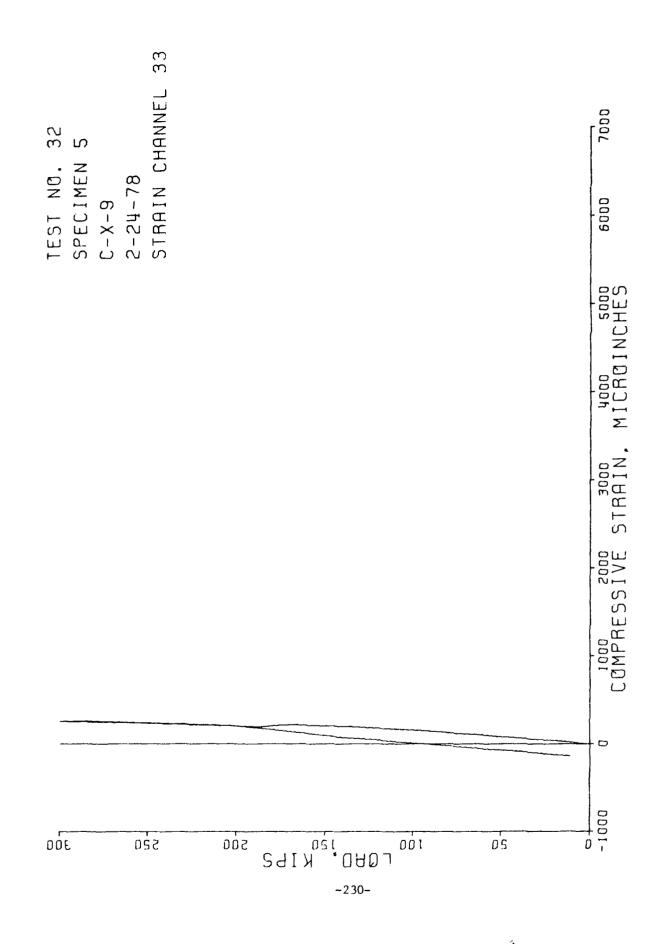


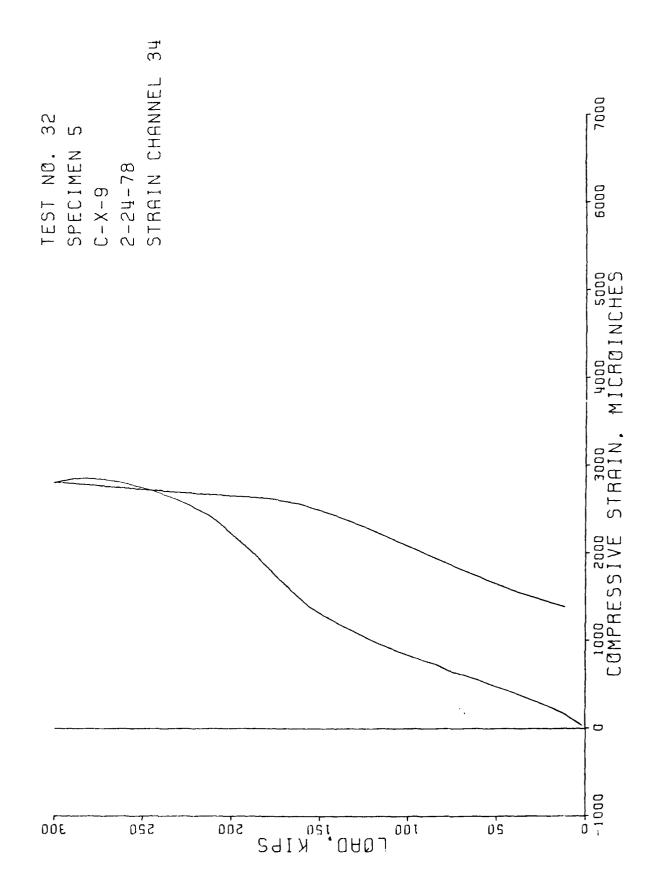


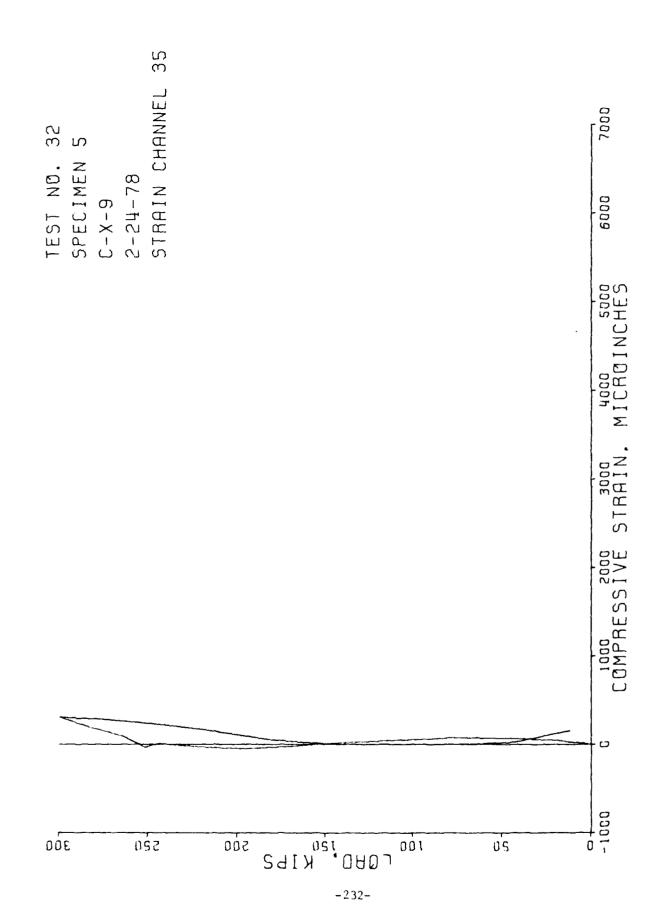


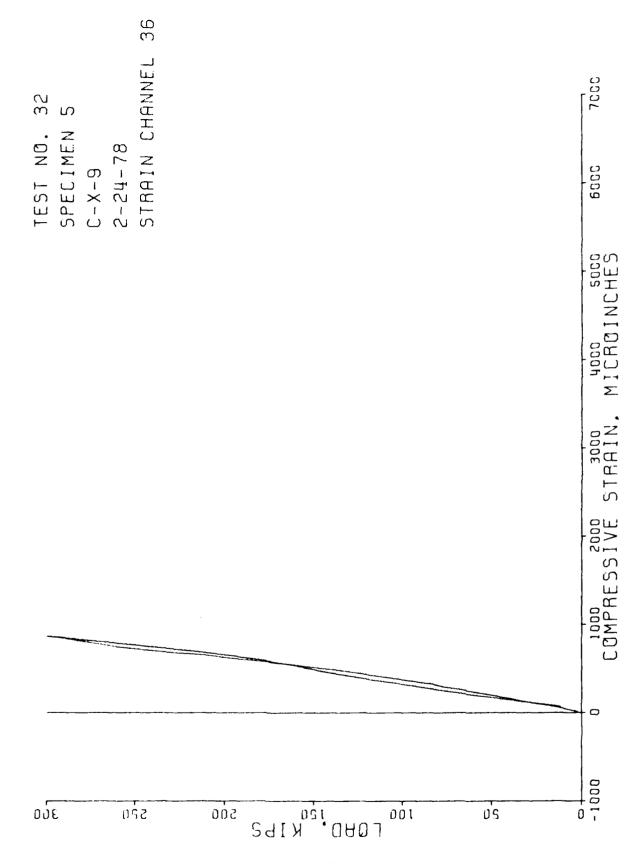


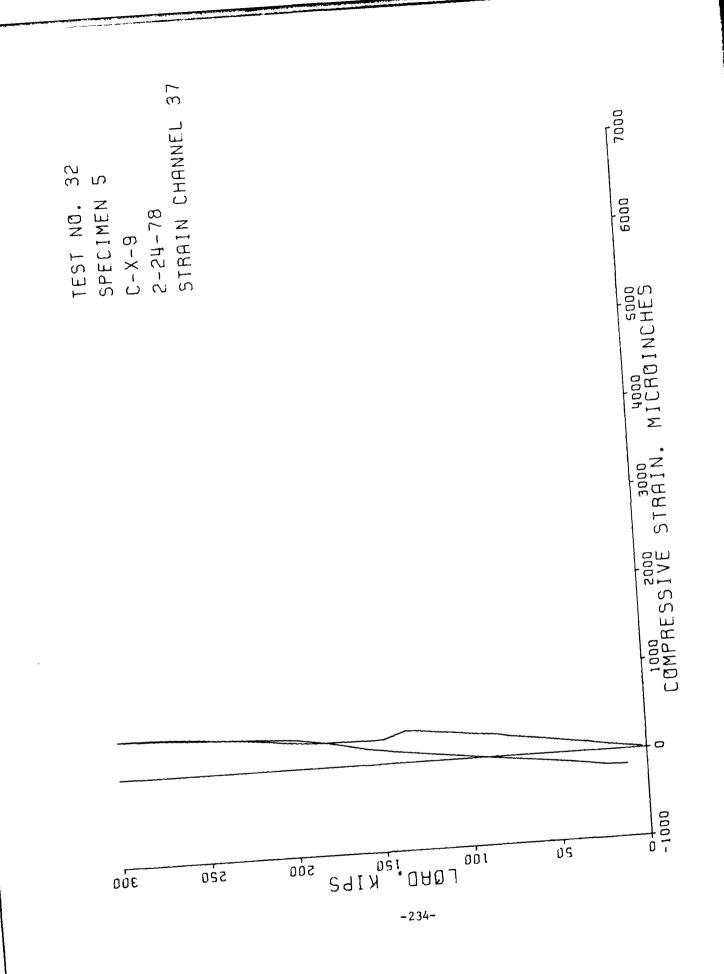


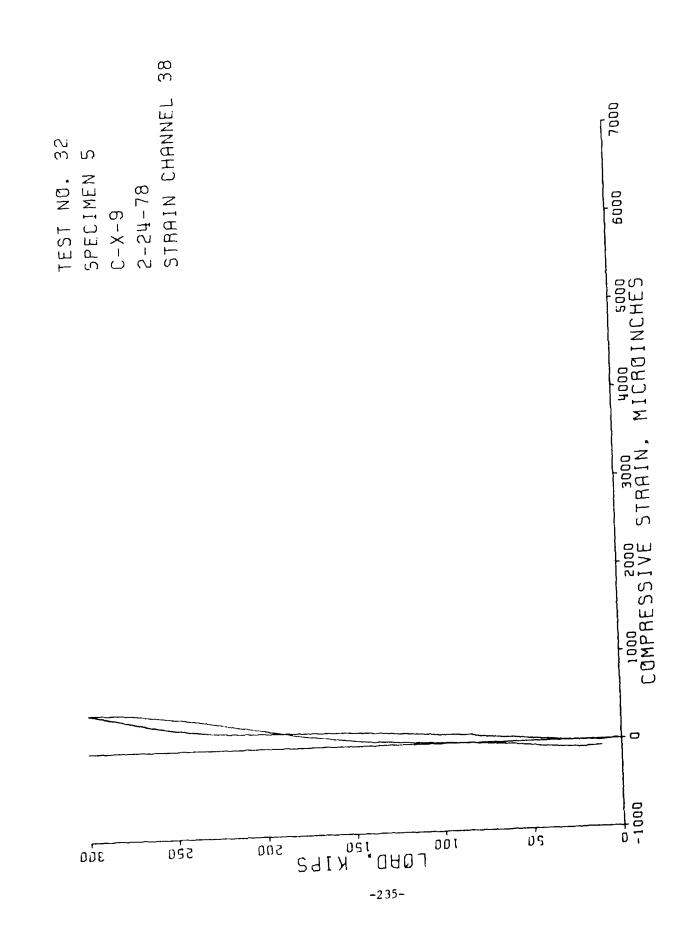


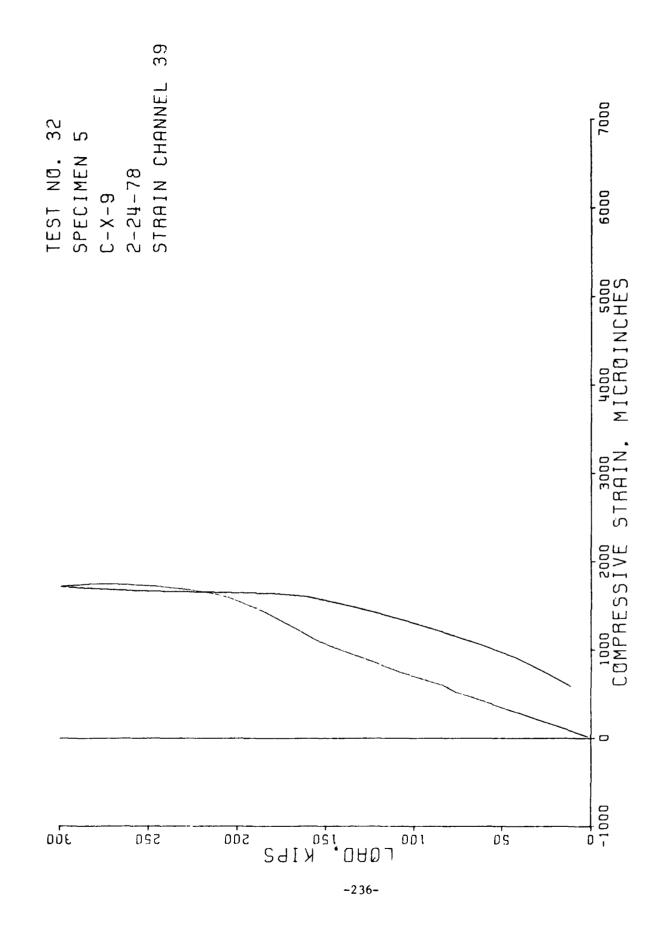


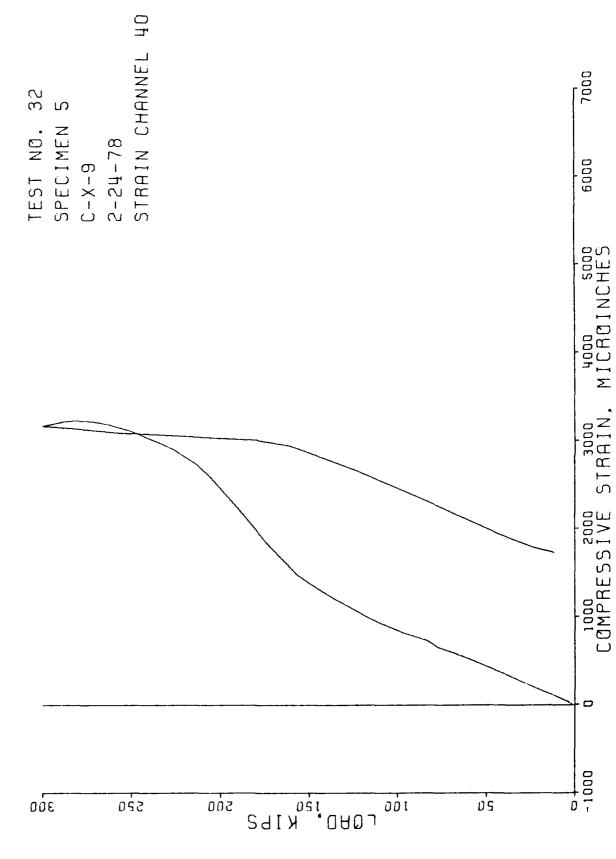


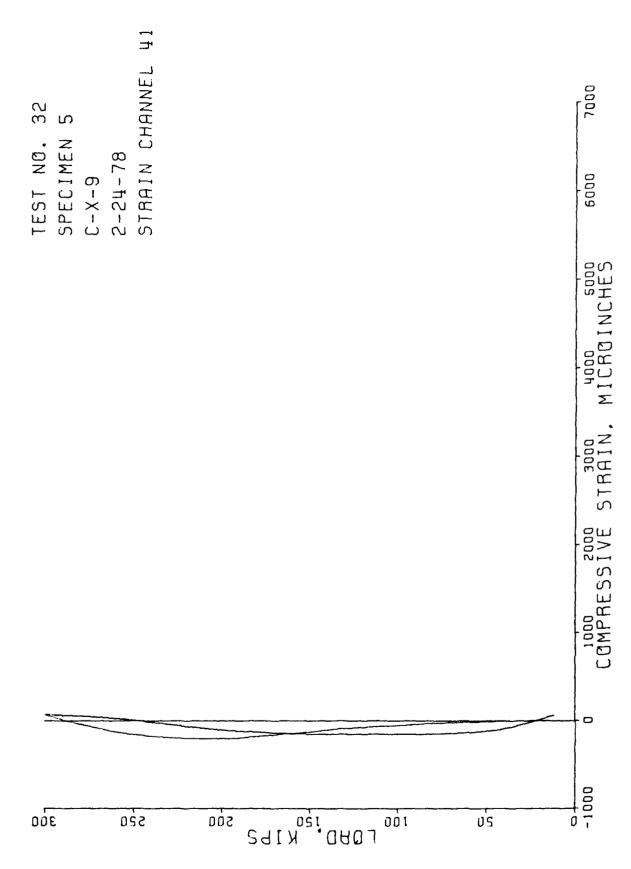












11.22.000	CALIBRATION	000000000000000000000000000000000000000	CALIBRATION	10.000 10.000 10.000 10.000 10.000	CALIBRATION	00000000000000000000000000000000000000
358844 3788901	DISPLACEMENT CHANNEL	14444444444444444444444444444444444444	LOAD CHANNEL	2.8 2.7 2.5 2.2 2.0 2.0	ROD CHANNEL	ያ የ የ የ የ የ የ የ የ የ የ የ የ የ የ የ የ የ የ የ

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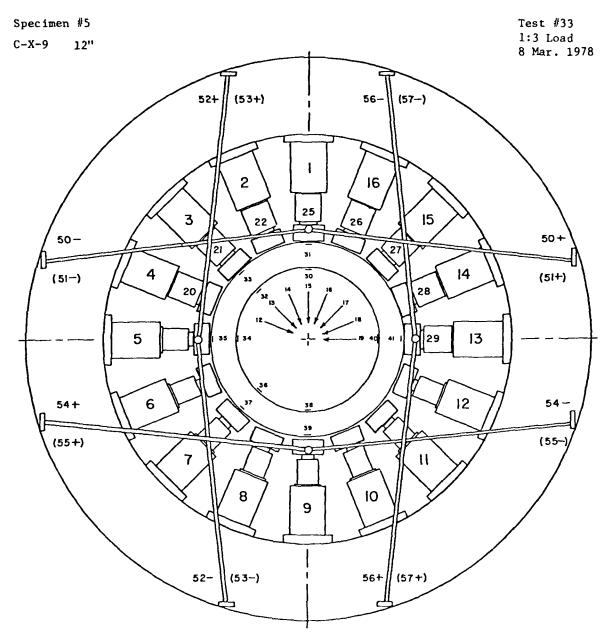
TEST NO. 33

COMPOSITE INTEGRAL LINER

1:3 LCADING RATIO

TESTED 8 MARCH 1978

## REACTION FRAME TEST SET-UP

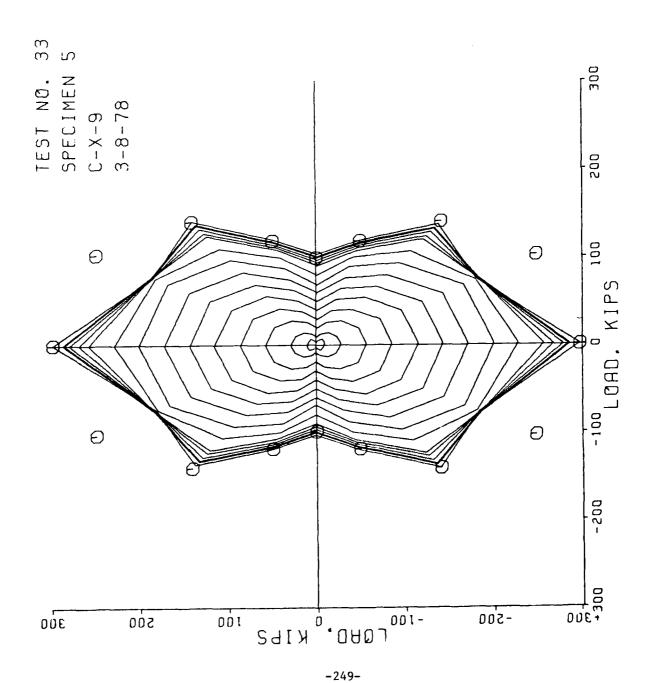


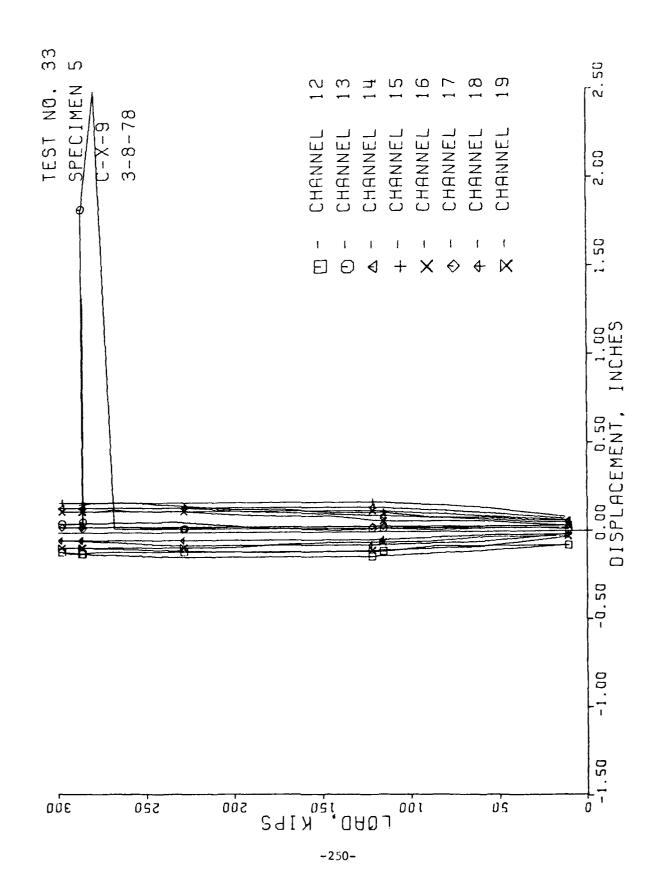
CH 12-19 Load axis I.D. (Research, Inc. Model 4040).

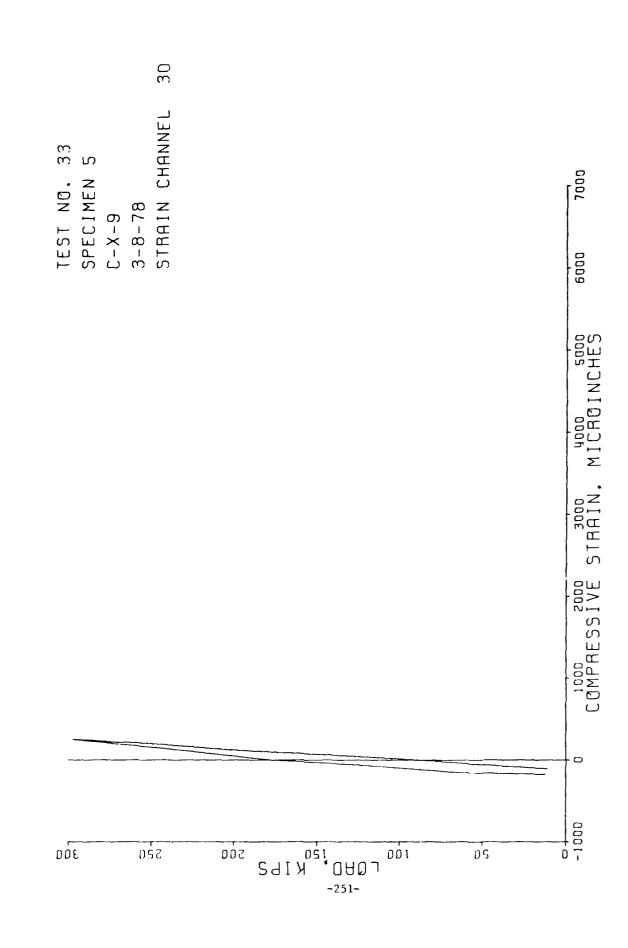
CH 20-22, 25-29 Axial load (Transducers, Inc. Model 693-300K).

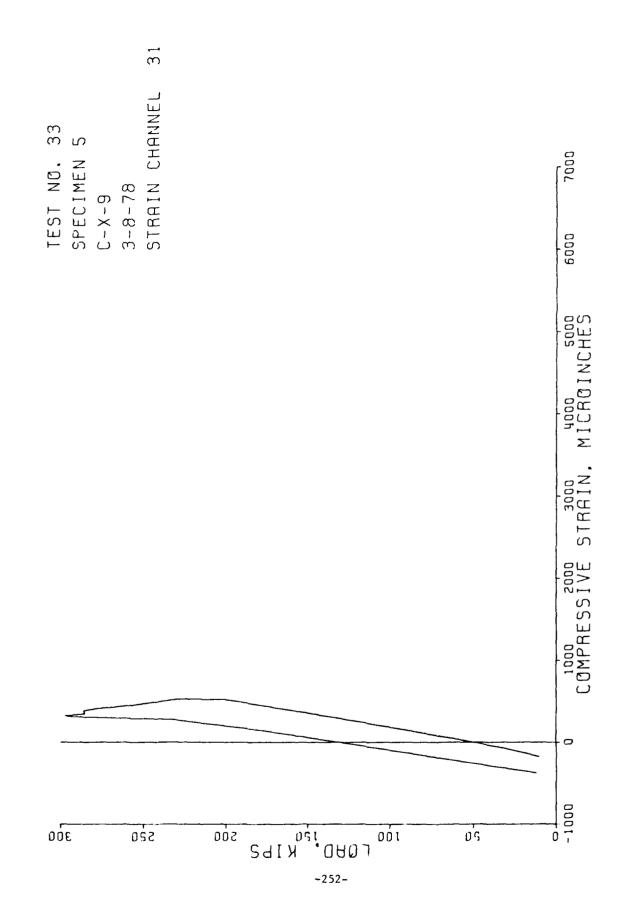
CH 30-41 (Ailtech SG 129-6S) Radial pairs 3" from top. Odd gages on Rebar

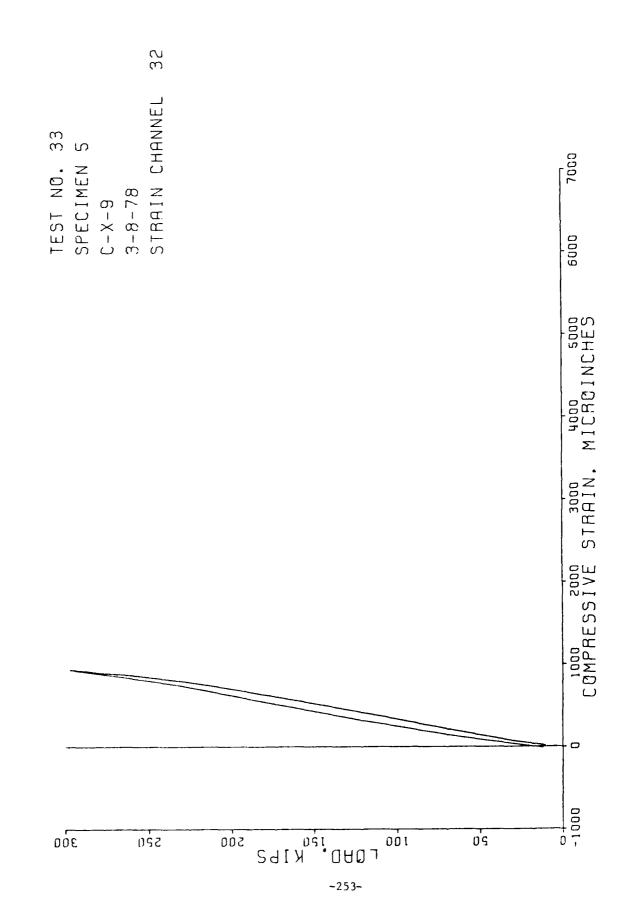
CH 50-57 (Ailtech SG 129-6S) Polarity indicates rod under tension. Lower rod shown (XX).

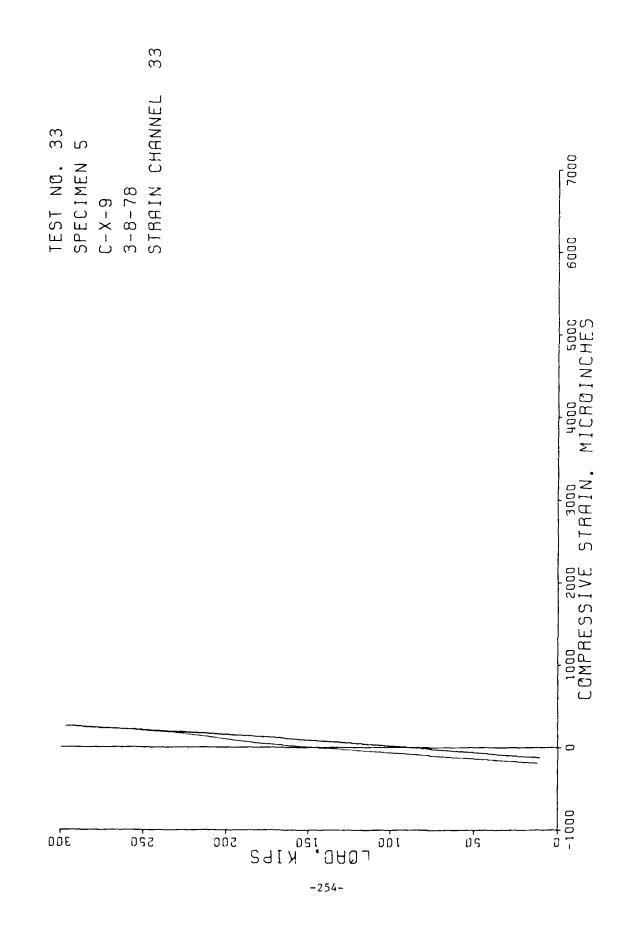


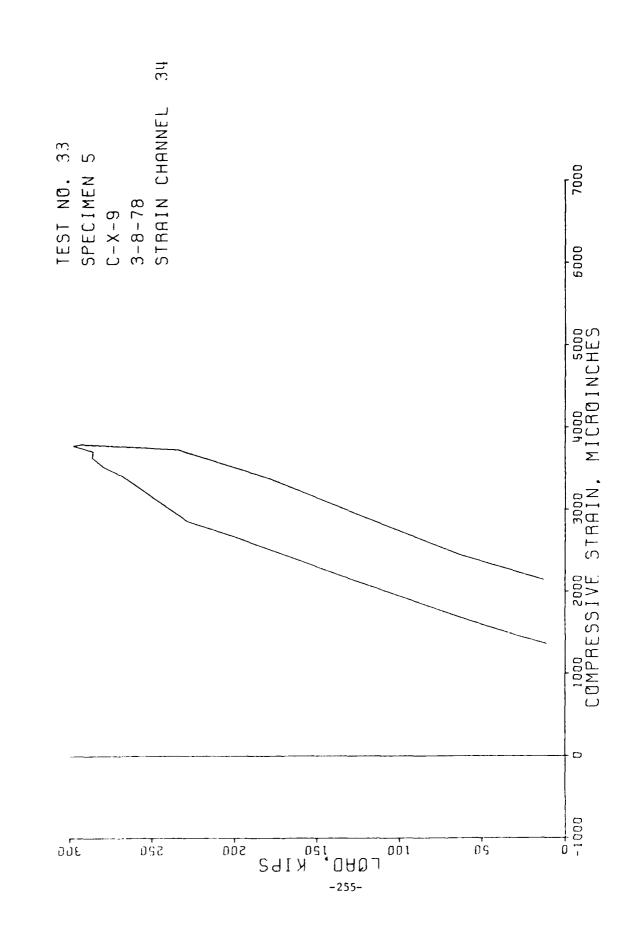


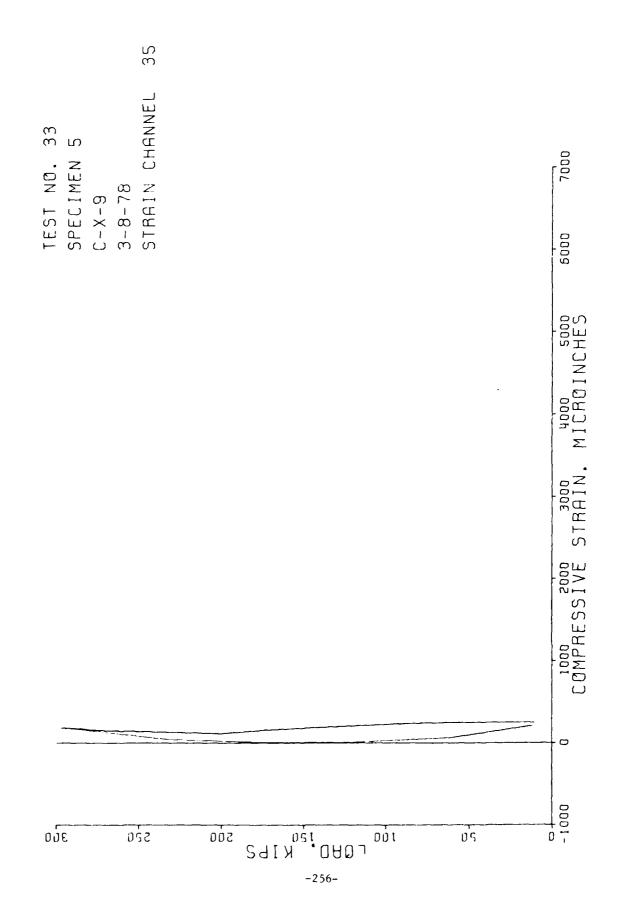


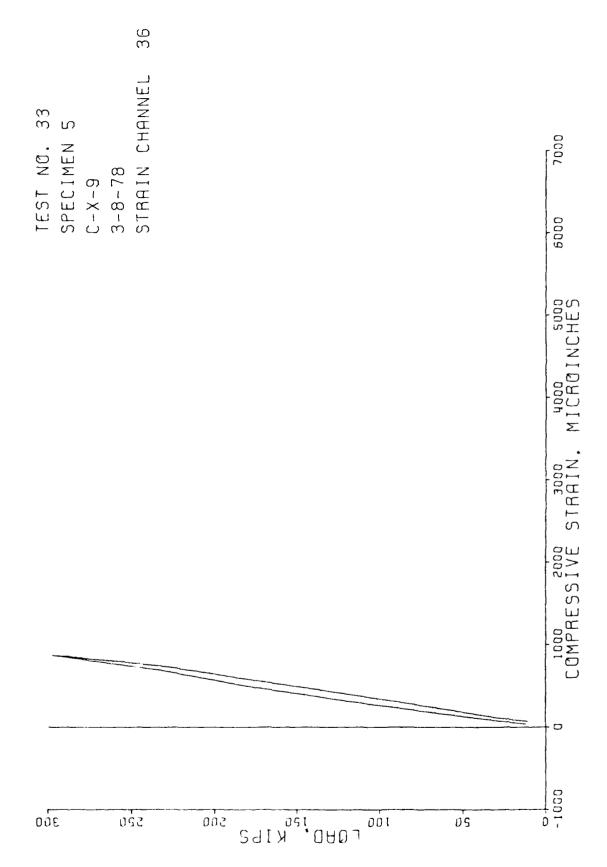


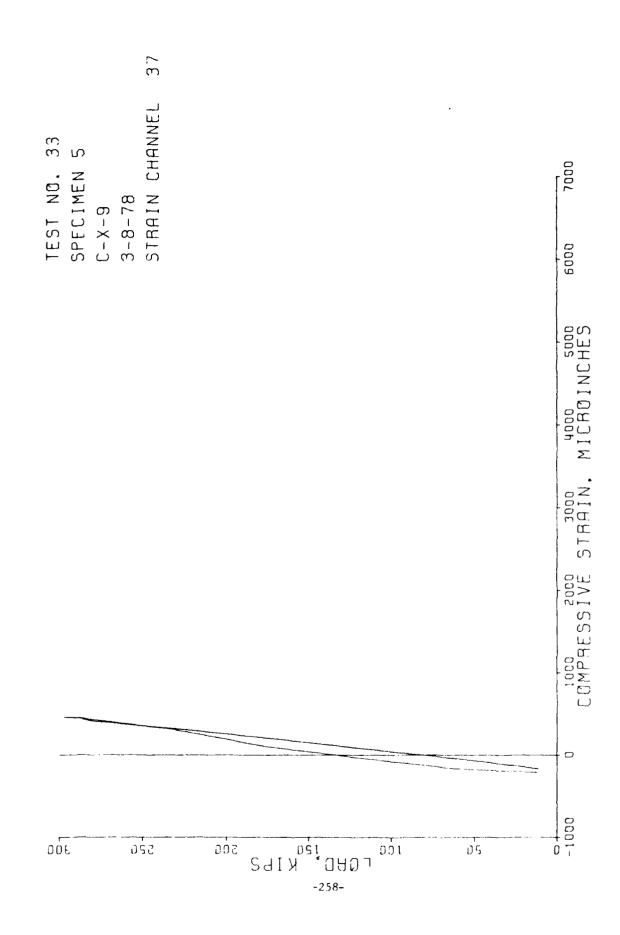


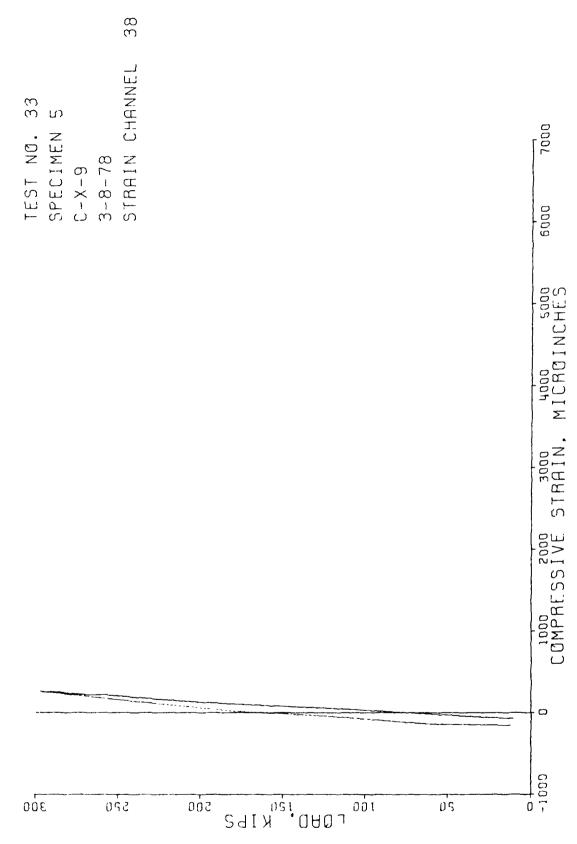


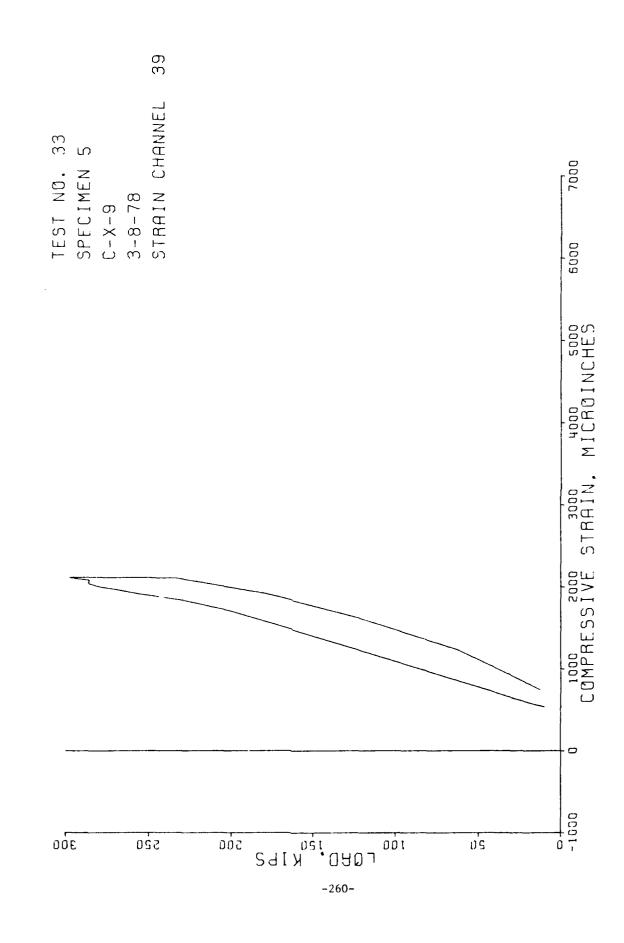


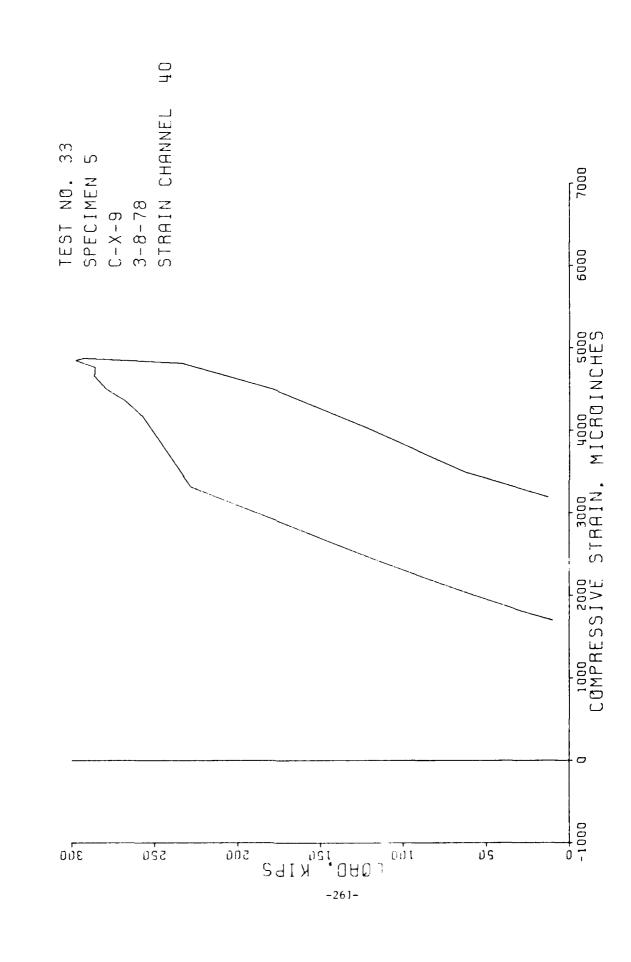


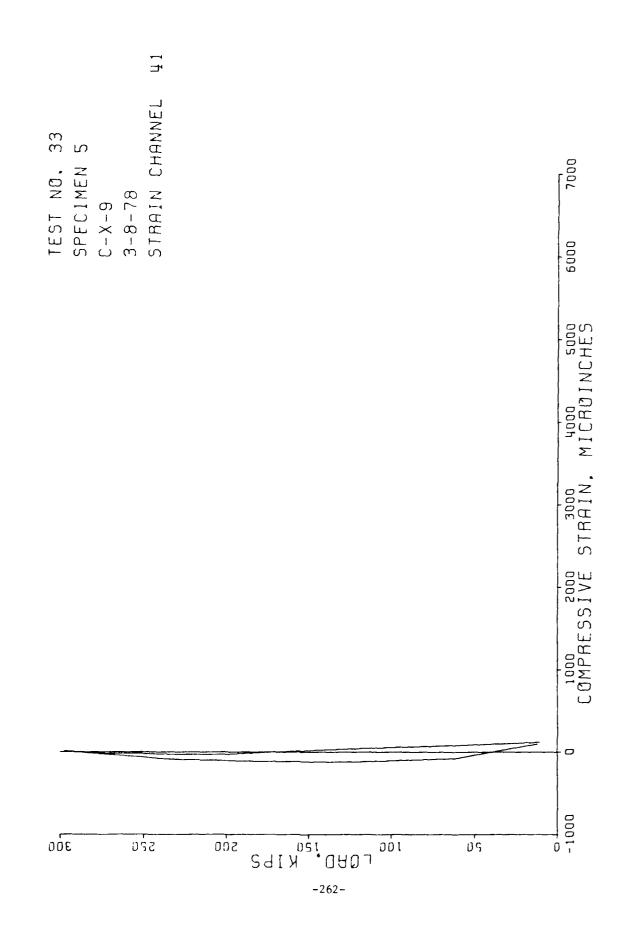












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CH. 4 202.00 803.00 204.00 204.00 639.00 871.00 319.00	-4461.000 -4661.000 -4661.000 -4713.000 -4741.000 -4753.000 -4852.000 -4852.000 -4493.000 -4493.000 -3491.000
CH. 3. CH	2002.2002.2004.2004.2009.2009.2009.2009.
CH.3 70.00 57.00 121.00 121.00 148.00 178.00 179.00 179.00	12552.000 12552.000 12552.000 12552.000 12551.000 1251.000 1251.000 1251.000 1252.000
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<b>まごさみららてきりじ</b>	26.55.42.22.22.22.22.22.22.22.22.22.22.22.22.

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	CH.19	-0.030	0.03	0.05	0.05	0.06	. 0 80 80	0.08	0.08	0.03	0.08	0.08	90.0	200	0.08	0.08	0.08	0.08	0.08	0.10	0.11	0.10	0.08	. O.
	CH.18	-0.019		0.03	0.04	0.04	90.04 9.04	0.04	0.04	0.04	0.04	40.0	9.0	0.0	0.04	0.04	0.04	0.04	0.04	0.07	0.07	. 07	0.05	. 02
	CH.17	0.030	.03	.02	93	.03	.03	. 03	. 03	. 03	.03	50.	.03	3.5	.03	.04	. 03	. 03	.03	.03	. 03	.03		.03
	CH.16	0.030	90	90.	60.	60.	.10	. 12	. 13	. 12	.12	. 1.5	. 13	12	. 12	. 12	. 12	. 12	. 12	. 12	. 12	. 12	50.	90.
	CH.15	0.050	.03	. 03	::	.13	.13	. 17	. 17	. 17	. 16	. 17	91.	120	. 16	. 17	. 17	. 17	. 17	. 17	. 17	. 17	. 14	. D.
	CH.14	09.00	88	80.0	20	7	7 7	14	. 14	. 14	. 14	Ţ	. I &	5 V	,	. 14	. 14	. 14	4	. 14	. 14	7	= :	. 07
N E L S	CH.13	0.010	. 92	20.	.0.	. 02	. 02	. 02	. 02	. 50	.83	Ξ.	. 73	25.	30.	. 05	.05	. 05	. 05	. 06	. 92	. 02	. 02	. 02
X + C T A T	CH.12	0.080	80.	0.08	0.11	0.11		0.11	0.11	0.11	0.12	0.12	0.12	71.0	0.12	0.12	0.12	0.11	0.12	0.14	0.14	0.14	0.11	0.08
DISPLACEME	TIME	1. 8:14:68:45	8:14:50:4	8:14:51:2	8:14:53:2	8:14:54:2	. 8:14:55:1 8:14:56:	8:14:57:1	1. 8:14:57:5	2. 8:14:58:3	3. 8:14:59:3	4. 8:14:59:5	5. 8:15: 0:	6. 8:15: 0:2	8:15: 0:5	9. 8:15: 1:1	0. 3:15: 1:2	1. 8:15: 2:3	2. 8:15: 3:2	3. 8:15: 4:3	4. 8:15: 5:2	5. 8:15: 6:1	6. 8:15: 7:	7. 8:15: 7:5
ISPLACEMENA	E. CH	8:14:68:45 -0.0	8:14:50:40 -0.0	8:14:51:22 -0.0	. 8:14:52:27	8:14:54:27 -0.1	8:14:55:17 -0.1 8:14:56: 8 -0.1	0. 8:14:57:12 -0.1	1. 8:14:57:57 -0.1	2. 8:14:58:34 -0.1	3. 8:14:59:37 -0.1	4. 8:14:59:53 -0.1	5. 8:15: 0: 9 -0.1	8:15: 0:24 -0.1	8:15: 0:55 -0:1	9. 8:15: 1:11 -0.1	0. 8:15: 1:27 -0.1	1. 8:15: 2:30 -0.1	2. 8:15: 3:23 -0.1	3. 8:15: 4:31 -0.1	4. 8:15: 5:24 -0.1	5. 8:15: 6:16 -0.1	6. 8:15: 7: 3 -0.1	7 0 . 1 5 . 2 . 2 . 2 . 2

CH.20	5650.000	. 00	00.0	00.0	00.0	00.0	00.0	00.0	00.0	00.0	00.0	00.0	00.0	00.0	00.0	00.0	00.0	00.0	00.0	00.0	00.0	00.0	00.0	00.0	00.0	00.0	00.0
CH.21	9230.000	0	0	0	0	0	0	0	00	00	00	00	00	00	00	8	00	00	00	00	0	0	00	00	00	00	0
CH.22	9700.000	. 00	00.0	00.0	02630.00	28060.00	53390.00	78790.00	93210.00	96740.00	96640.00	95510.00	00.0	96280.00	96460.00	96610.00	96660.00	96770.00	96820.00	96770.00	94530.00	94320.00	99110.00	73200.00	00.0	00.0	0.00
CH.25	10190.000	8	00	0	00	00	00	00	0	00	00	00	00	00	00	00	00	00	00	0	0	00	0	00	00	00	0
CH.26	8910.000	00.0	00.0	00.0	00.0	00.0	00.0	.00	.00	00.0	00.0	00.	00.0	00.0	00.0	. 00	00.0	00.0	00.0	00.0	00.0	0000	00.0	00.	.00	9.0	00.0
CH.27	8200.000	6	00	00	00	00	17150.00	36970.00	54710.00	74410.00	75830.00	86870.00	00	92750.00	92760.00	92750.00	92750.00	92740.00	\$2690.00	92680.00	98830.00	95180.00	59030.00	20360.00	00	00	0
CH.28	4510.000	3250.00	7540.00	1380.00	4440.00	7900.00	0860.00	4620.00	7910.00	6890.00	0080.00	2770.00	00	5010.00	5300.00	5410.00	5600.00	5660.00	5760.00	5800.00	9910.00	9470.00	7970.00	3570.00	0770.00	4720.00	4380.00
CH.29	2920.000	90.0	30.0	30.0	30.0	0.09	50.0	50.0	50.0	0.0	0.0	0.0	ວ. ວ.	0.0	0.0	0.0	0.0	00110.0	0.0	0.08000	02890.0	0.0	0.0	0.0	0	0.0	0.09
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CH.57	12.81 51.24 02.49	07.43 45.91 79.67 79.36	92.17 30.61 81.85 84.35	009.97 009.97 009.97 009.97 009.97	422.789 461.225 461.225 345.918 -602.154 -563.719 -217.301
CH.56	4000	289.6 289.6 289.6 284.6	243.4 192.1 128.1 -76.8	200000	-51.247 -25.624 -153.742 -397.166 -204.989 12.812 64.059
CH.55	88	2022	2044 4044	342424	243.424 230.612 230.612 602.154 1191.497 1575.851 1832.087
CH.54	0.90 2.78 1.85		20.02 20.03 20.03	20.02.02.02.02.02.02.02.02.02.02.02.02.0	12.812 12.812 12.812 12.812 594.671 960.835 85.390
CH.53	76.871 115.306 166.553 76.871	-889.683 -384.354 -653.402 -1127.438	-1255.556 -1306.803 -1370.862 -1434.921	-1460.545 -1460.545 -1460.545 -1473.357	-1473.357 -1511.792 -1268.368 -281.859 115.306 128.118
CH.52	204.989 461.225 845.579 1024.944	34481	1319.615 1242.744 1153.062 1050.567	00000000000000000000000000000000000000	986.508 909.637 922.449 1217.121 2101.135 1793.652 960.885
CH.51	40080 20090	x ∽ ∞ ∞ ∞ ∞ ∞ ∞ ∞			38.435 38.435 38.435 38.435 25.624 -102.494 -409.978
CH.50		9000	,,,,,,,		0.0 12.0 12.312 12.312 12.812 -64.059 -307.483
TIME	14:48	. 14	. 14:57 . 14:57 . 14:58 . 14:58 . 14:59		8:15: 1:27 8:15: 3:23 8:15: 4:31 8:15: 5:24 8:15: 6:16 8:15: 7:57
	H0.0.4.	. 9 % 7 % 9	<b>CHUND</b>	12.5.5	265.53.5.7

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1. 7413.750

2. 19245.000

3. 59153.750

4. 78598.750

6. 16822.500

8. 152385.000

10. 165263.750

11. 173046.250

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## 3.4.3 RELOAD OF SPECIMEN #5

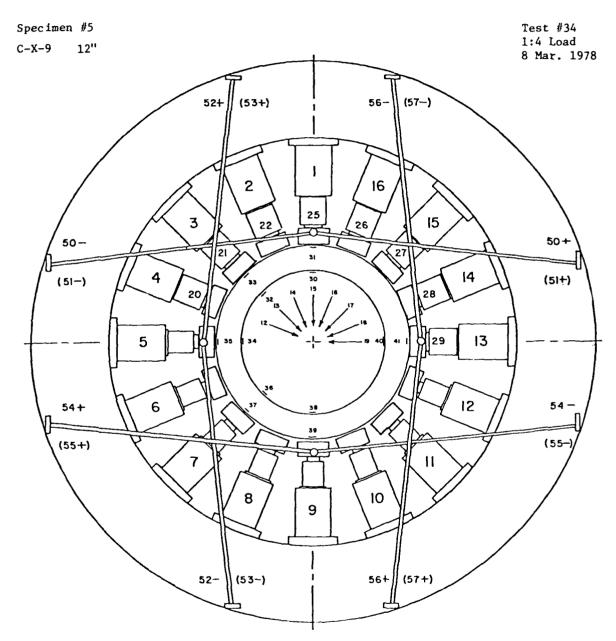
TEST NO. 34

COMPOSITE INTEGRAL LINER

1:4 LOADING RATIO

TESTED 8 MARCH 1978

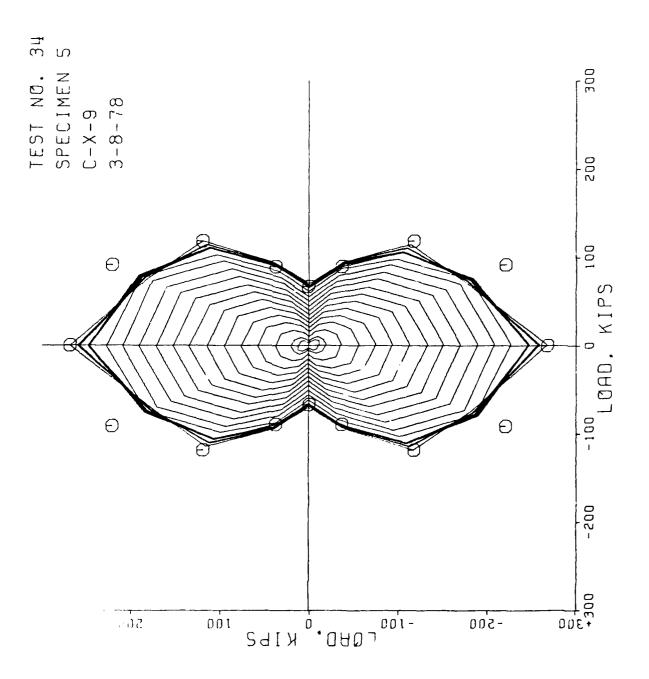
## REACTION FRAME TEST SET-UP

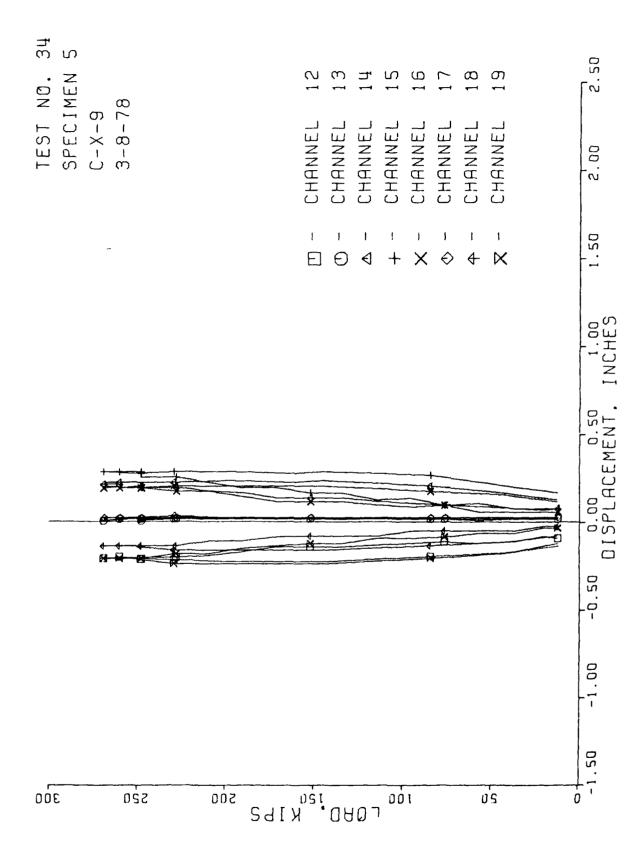


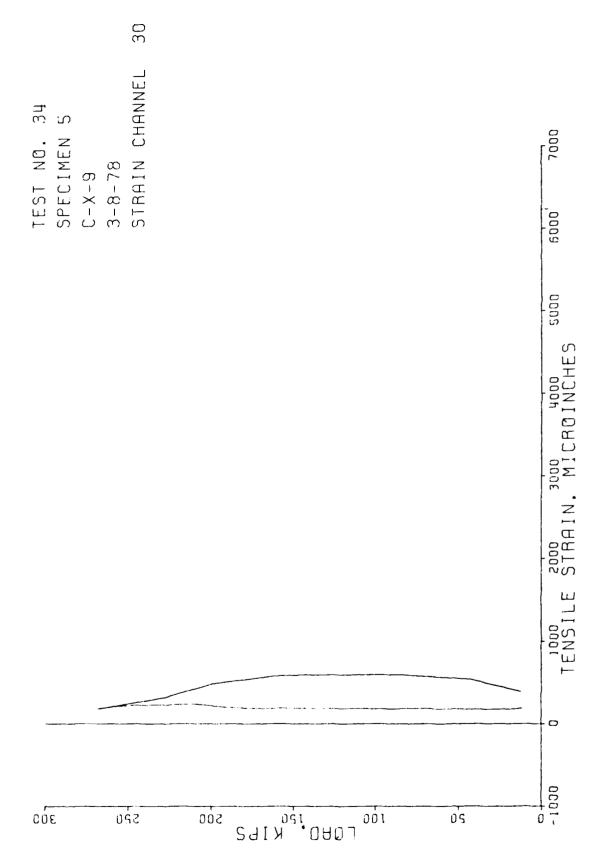
CH 12-19 Load axis I.D. (Research, Inc. Model 4040).

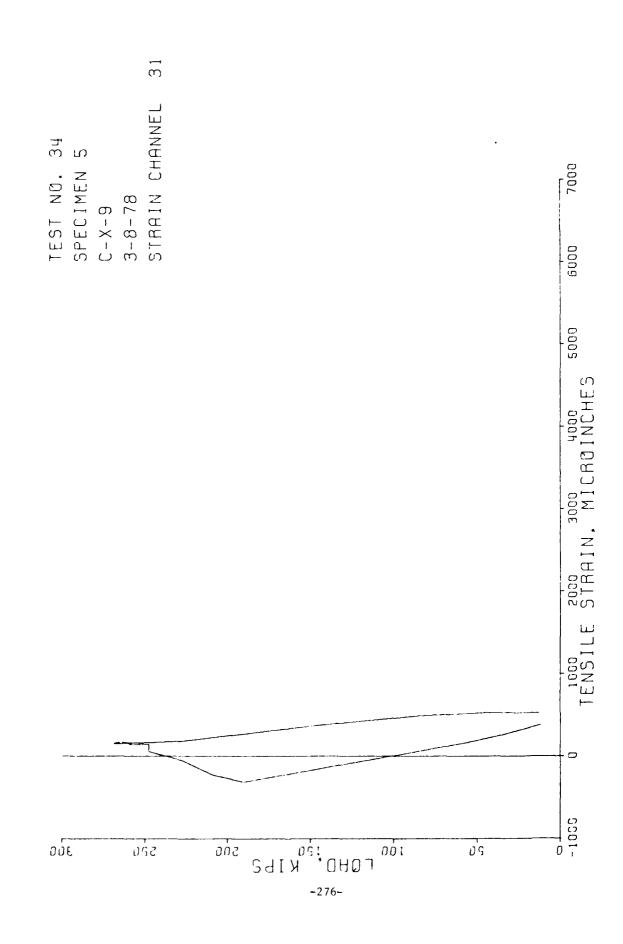
CH 20-22, 25-29 Axial load (Transducers, Inc. Model 693-300K). CH 30-41 (Ailtech SG 129-6S) Radial pairs 3" from top. Odd gages on Rebar

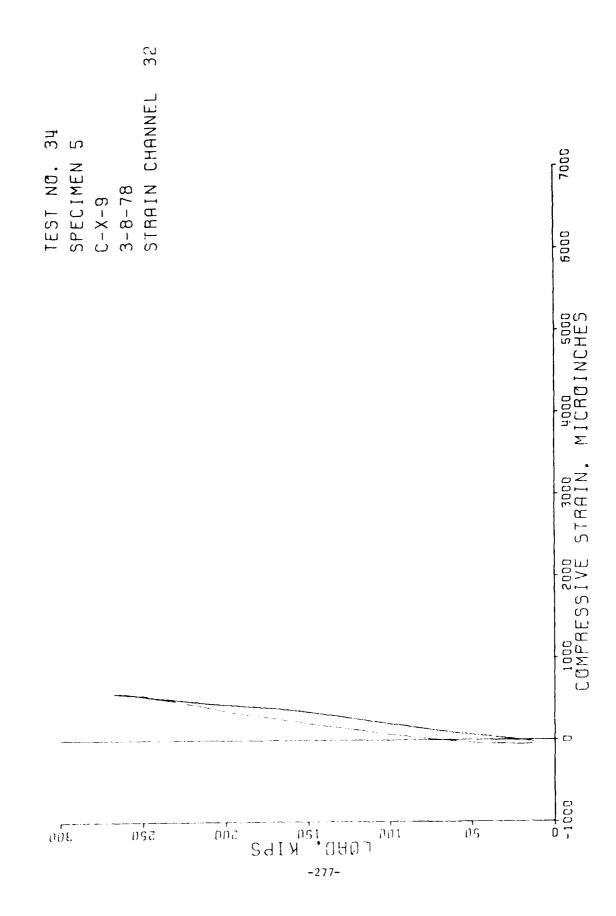
CH 50-57 (Ailtech SG 129-6S) Polarity indicates rod under tension. Lower rod shown (XX).

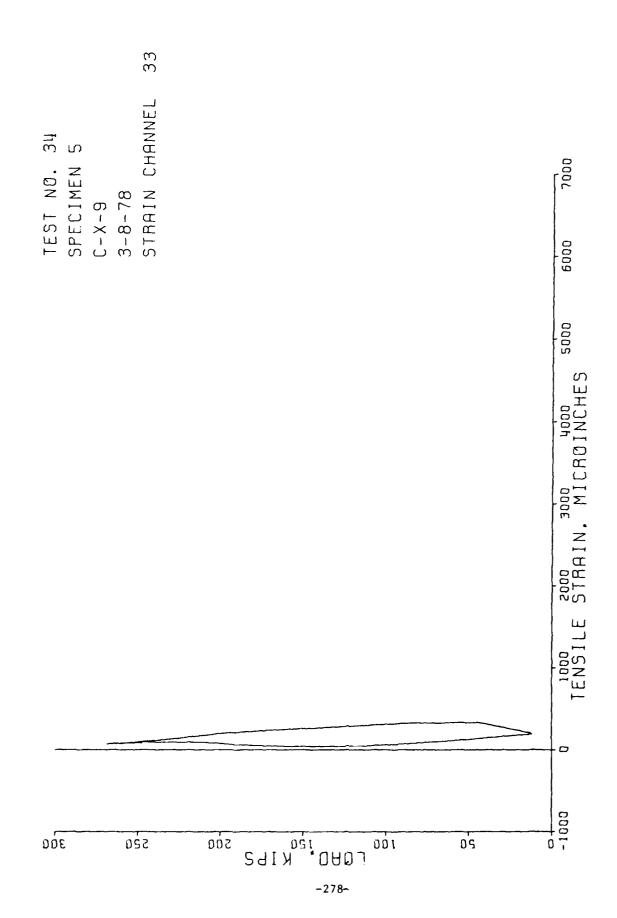


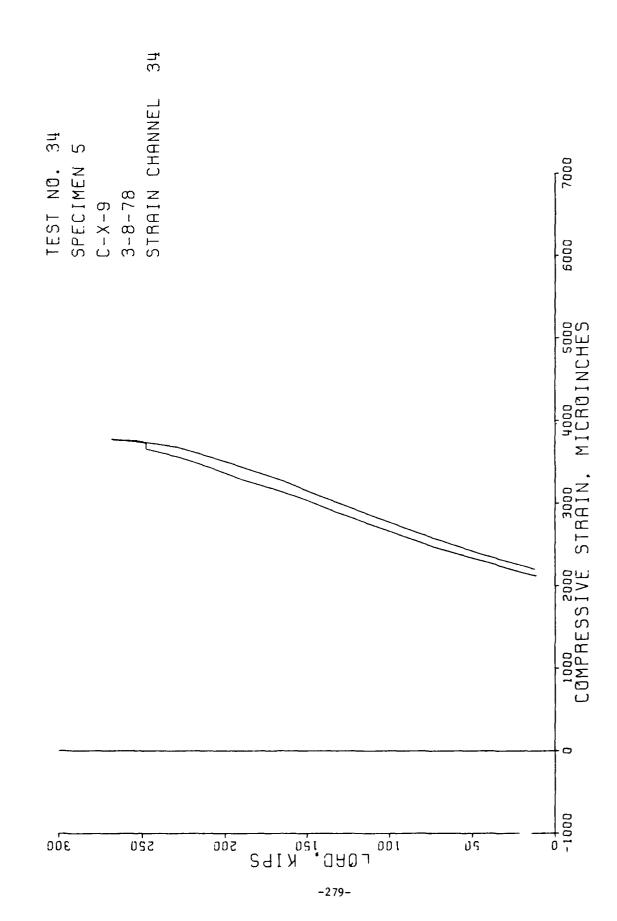


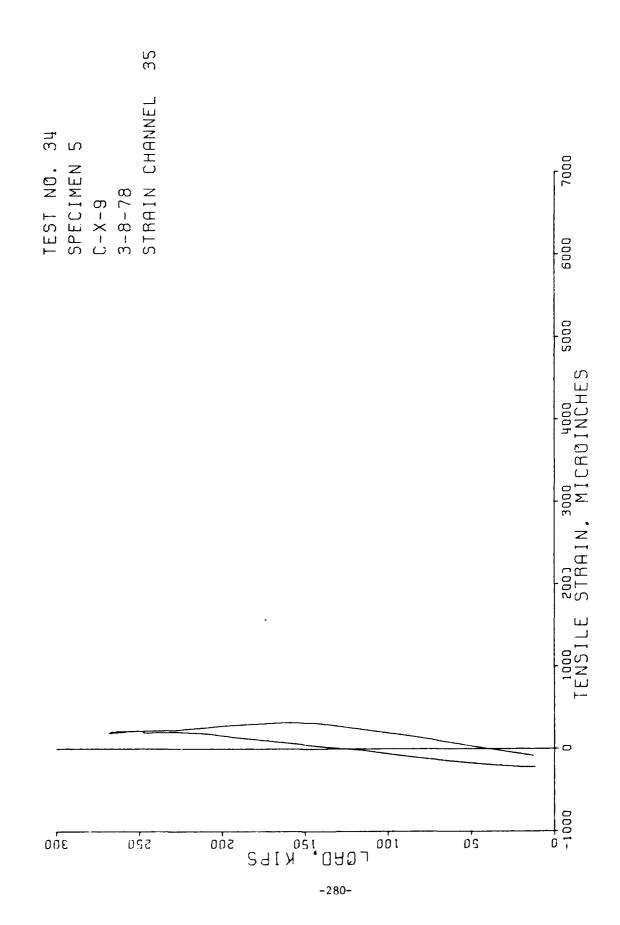


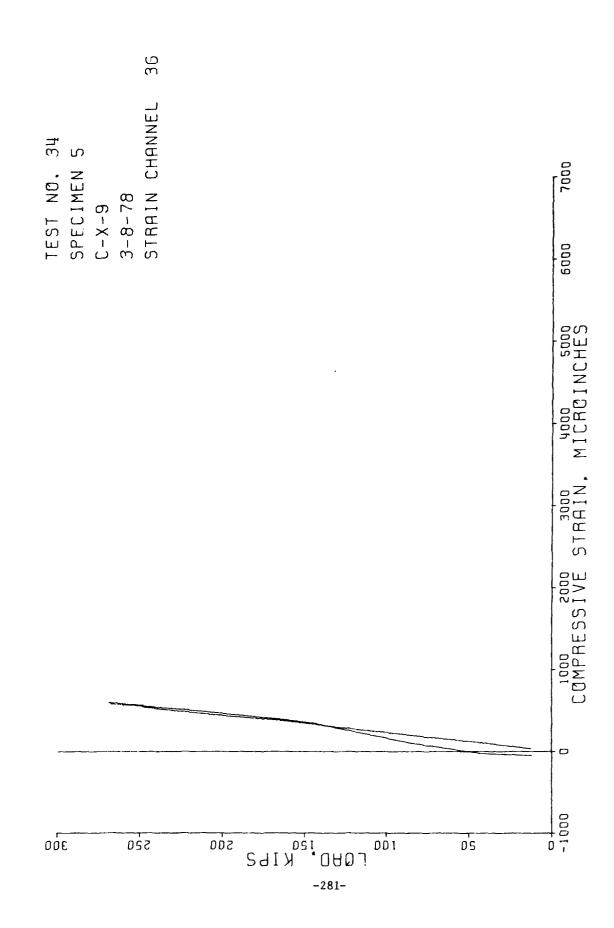


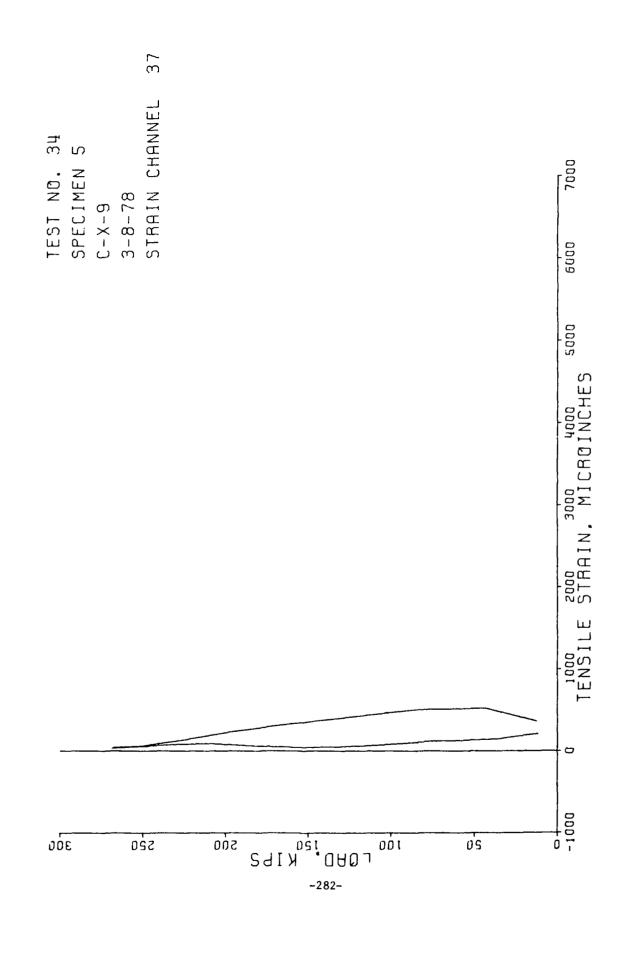


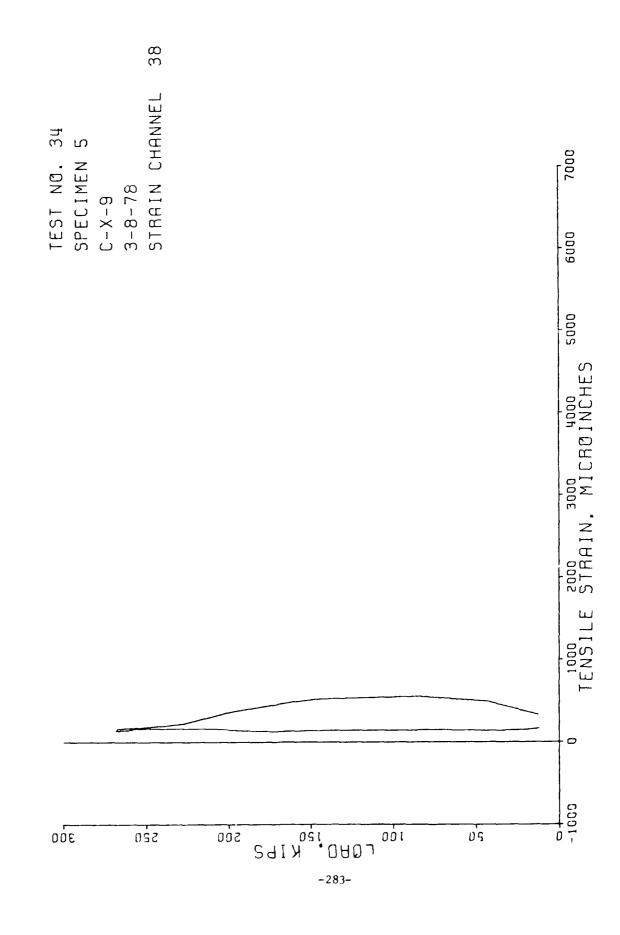


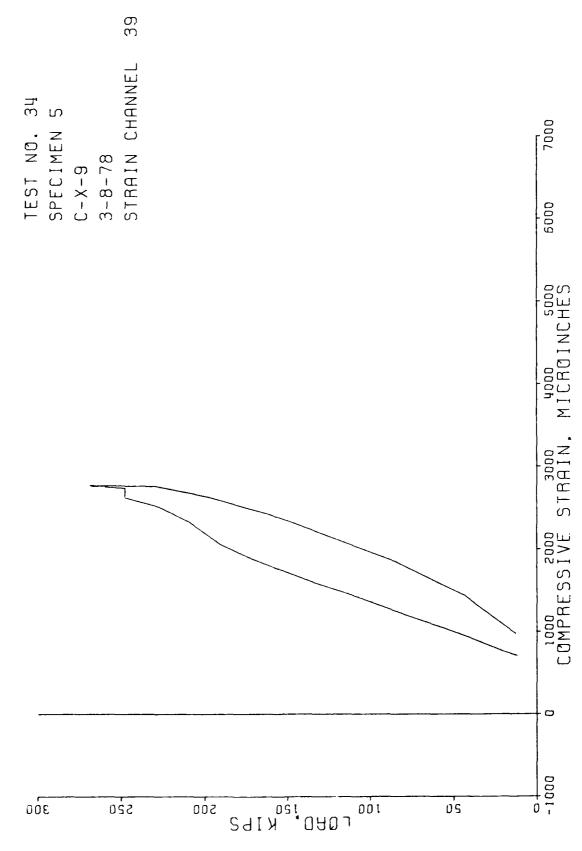


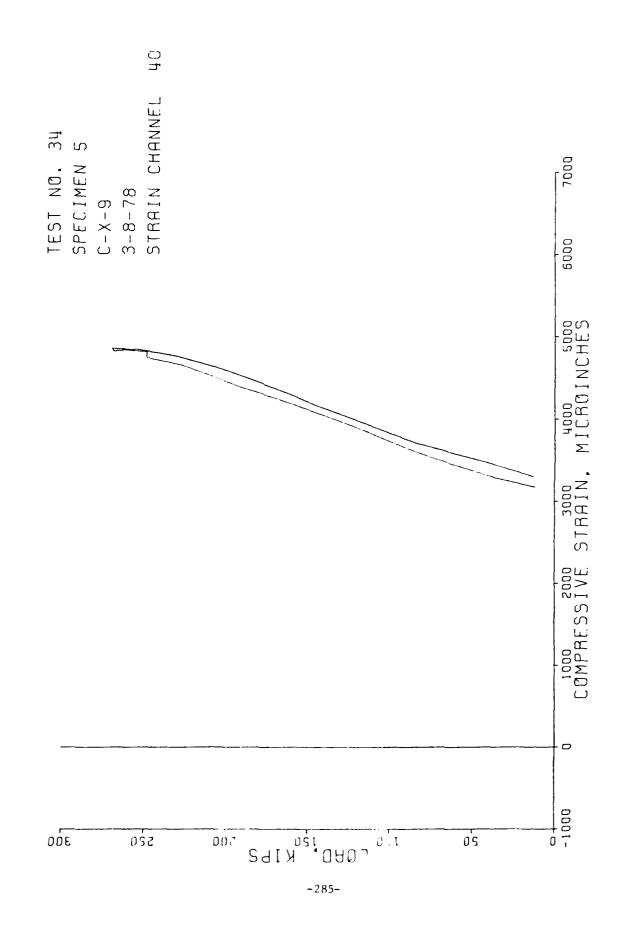


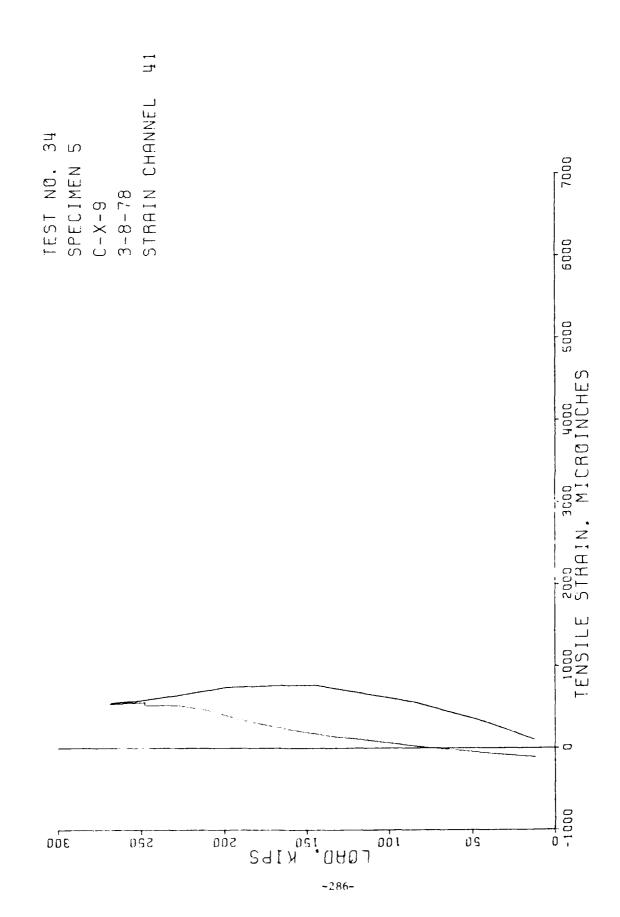












MERRITT CASES INC REDLANDS CA F/6 1
STATIC TESTS OF SEGMENTS OF TUNNEL LININGS. VOLUME II. DATA.(U)
JUN 79 H C DAVIS, K B MORRILL, J L MERRITT DNA-4976F-2

DNA-4976F-2

NL AD-A083 453 F/6 18/3 UNCLASSIFIED 4 or 5 400 4083453

-287-

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11.0000	CALIBRATION	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	CALIBRATION	100.000	CALIBRATION	11.00000
WWWW44 AV&&OI	DISPLACEMENT CHANNEL	112 114 116 118 118 118	LOAD CHANNEL	222 225 225 20 20 20 20 20 20 20 20 20 20 20 20 20	ROD CHANNEL	555 555 555 555 555 555 555 555 555 55

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CH.																																						
CH. 4	-108.000	00.101	32.00	7.00	1.00	99.00	44.00	00.00	65.00	50.00	61.00	24.00	26.00	29.00	32.00	33.00	36.00	38.00	42.00	47.00	50.00	52.00	61.00	55.00	54.00	53.00	48.00	41.00	39.00	6.00	00.//	46.00	43.00	68.00	68.00	59.00	23.00	04.00
CH. 4	-31/6.000	20.0175	3473.00	3538.00	3684.00	5844.00	4002.00	4131.00	4259.00	4385.00	4527.00	4660.00	4747.00	4765.00	4775.00	4783.00	4789.00	4795.00	4802.00	4806.00	4809.00	4811.00	4814.00	4836.00	4838.00	4838.00	4846.00	4856.00	4856.00	4827.00	00.7585	4762.00	4583.00	4316.00	4164.00	3712.00	3478.00	3295.00
CH. 3	000.60/-	20.00	1048.00	185.00	1325.00	1466.00	1601.00	1735.00	1879.00	2062.00	2323.00	2516.00	2631.00	2649.00	2662.00	2672.00	2681.00	2688.00	2696.00	2703.00	2710.00	2715.00	2744.00	2759.00	2762.00	2764.00	2769.00	2778.00	2781.00	2771.00	27.7.00	2763.00	2640.00	2429.00	2304.00	1846.00	1437.00	974.00
CH. 3	165.000		45.00	48.90	46.00	47.00	45.00	39.00	31.00	41.00	67.00	67.00	63.00	62.00	61.00	60.00	60.00	62.00	63.00	64.00	65.00	65.00	68.00	59.00	58.00	57.00	52.00	41.00	39.00	64.00	75.00	21.00	70.00	86.00	24.00	54.00	97.00	31.00
TIME	8:15:16:17		. 15:19:2	:15:20:1	:15:20:5	:15:21:4	:15:22:4	:15:23:3	:15:24:2	:15:55:1	:15:26:	:15:26:4	:15:27:2	:15:27:4	:15:27:5	:15:28:1	:15:28:2	:15:28:4	:15:28:5	:15:29:1	:15:29:3	:15:29:4	:15:32:2	:15:32:3	:15:32:5	:15:33:	:15:33:2	:15:33:3	:15:33:5	:15:34:1	: 15:34:2	:15:35:	: 15:35:3	:15:36:2	:15:37:	:15:38:1	:15:39:1	:15:39:5
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CH.19	0.030	20.0	0.38	11.0 0.12 1.0	0.17	0.20 0.20	0.20	0.20	0.20	0.20	0.20	0.20	0.20	0.20 0.20	0.20	0.23	0.23	0.23	0.17
CH.18	-0.019 -0.019 -0.046	* * * * * * * * * * * * * * * * * * *	0.07	0.07 0.07 0.10	0.10	$0.12 \\ 0.12$	$0.12 \\ 0.12$	0.12	0.12	0.12	0.12	0.12	0.12	9.12 0.12	0.12	0.15	0.15	0.15	0.07
CH.17	0.030		0.03	0.00	030	. 03 . 03	.030	.03	50.	.03	0.0	.03	.03		.03	.04	30.	.03	.03
CH.16	0.060	87.5	12	122	 82	202.	202	.21	202	22	202	.21	12:	22.2	22	22	12	.21	. 12
CH.15	0.080.080	101	113	202	.23	.26 26	.28	29	29	29	29	200	.23	2.5	.29	52.	28,	29	. 17
CH.14	0.080	. 10	175	.14	. 18	202.	.212	202.	22.	23	233	22.5	.22	222	233	23	23.	25	.13
CH.13	0.020	.020	.02	000	.02	. 02	.02	.02	.02	2.5	.02	20.		. 02 . 02	.01	20.	. 22	20.	.02
CH.12	.0.090 -0.080 -0.110	0.12	0.13	0.14 9.14 0.17	0.19	0.20	9.20	0.20	0.21	0.20	0.21	12.0	0.23	0.27	6.21	0.22	0.23	0.23	0.18
TIME		. 8:15:19:2 . 8:15:20:1 8:15:20:5	8:15:21:4 8:15:22:4	8:15:23:3 8:15:24:2 8:15:25:1	8:15:26:	. 8:15:27:2 . 8:15:27:4	. 8:15:27:5 . 8:15:28:1	8:15:28:2	8:15:28:5	8:15:29:3	8:15:32:2	8:15:32:5	8:15:33:2	. 8:15:33:5 . 8:15:33:5	8:15:34:1	8:15:35:	8:15:36:2	8:15:37:	8:15:39:1
	HOM	a m	, r~ «		13	44	11	# C	22	22,2	25	26	180	NE	50 FG	2	, m	50 M	33.5

CH.20	930.00 800.00 800.00 850.00	520.00 270.00 250.00 260.00 740.00	94440.00 97470.00 99450.00 00280.00 00610.00	450.00 540.00 540.00 750.00 750.00 740.00	102580.000 102770.000 102770.000 101240.000 94040.000 76880.000 54270.000 54270.000 12920.000 3560.000
СН.21	9470.00 4170.00 4960.00 7170.00 8230.00 9940.00	22160.00 22160.00 94290.00 07130.00 18100.00	39050.00 50470.00 50250.00 50110.00 50180.00	9980.00 0060.00 0060.00 0040.00 0790.00 6090.00	61710 61640 61560 61560 61560 61560 61560 6150 615
CH.22	810.00 040.00 260.00 120.00	00650.00 17070.00 33890.00 50510.00 66510.00	96220.00 95000.00 96630.00 97490.00 98270.00 98370.00	510.00 700.00 540.00 580.00 580.00 830.00	188900.000 1888710.000 188690.000 193120.000 178200.000 155540.000 155540.000 78866.000 42030.000
CH.25	080.00 030.00 160.00 120.00 650.00	14290.00 14290.00 51860.00 70870.00 90610.00	27510.00 47790.00 47700.00 47400.00 47520.00 47540.00	460.00 369.00 580.00 670.00 850.00 310.00	68680 67980 67210 67210 53460 28690 28690 62080 62080 62080
CH.26	0480.00 7180.00 3990.00 1860.00 8160.00	00.00 38250.00 55560.00 72500.00	03460.00 02980.00 04690.00 05660.00 06570.00	7080.00 7290.00 7310.00 7280.00 3830.00 0670.00	97150 97060 97060 97290 00210 02570 75380 42730 72210 37610
CH.27	7870.00 2960.00 4380.00 6940.00 8510.00	74600.00 74600.00 97530.00 10970.00 22890.00	45820.00 56370.00 56340.00 56430.00 56430.00 56430.00	6560.03 6750.00 6820.00 6780.00 6460.00 1910.00 1880.00	167510.000 167430.000 167430.000 1588510.000 173240.000 123240.000 99550.000 88140.000 25570.000
CH.28	3980.00 7450.00 5750.00 4150.00 1560.00	6510.00 4060.00 1450.00 8790.00 6180.00	1200.00 6680.00 8290.00 8850.00 8850.00	9090.00 8960.00 8860.00 9110.00 8830.00 0630.00	101600.000 101550.000 101550.000 10150.000 91310.000 76220.000 50450.000 50450.000 13350.000 3610.000
CH.29	2830.00 4500.00 9890.00 5260.00 6560.00	5060.00 5060.00 5060.00 5020.00 5540.00	1650.00 6390.00 5630.00 6200.00 7020.00	6920.00 7030.00 7130.00 6960.00 6420.00 8470.00 8000.00	70590.000 70360.000 63920.000 59580.000 49710.000 46270.000 19670.000 2370.000
TIME	15:16:1 15:17:5 15:18:3 15:19:2 15:20:1	15:21:4 15:22:4 15:23:3 15:24:2 15:25:1	115:23:4 115:27:2 115:27:4 115:23:15:15:28:1	115:28:5 115:29:15 115:29:4 115:32:2 115:33:2 115:33:2	88:155:333 88:155:334:56 88:155:334:10 88:155:334:10 88:155:335:34 88:155:335:34 88:155:383:14 88:155:383:14
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CH.57	2.81 2.45 2.45 8.11 8.11 9.36	79.36 115.30 112.81 28.11 22.78	4635.60 474.03 474.03 486.84 486.84	86.84 86.84 86.34 99.66 112.47 112.47	2001 2001 2001 2001 2001 2001 2001 2001
CH.56	64.05 76.87 76.87 38.43 38.43	-64.05 115.30 166,55 243.42 320.29 448.41	35.60 61.22 61.22 74.03	461.22 461.22 461.22 461.22 461.22 461.22 461.22	44444444444444444444444444444444444444
CH.55	78 91 . 4 8 8 9 1 . 4 8 8 9 . 0 9 9 9 1 . 4 8 8 9 . 0 9 9 9 8 8 9 9 9 9 9 9 9 9 9 9 9 9 9 9	04.64 89.34 99.66 97.16 07.48 79.36	553.745	555.74 553.74 553.74 56.55 74 74	179.365 156.553 158.242 217.801 230.612 1012.132 1345.239 1498.334 1883.334 12812.087
CH.54	6.53 6.53 6.53 6.53 6.53 6.55	38.68 125.843 125.862 125.862 125.862 125.862 125.862	222222	2222222 802882828 8028838	12.812 12.812 25.812 12.812 12.812 166.553 4615.812 4615.812 765.553 765.553 768.390
CH.53	51.24 89.68 15.30 02.49 76.87	-204.98 -409.97 -691.83 -935.26 1140.25 1460.54	1550.22 1554.60 1524.60 1511.79	524.60 524.60 537.41 537.41 537.41 550.22	1553 11563 11563 11550 11550 11550 11550 11550 11550 11550 11550 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1150 1
CH.52	179.36 256.23 525.28 819.95 050.56	281.18 396.48 409.29 396.48 358.05 388.05	293.99 306.80 319.61 332.42 332.42	345.42 332.42 332.42 319.61 306.80	1306.803 1281.180 1281.180 1293.991 1293.991 1153.062 1364.899 1362.605 365.918
CH.51	\$2.50.88 \$1.00.44	8888888 444444 88888888	8880000 444666 8886666	88866688888888888888888888888888888888	38.435 25.624 25.624 25.624 25.624 25.624 25.624 25.624 25.612 25.624 25.612 25.624
CH.50		0088880		5000000000	12.812 12.812 12.812 12.812 12.812 12.812 12.812 14.05.059 1.550.907
TIME	115:16:1 115:17:5 115:18:3 115:19:2 115:20:1	15:22:4 15:22:4 15:22:4 15:26:1 15:26:1	115:27:2 115:27:4 115:27:5 115:28:1 115:28:2	115.784 115.784 115.784 115.787 115.787 115.787 115.787 115.787	88:155:33:23 88:155:33:23 88:155:33:34 115:35:35 88:115:35 88:115:35 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115:33 115
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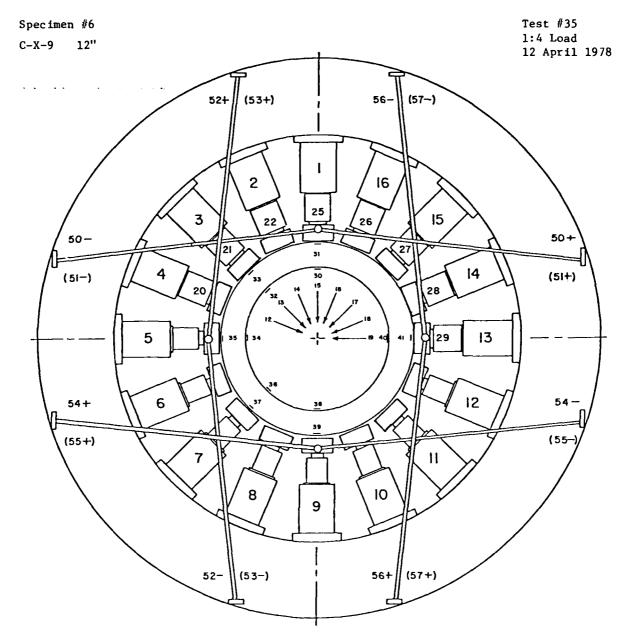
20562 22462 22462 22462 22462 22462 22462 2250 2250 2250 2250 2250 2250 2250 22	

MAXIMUM LOAD CHANNEL, 25 REACHES A MAXIMUM VALUE AT STEP NUMBER 29

## 3.4.4 SPECIMEN #6

TEST NO. 35
COMPOSITE INTEGRAL LINER
1:4 LOADING RATIO
TESTED 12 APRIL 1978

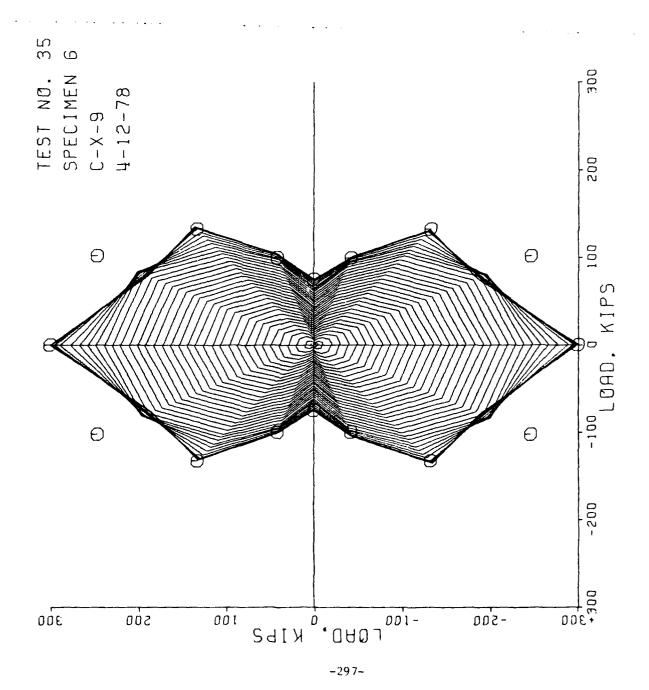
## REACTION FRAME TEST SET-UP

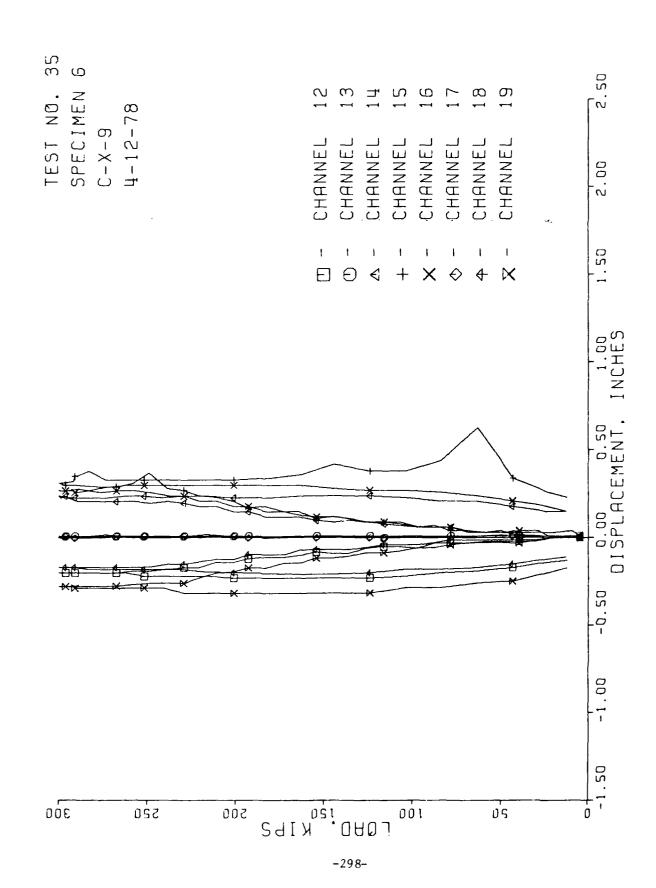


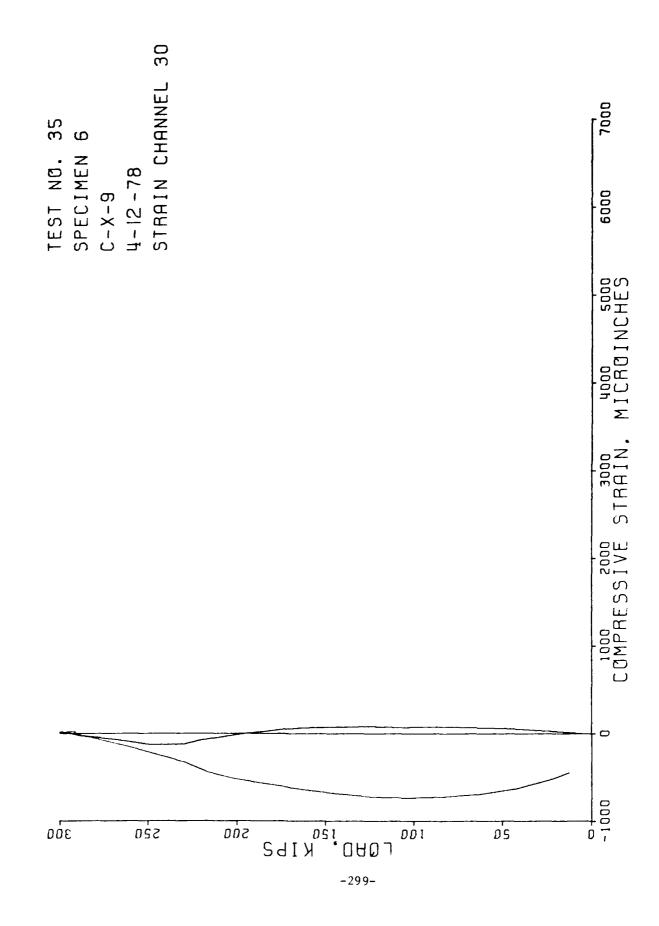
CH 12-19 Load axis I.D. (Research, Inc. Model 4040).

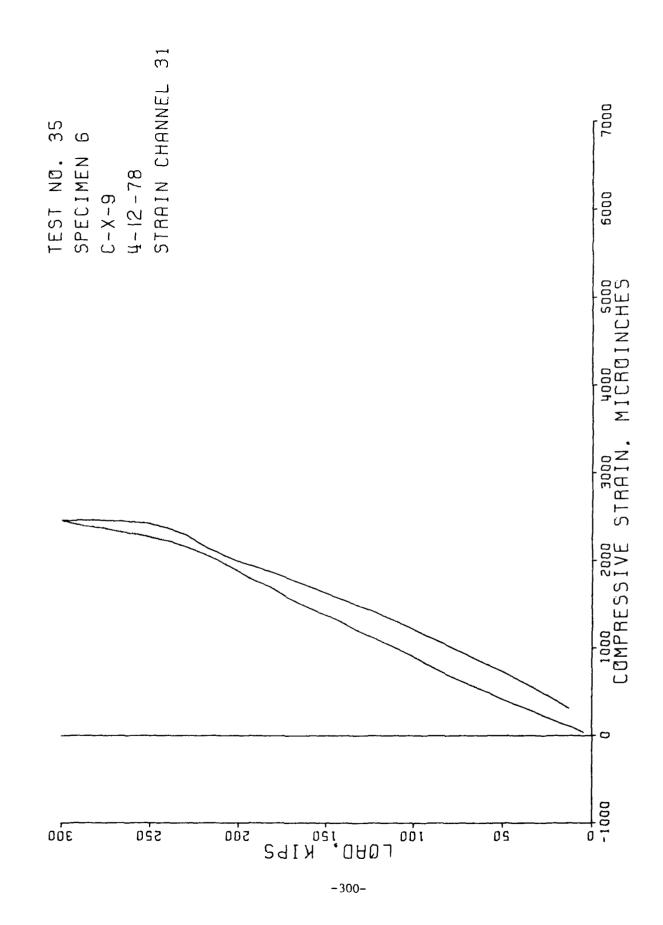
CH 20-22, 25-29 Axial load (Transducers, Inc. Model 693-300K).

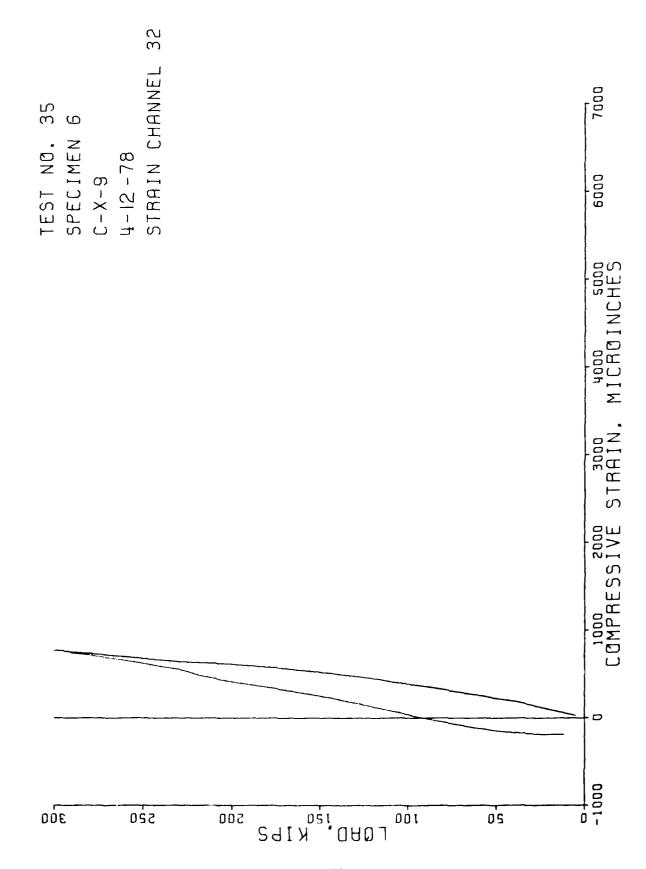
CH 30-41 (Ailtech SG 129-6S) Radial pairs 3" from top. Odd gages on Rebar. CH 50-57 (Ailtech SG 129-6S) Polarity indicates rod under tension. Lower rod shown (XX).

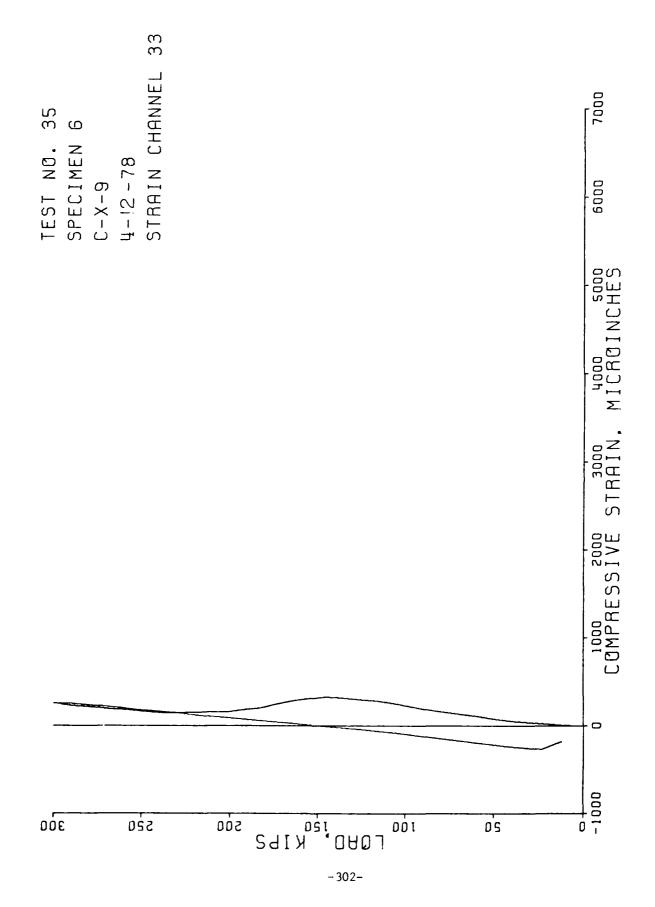


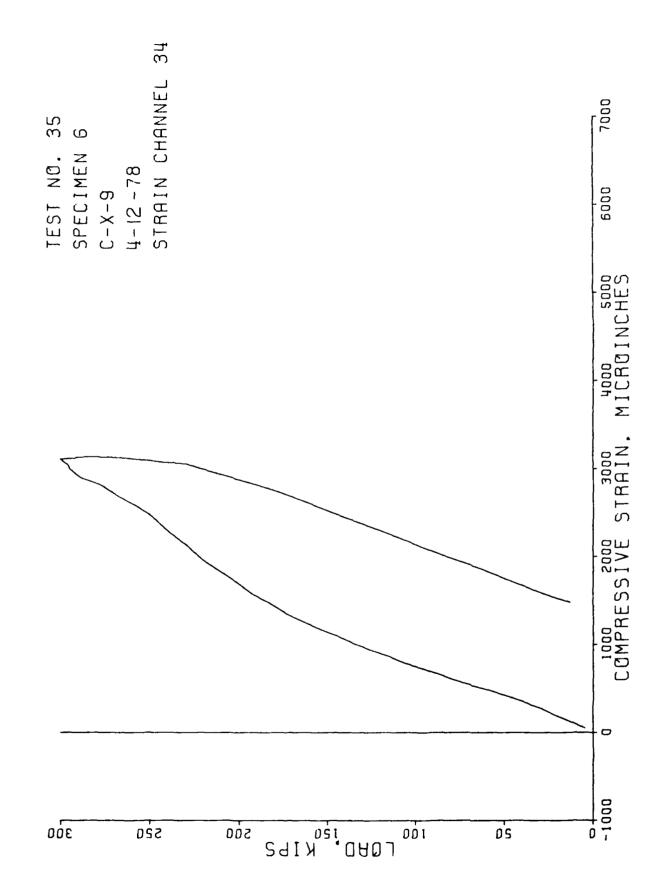


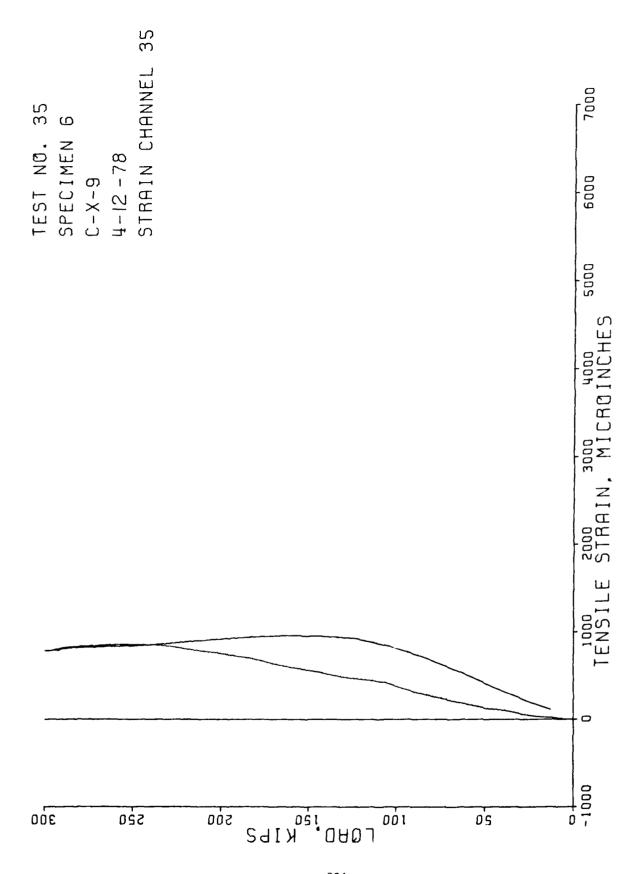


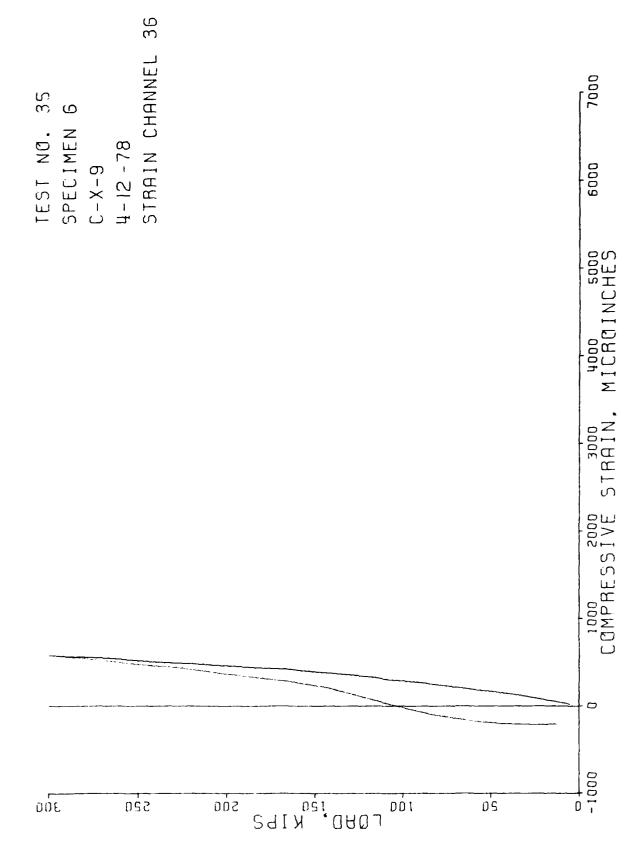


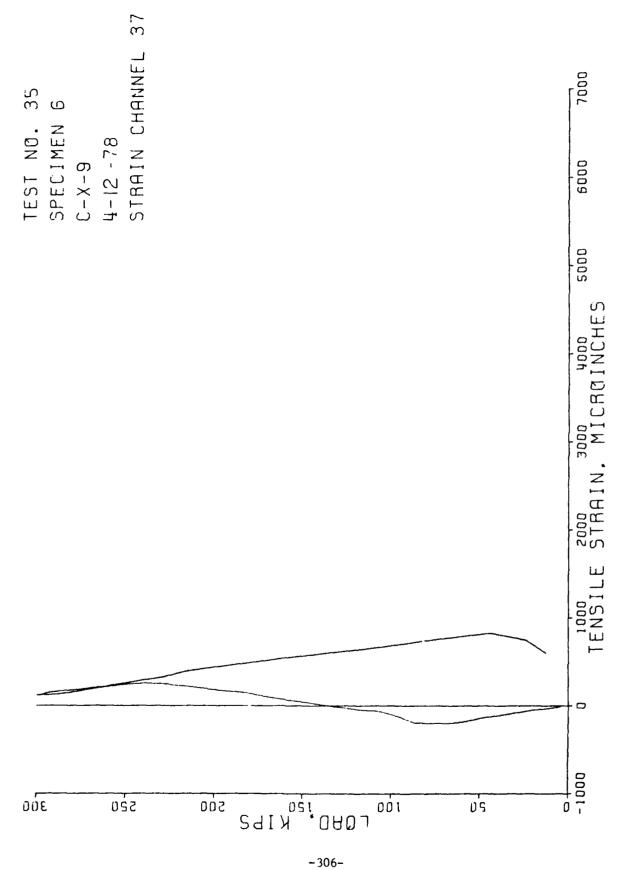


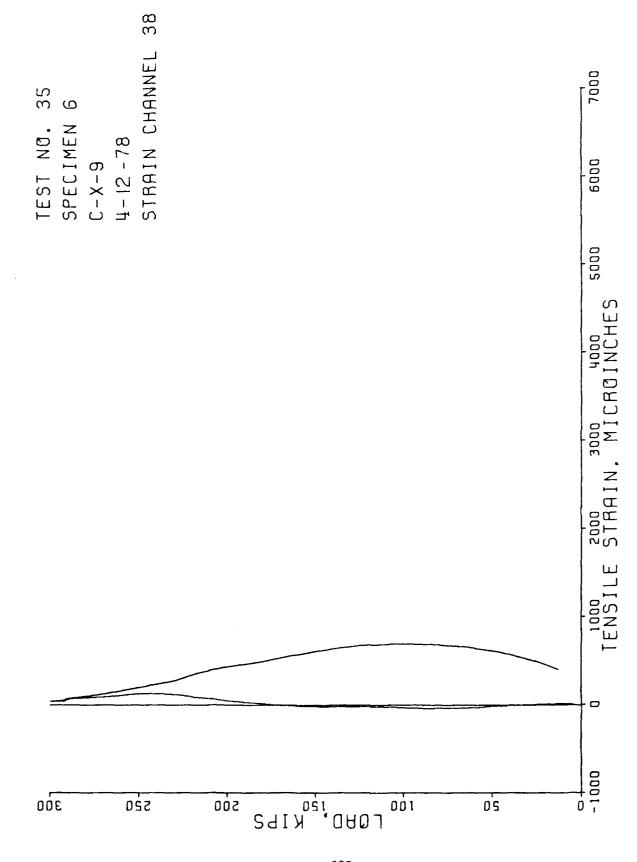


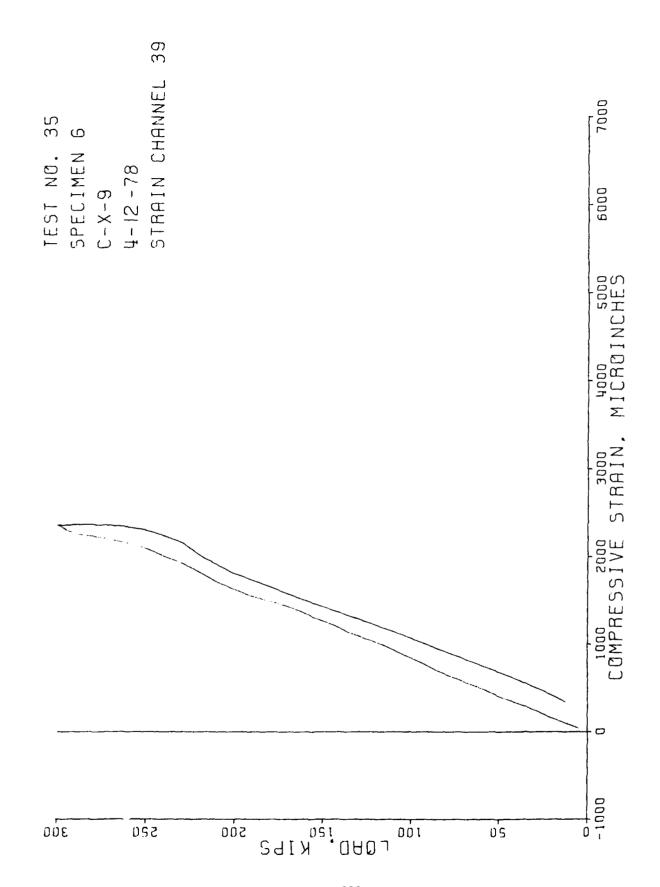


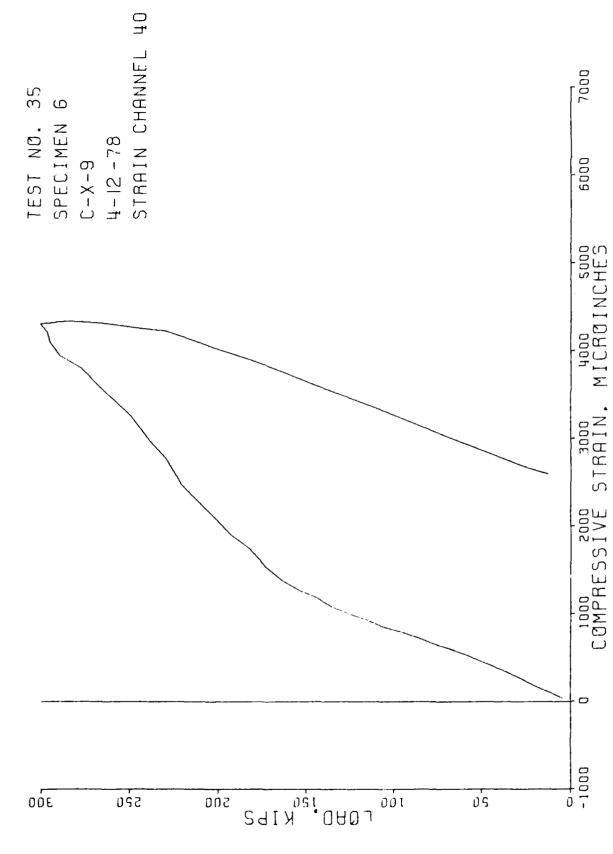


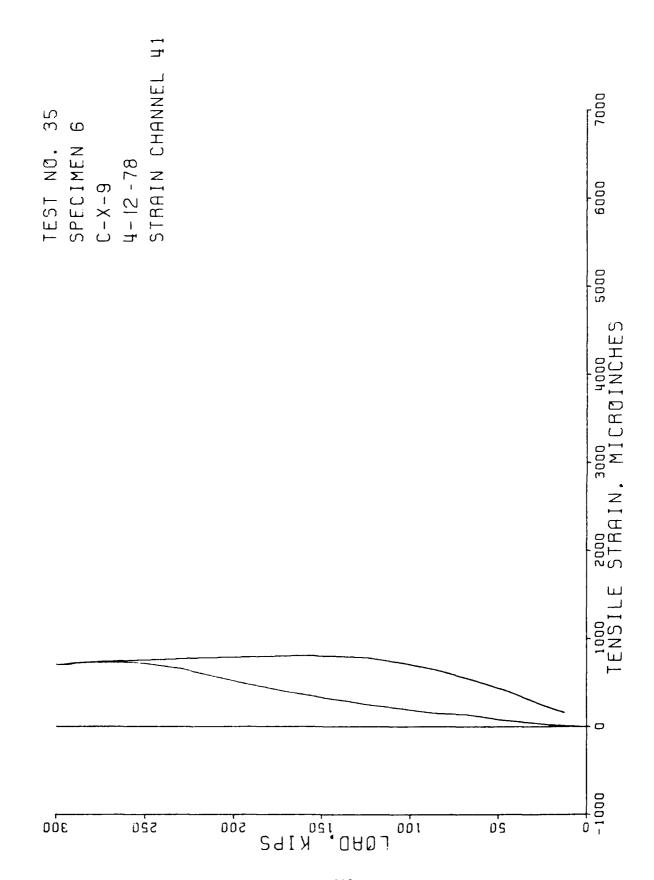












1.000	CALIBRATION	0.010 0.010 0.010 0.010 0.010 0.010	CALIBRATION	10.000 10.000 10.000 10.000 10.000 10.000	CALIBRATION	1.000 1.000 1.000 1.000 1.000
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CH.37	1   1   1   1   1   1   1   1   1   1	43.00
CH.36	11111111111111111111111111111111111111	15.00
CH.35	88888888888888888888888888888888888888	88.00.
CH.34	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	1552.00
CH.33	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	68.00
CH.32	11111111111111111111111111111111111111	90.00
CH.31	1   1   1   1   1   1   1   1   1   1	52.00
CH.30	11111128333.0000000000000000000000000000000000	30.60
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TITE	2014:190:170:170:170:170:170:170:170:170:170:17

| CH.19 | •                                                   | - 5                                                                                                     | 0.03                                                                                                         | 0.0                                                                | 2.0                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                        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MAXIMUM LOAD CHANNEL, 25 REACHES A MAXIMUM VALUE AT STEP NUMBER 35

## 3.4.5 SPECIMEN #8

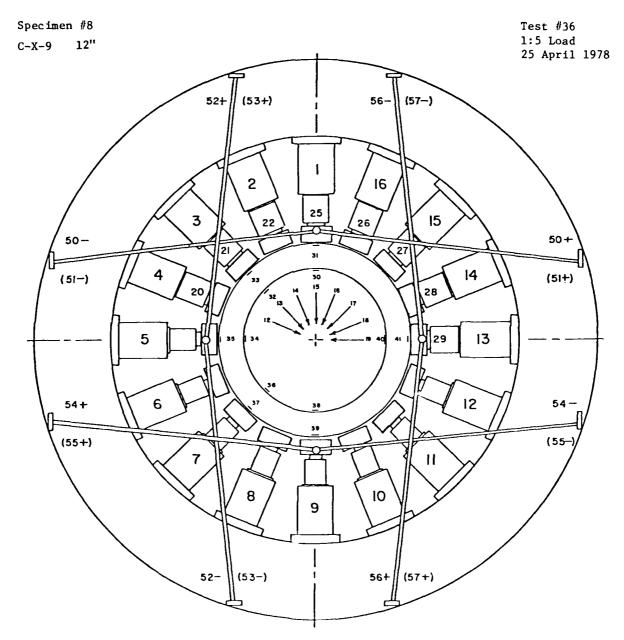
TEST NO. 36

COMPOSITE INTEGRAL LINER

1:5 LOADING RATIO

TESTED 25 APRIL 1978

## REACTION FRAME TEST SET-UP



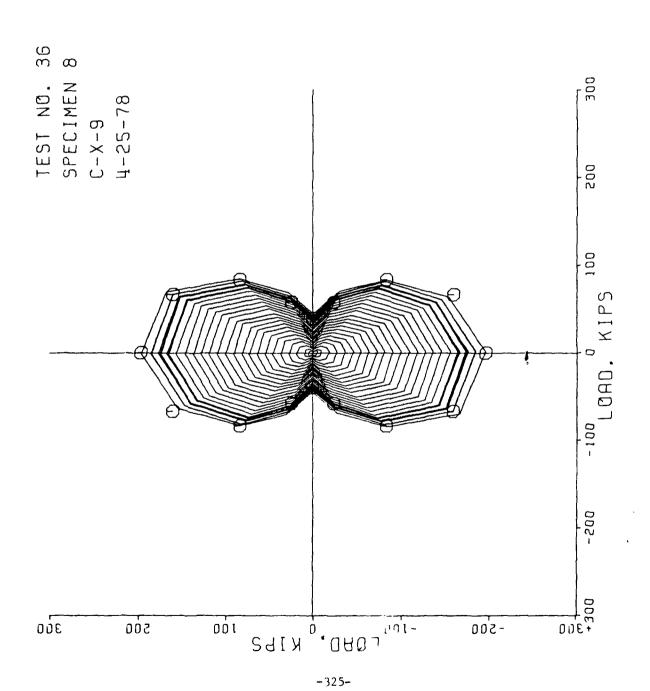
CH 12-19 Load axis I.D. (Research, Inc. Model 4040).

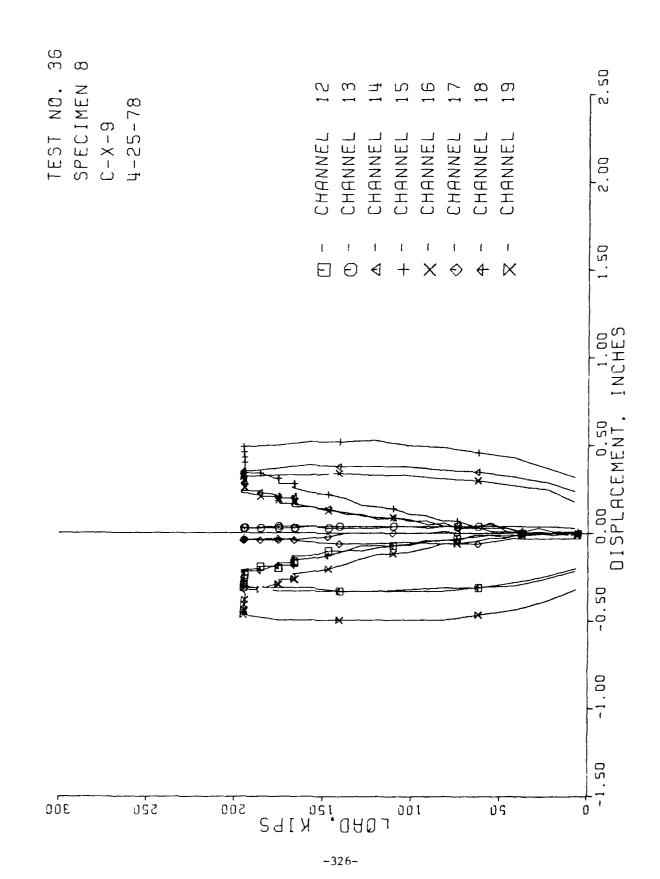
CH 20-22, 25-29 Axial load (Transducers, Inc. Model 693-300K).

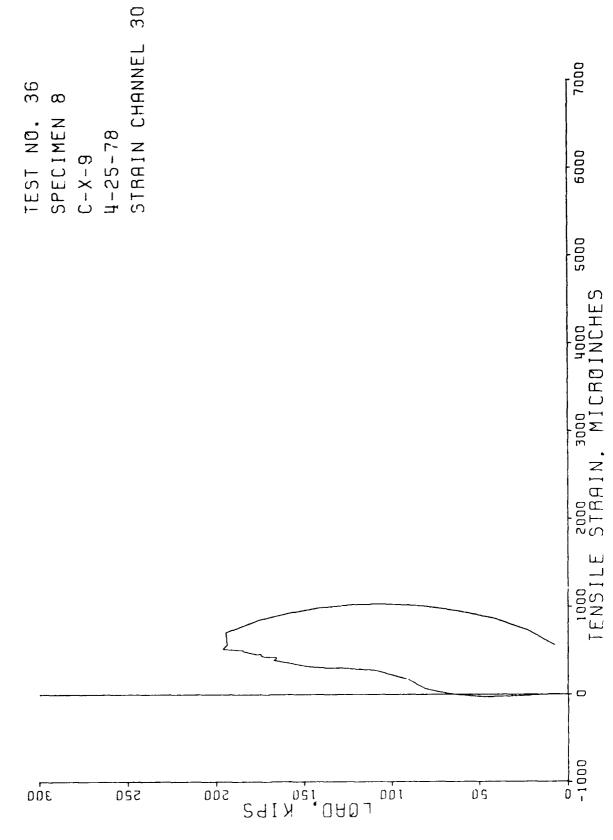
CH 30-41 (Ailtech SG 129-6S) Radial pairs 3" from top. Odd gages on Rebar.

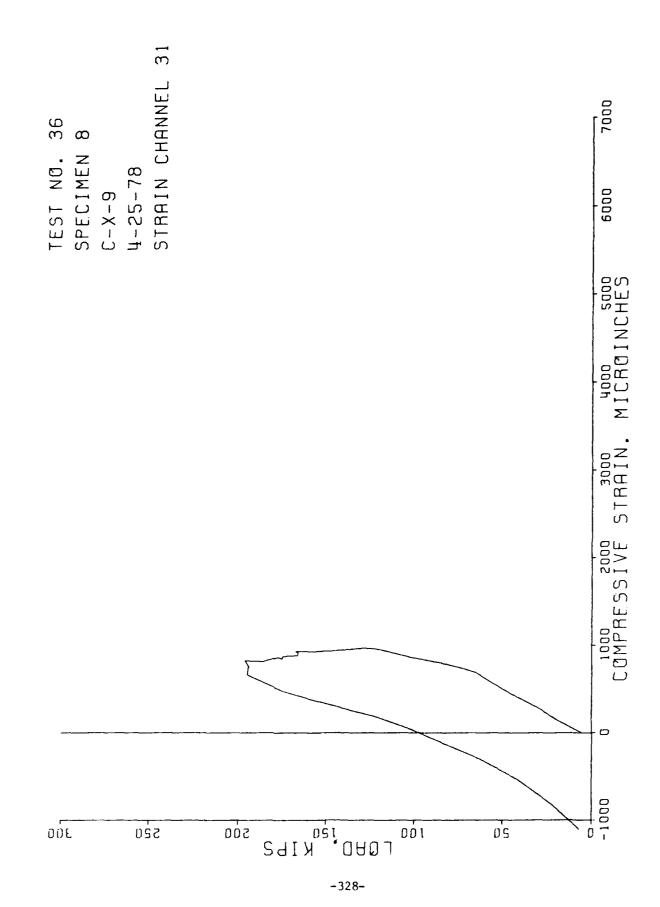
CH 50-57 (Ailtech SG 129-6S) Polarity indicates rod under tension.

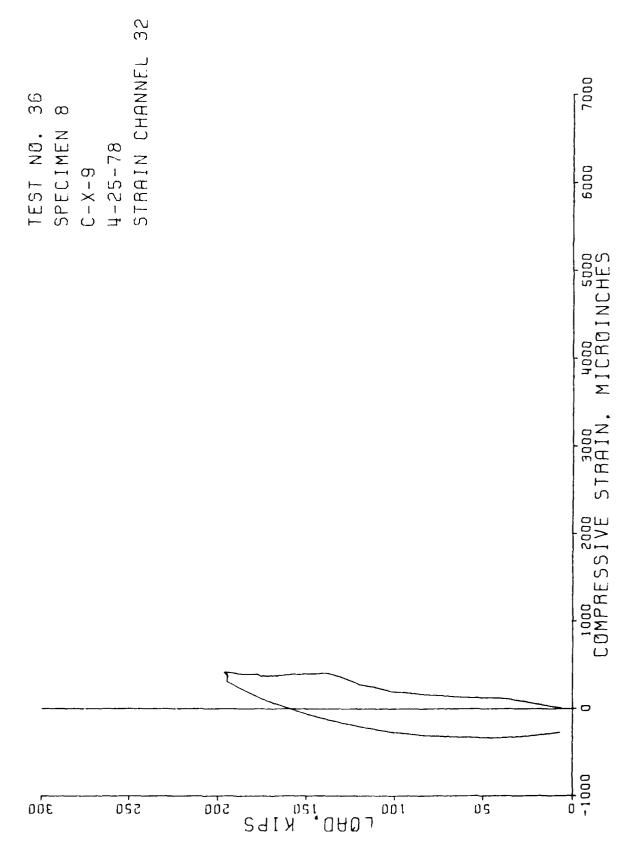
Lower rod shown (XX).

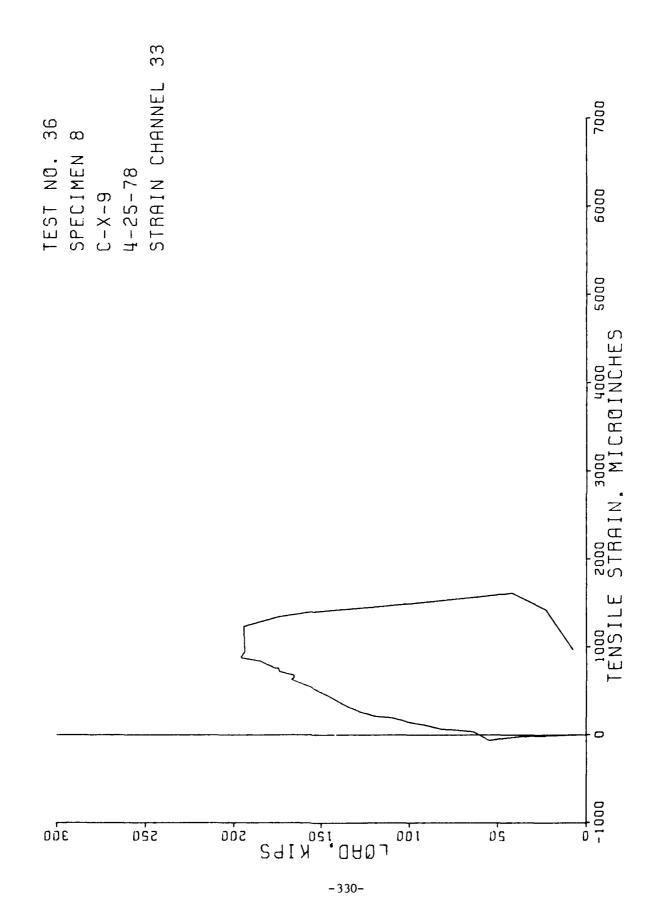


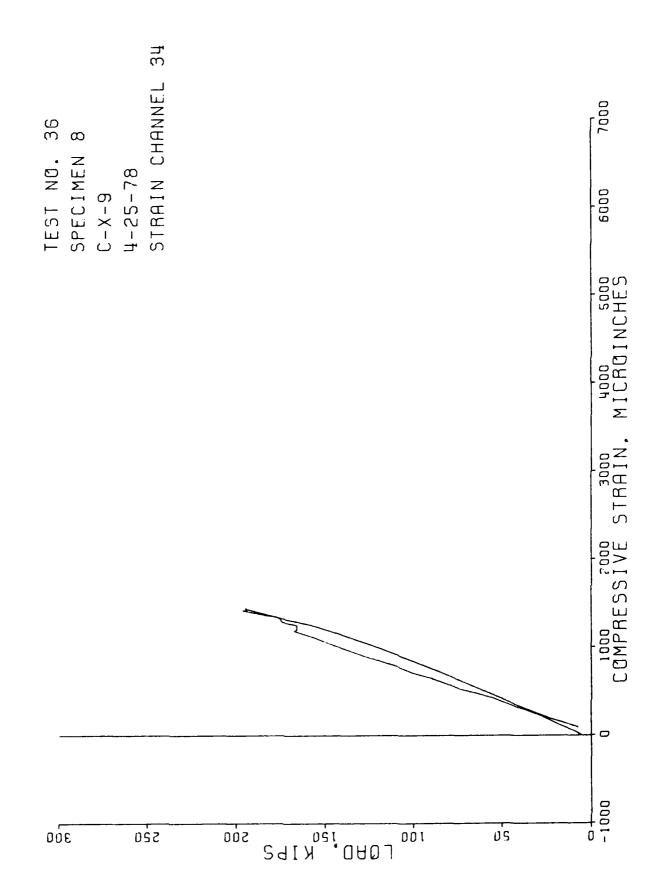


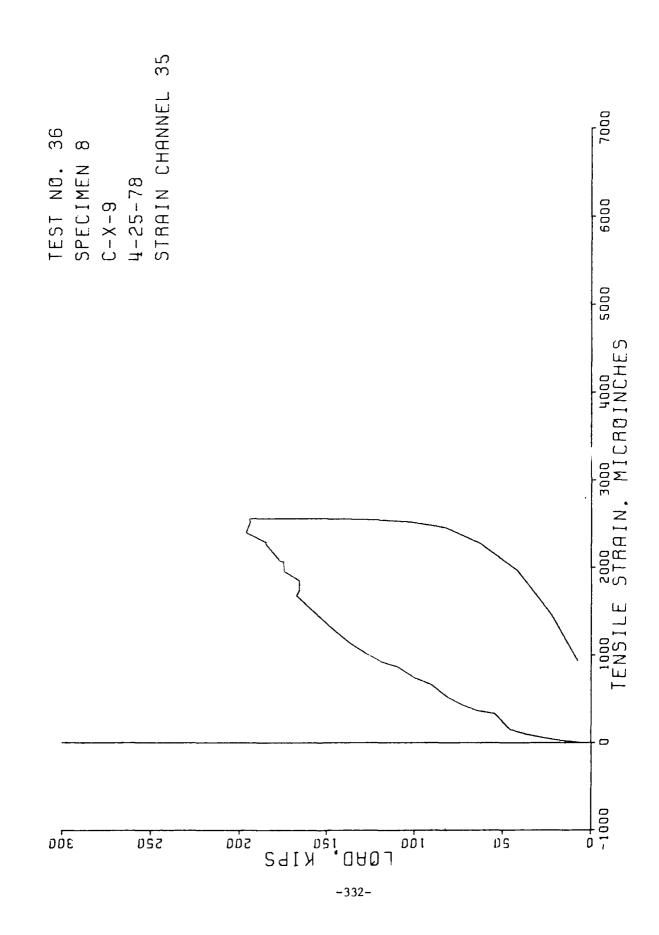


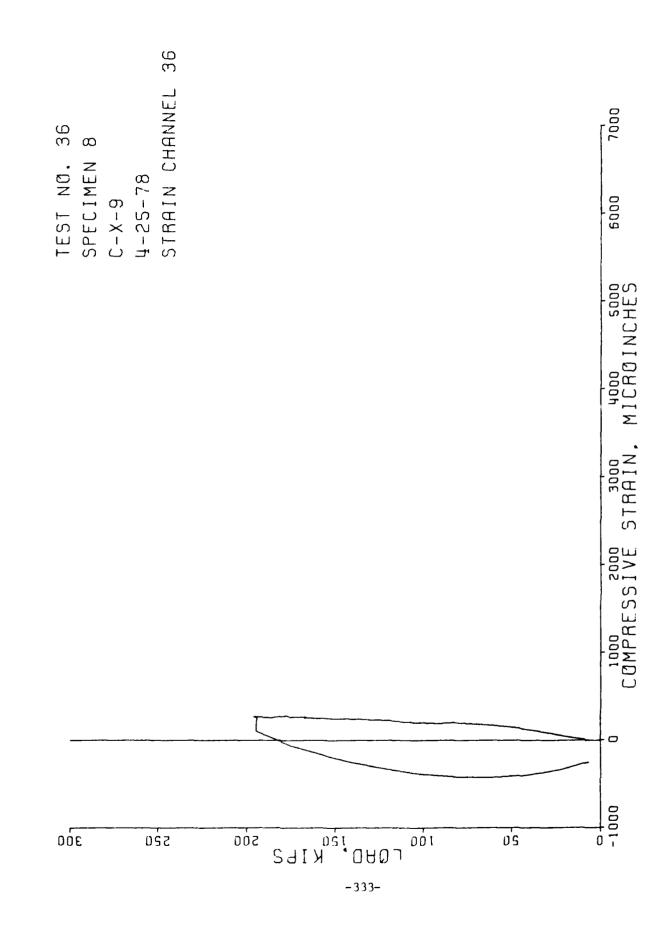


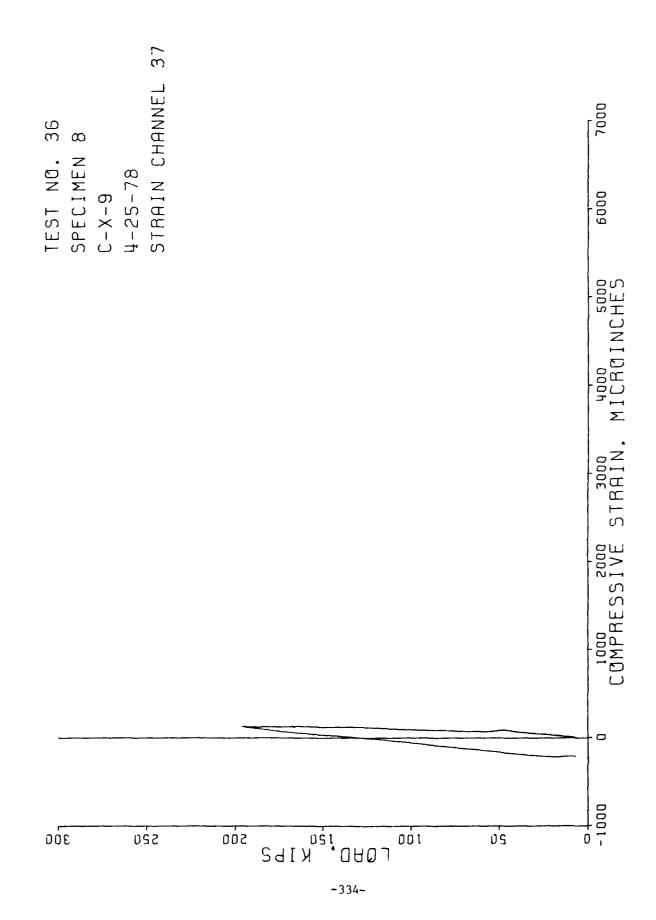


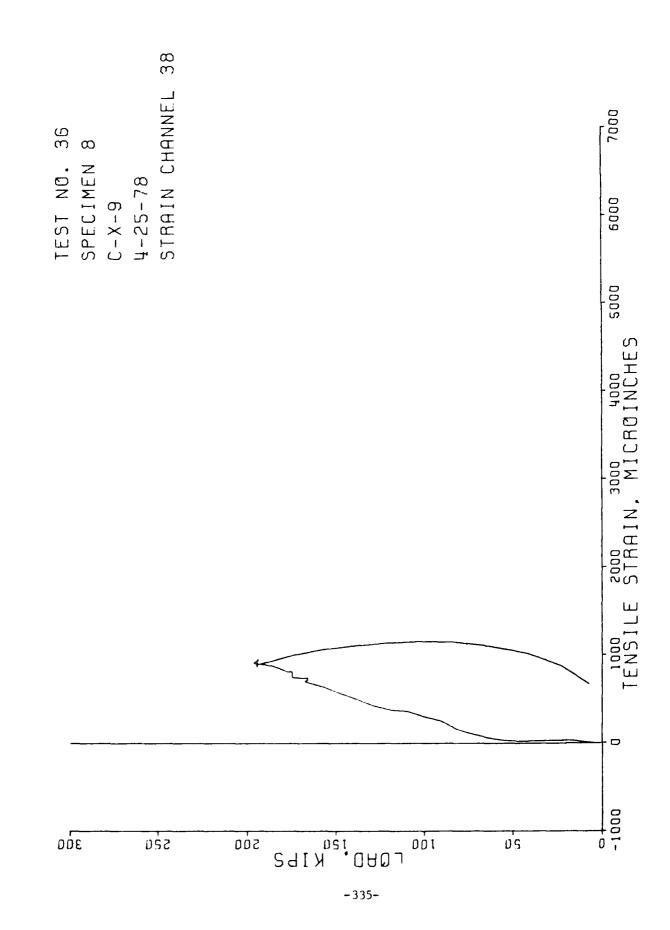


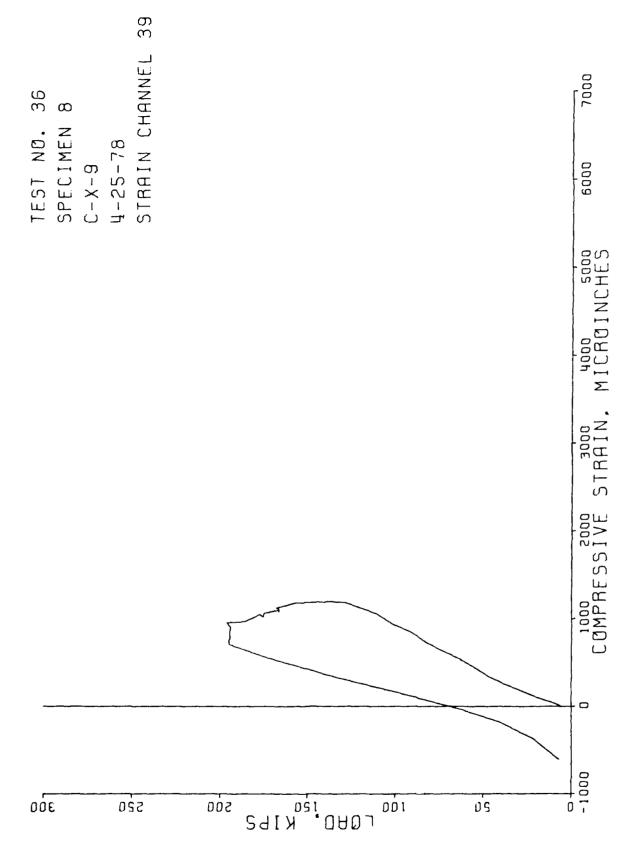


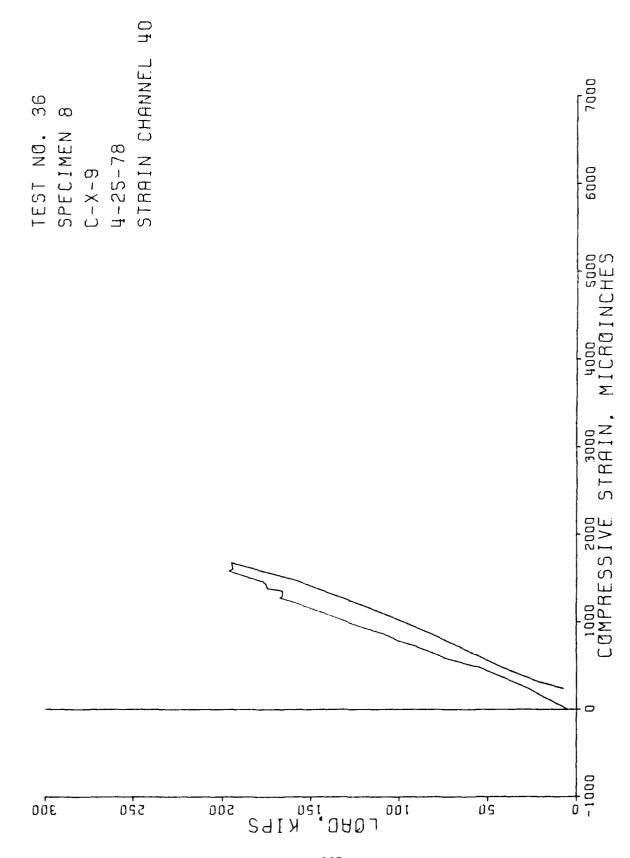


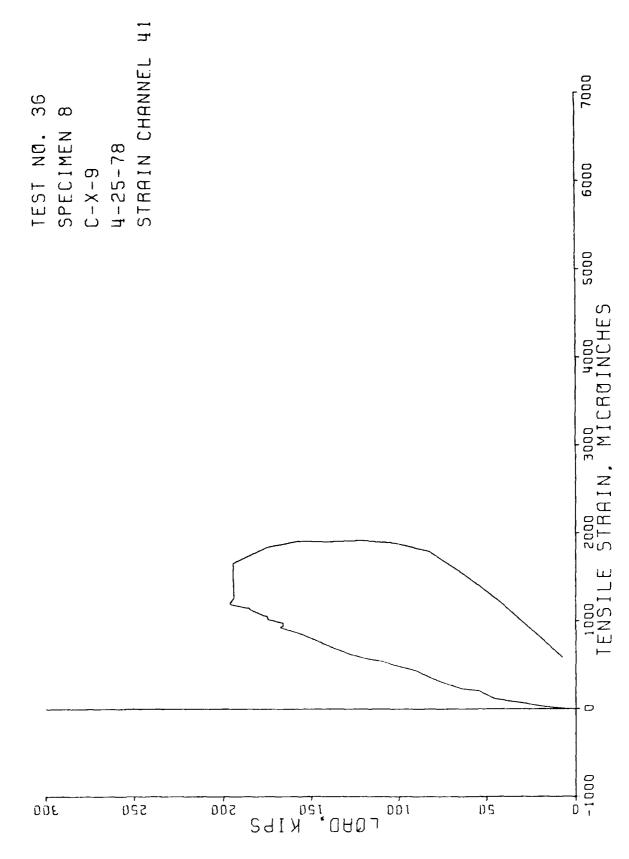












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102.494	115.306	115.306	128.118	115.306	128.118	256.236	358.730	358.730	422.789	499.660	627.778	743.084	832.767	858.390	743.084	461.225
-64.059																
-371.542	-358.730	-358.730	-358.730	-358.730	-358.730	-230.612	-38.435	-38.435	371.542	538.095	525.284	435.601	307.483	192.177	76.871	-64.059
-1153.062	-1127.438	-1114.626	-1114.626	-1101.814	-1089.003	-396.826	-730.272	-730.272	-397.166	-102.494	76.871	115.306	128.118	140.930	76.871	25.624
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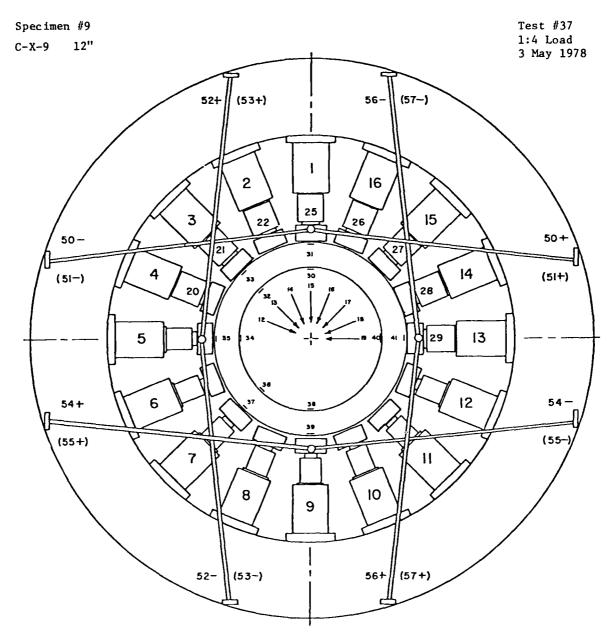
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## 3.4.6 SPECIMEN #9

TEST NO. 37
COMPOSITE INTEGRAL LINER
1:4 LOADING RATIO
TESTED 3 MAY 1978

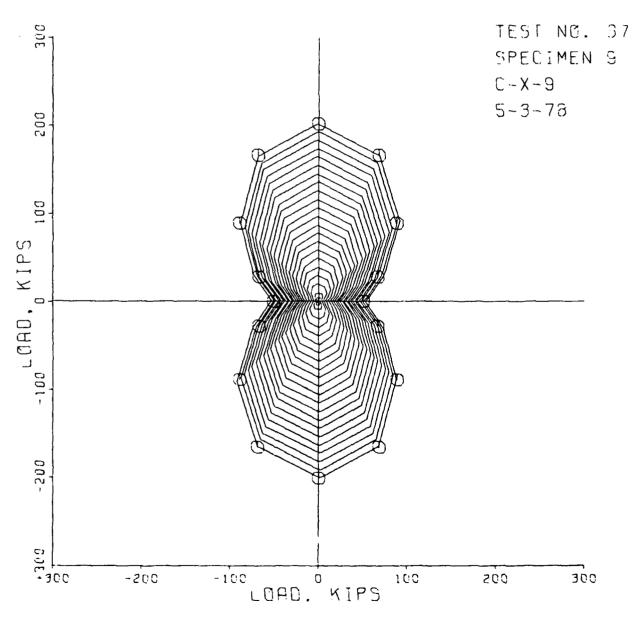
## REACTION FRAME TEST SET-UP

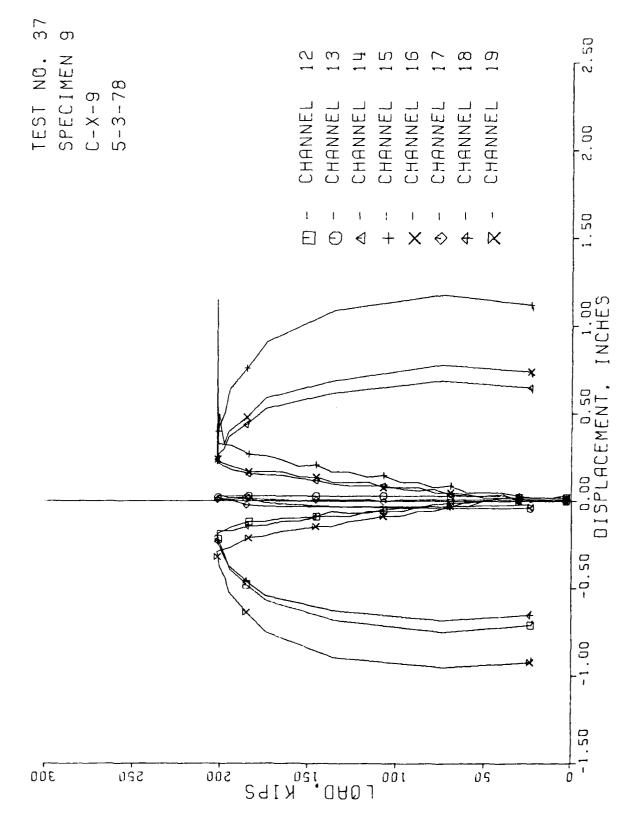


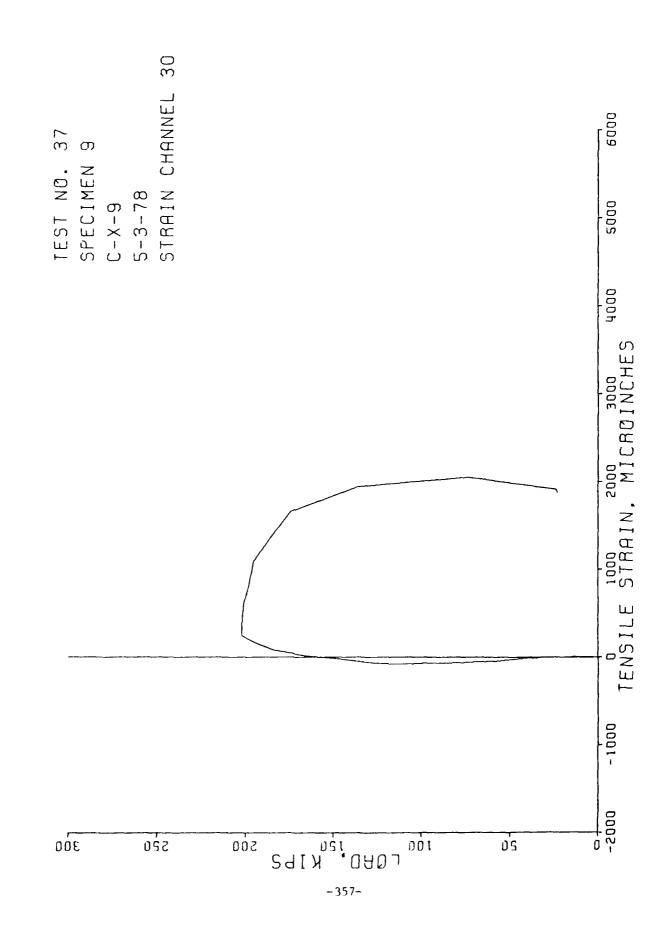
CH 12-19 Load axis I.D. (Research, Inc. Model 4040).

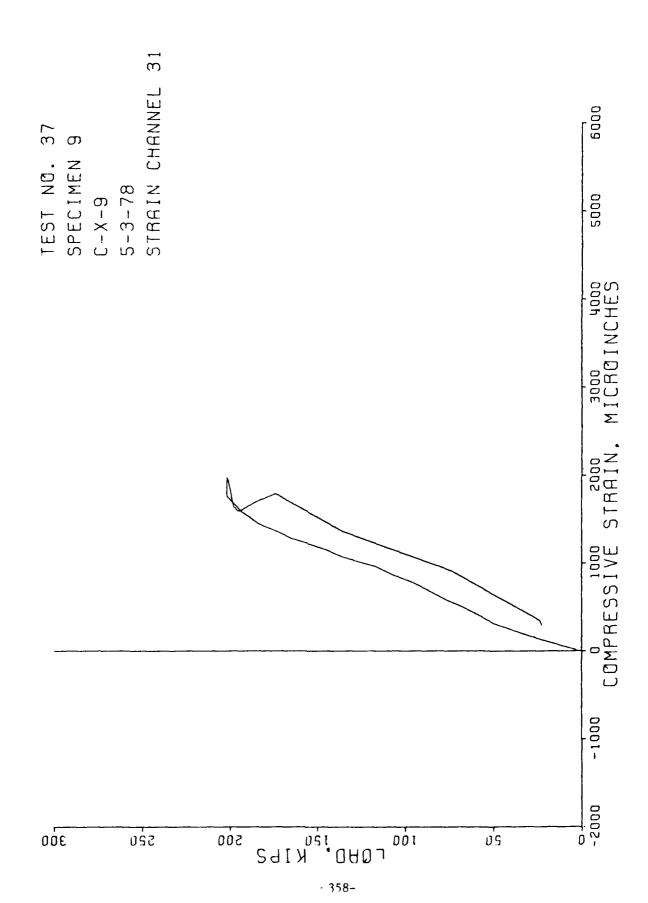
CH 20-22, 25-29 Axial load (Transducers, Inc. Model 693-300K).
CH 30-41 (Ailtech SG 129-6S) Radial pairs 3" from top. Odd gages on Rebar.

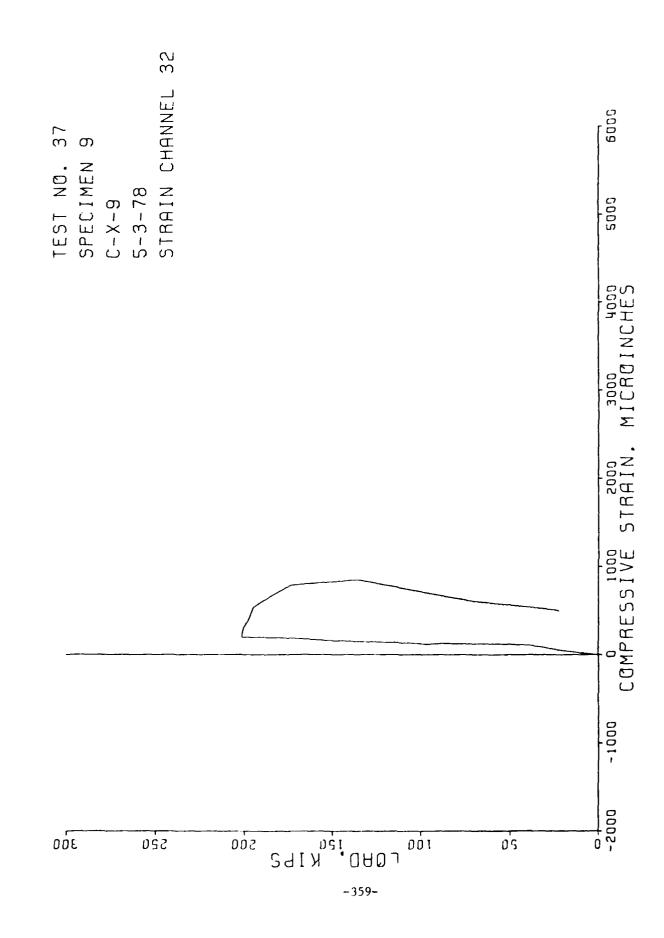
CH 50-57 (Ailtech SG 129-6S) Polarity indicates rod under tension. Lower rod shown (XX).

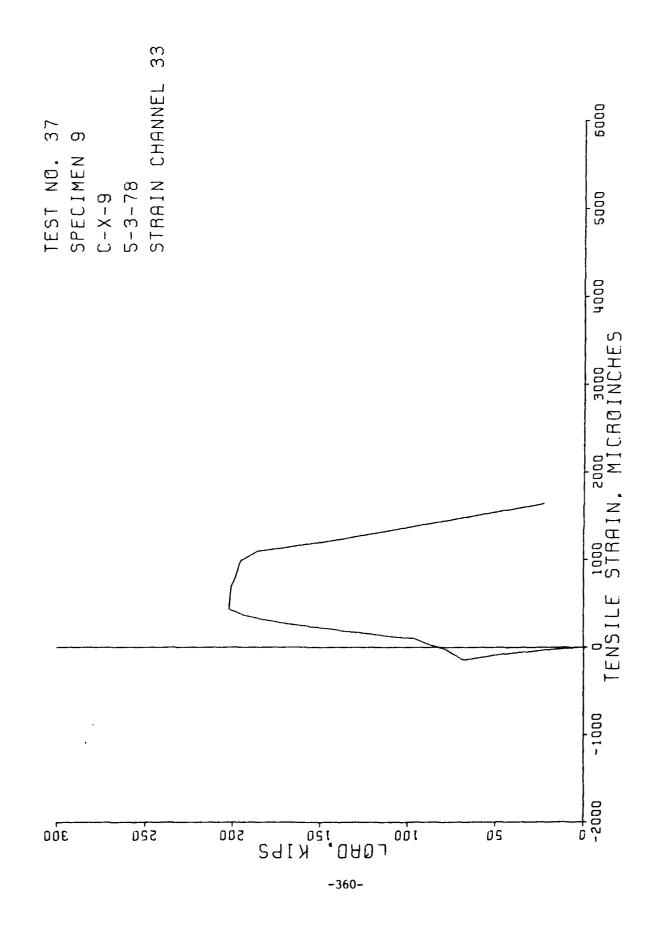


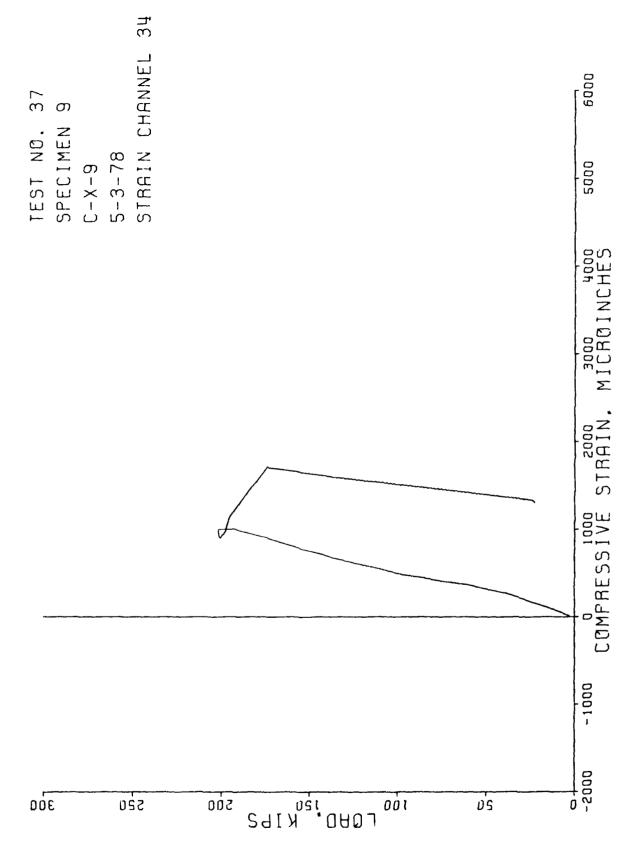


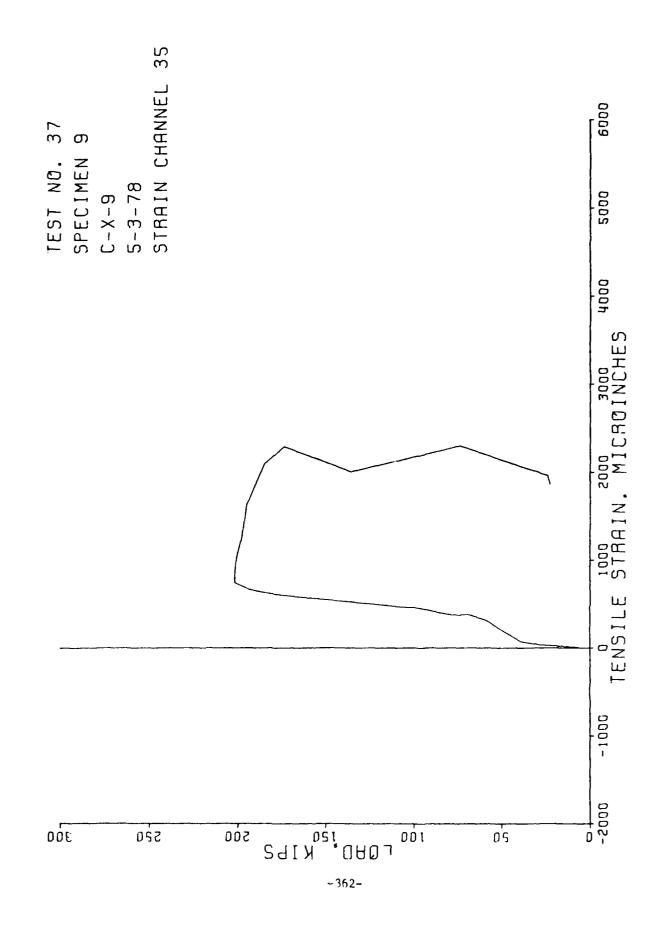


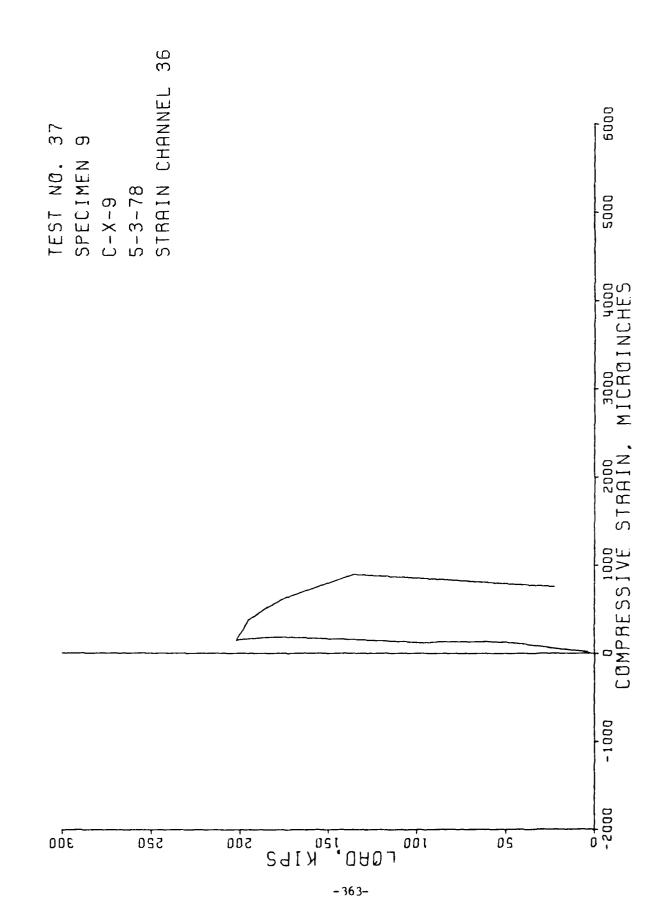


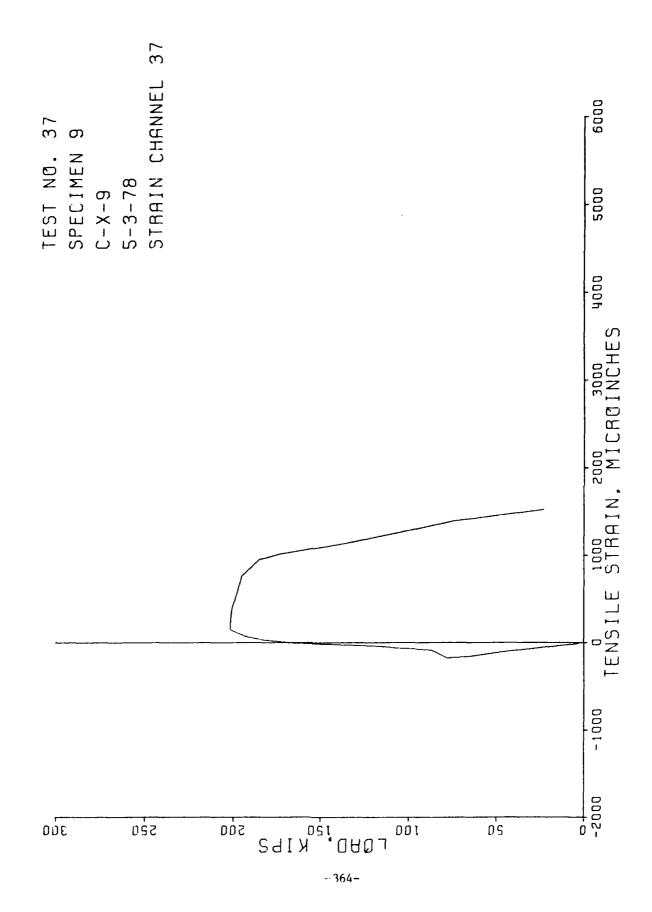


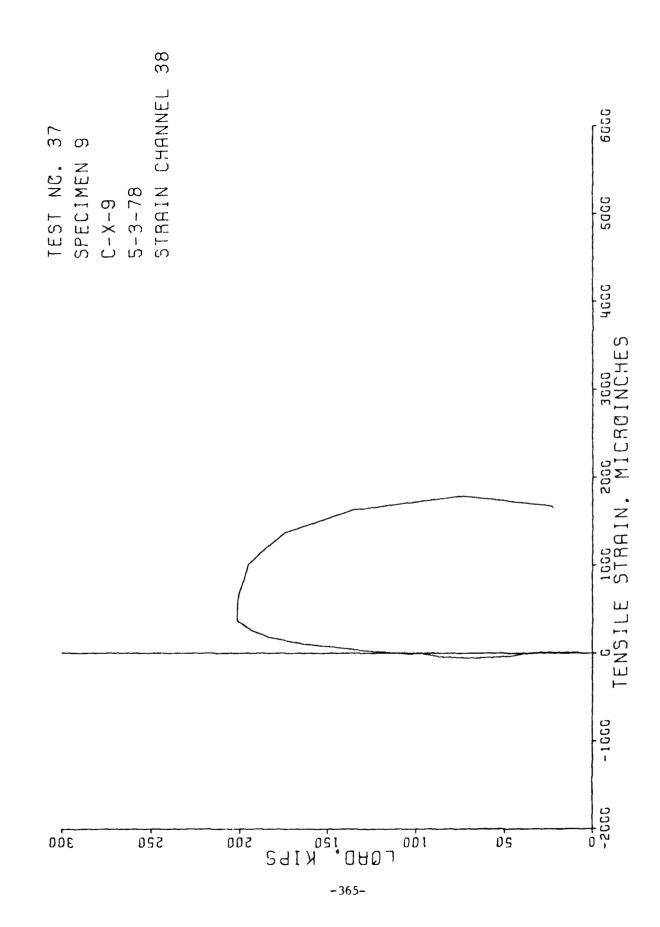


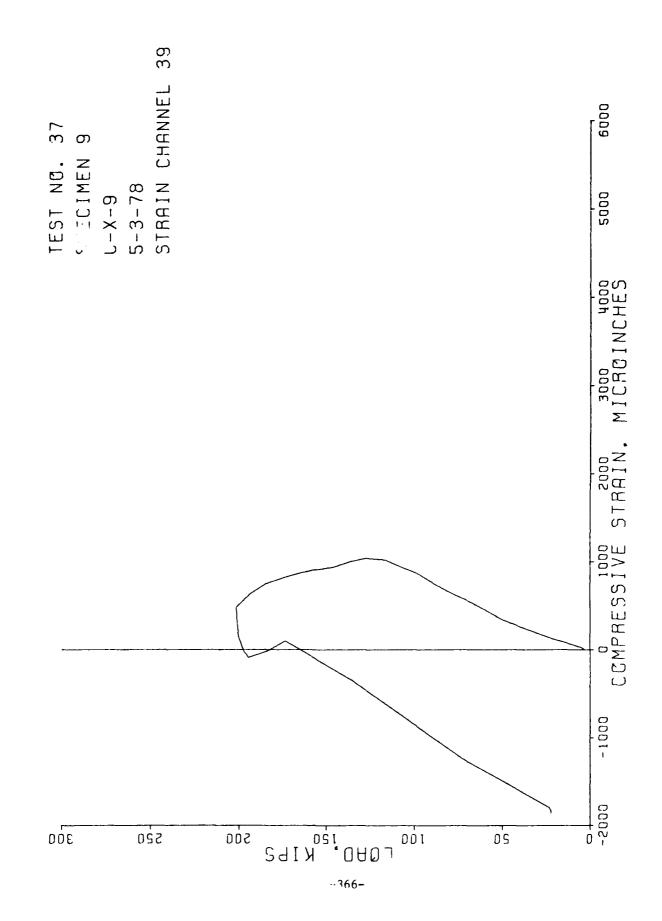


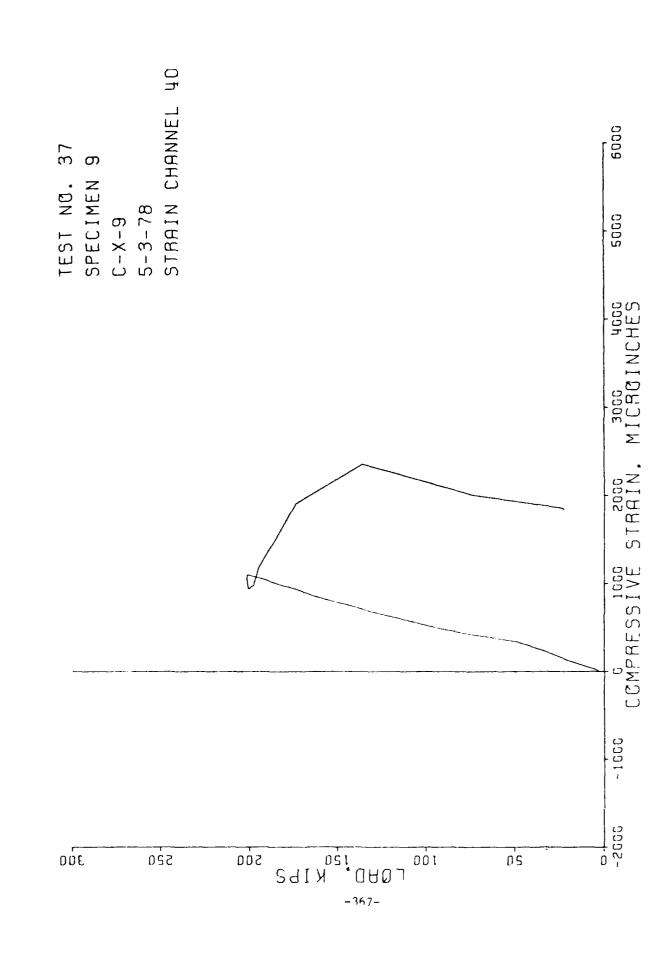


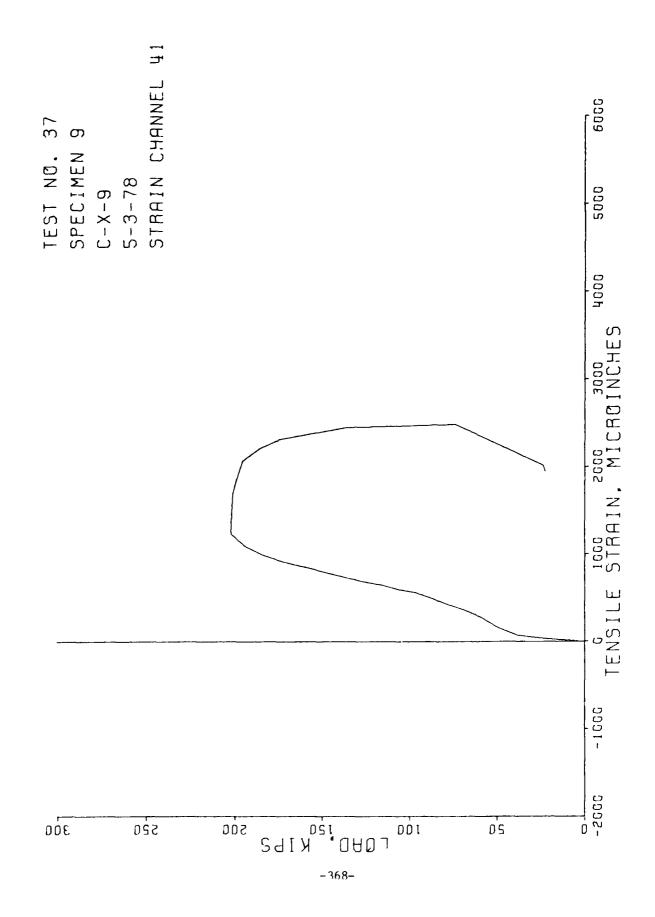












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## 3.5 VOUSSOIR BLOCK LINER 3.5.1 SPECIMEN #7

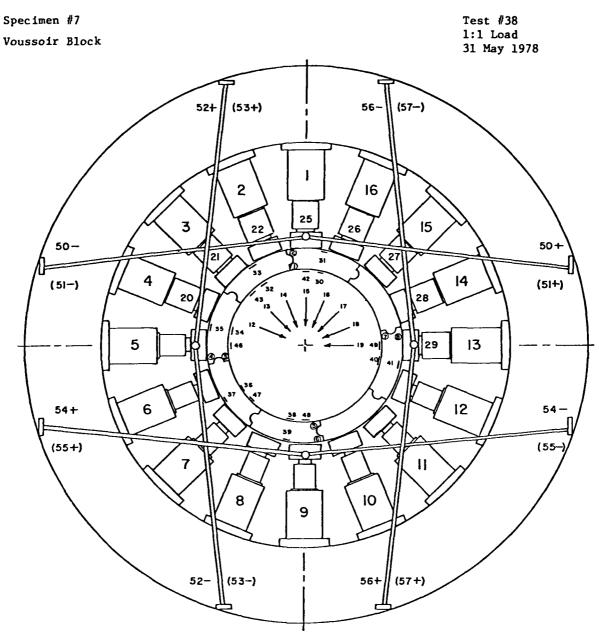
TEST NO. 38

VOUSSOIR BLOCK LINER

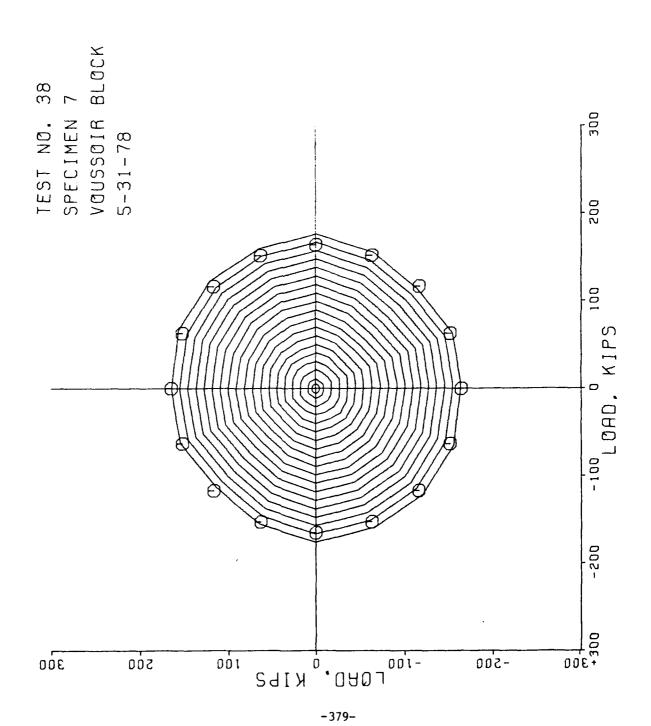
1:1 LOADING RATIO

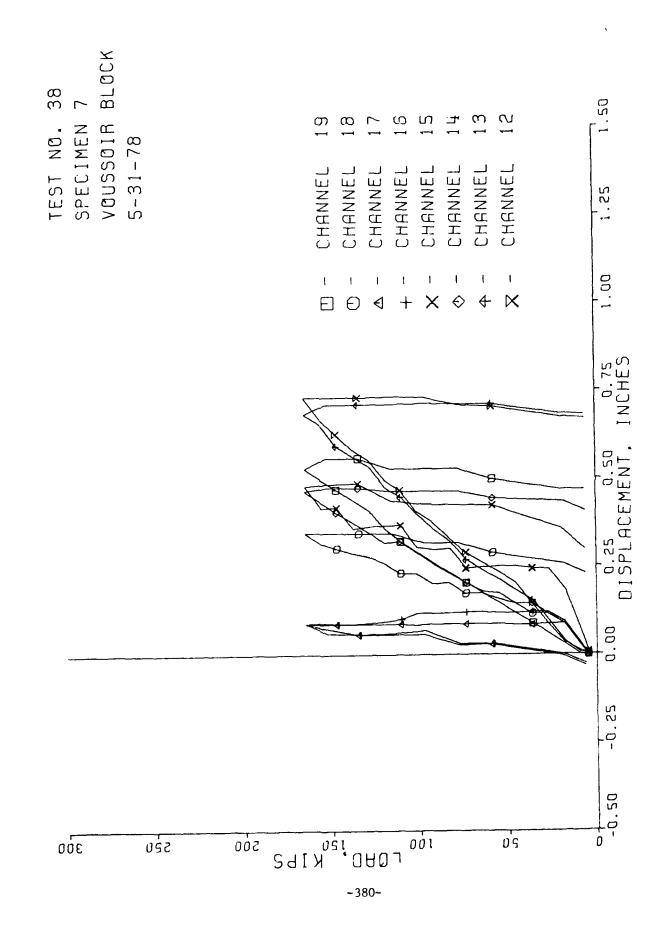
TESTED 31 MAY 1978

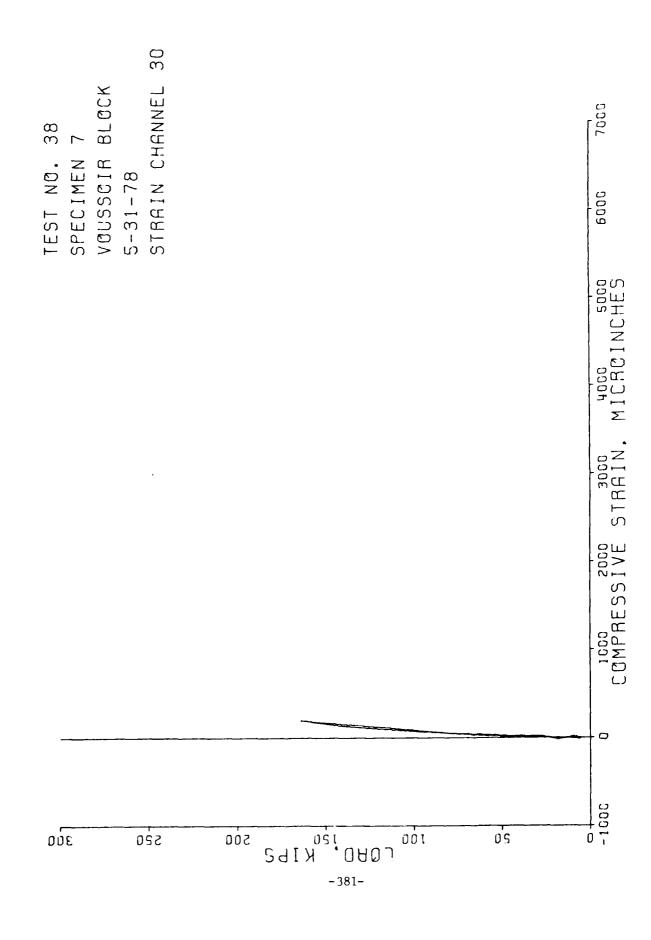
## REACTION FRAME TEST SET-UP

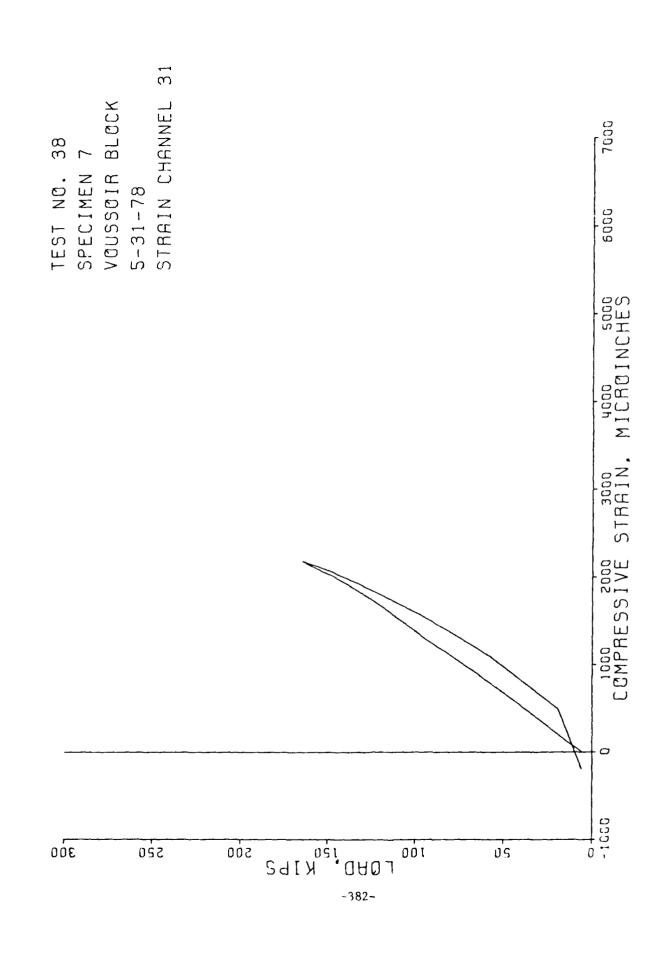


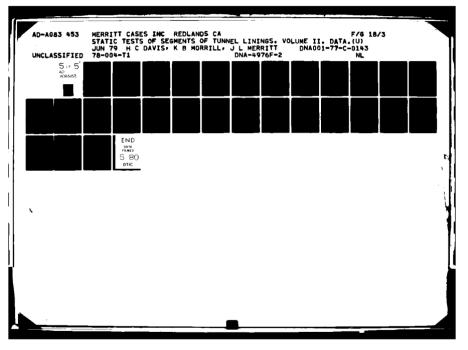
- CH 12-19 Load axis I.D. (Research, Inc. Model 4040).
- CH 20-22, 25-29 Axial load (Transducers, Inc. Model 693-300K).
- CH 30-41, (Ailtech SG 129-6S) Radial pairs between axes 2-1/2" from top. Odd gages on rebar.
- CH 42-43, 46-49, (Ailtech SG 129-6S) on load axes 2-1/2" from top.
- CH 50-57, (Ailtech SG 129-6S) Polarity indicates rod under tension. Lower rod shown (XX).
- Dial Gages 1 8 measure circumferential gap width at the top.

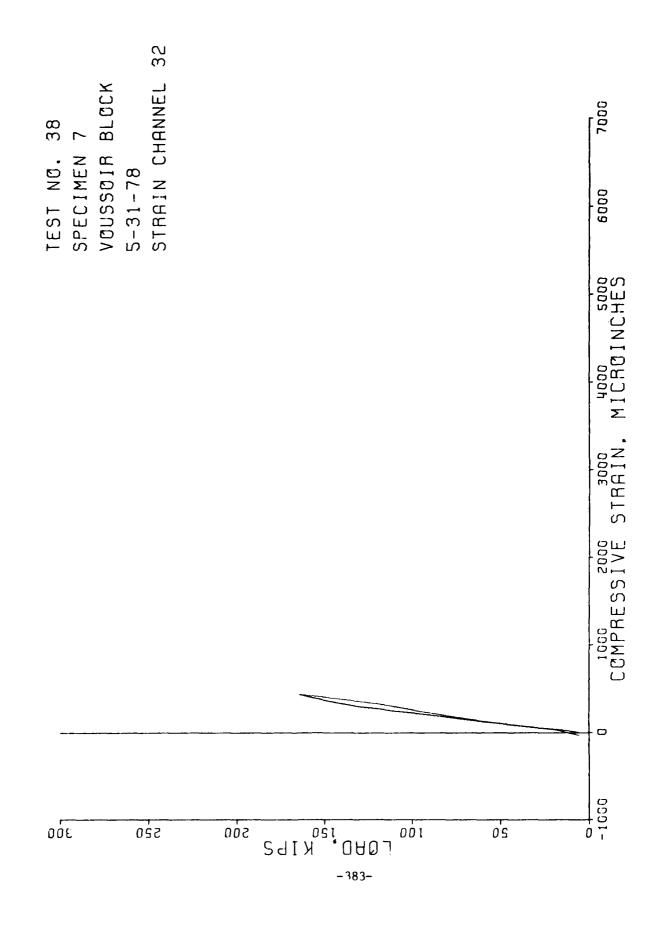


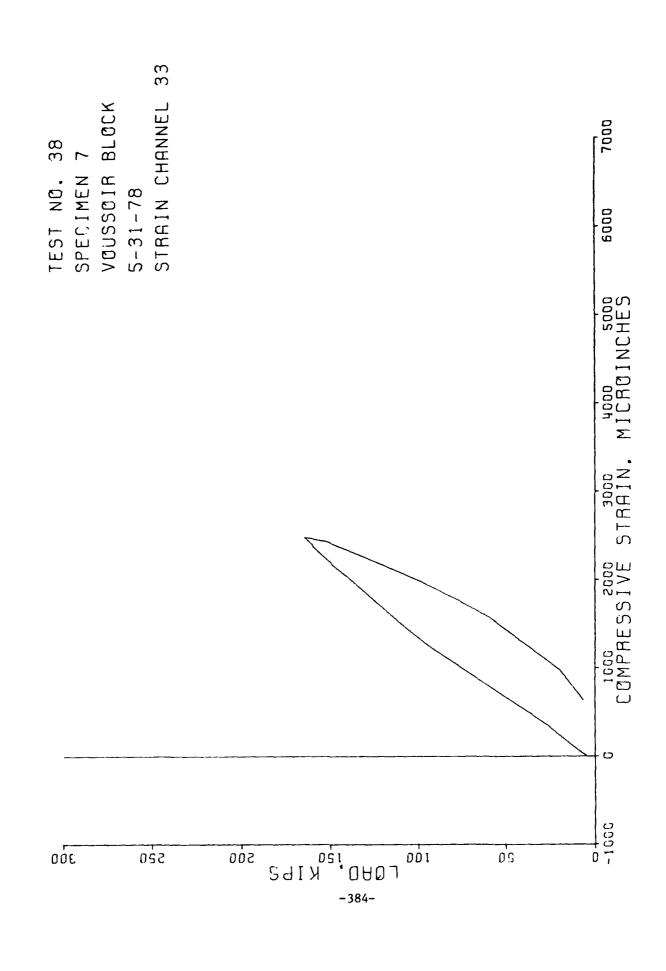


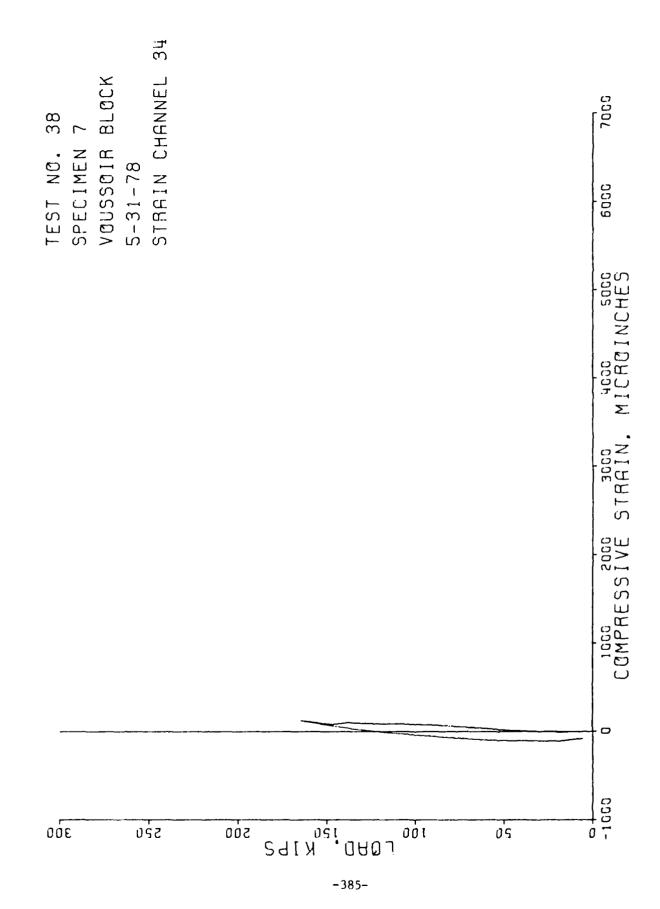


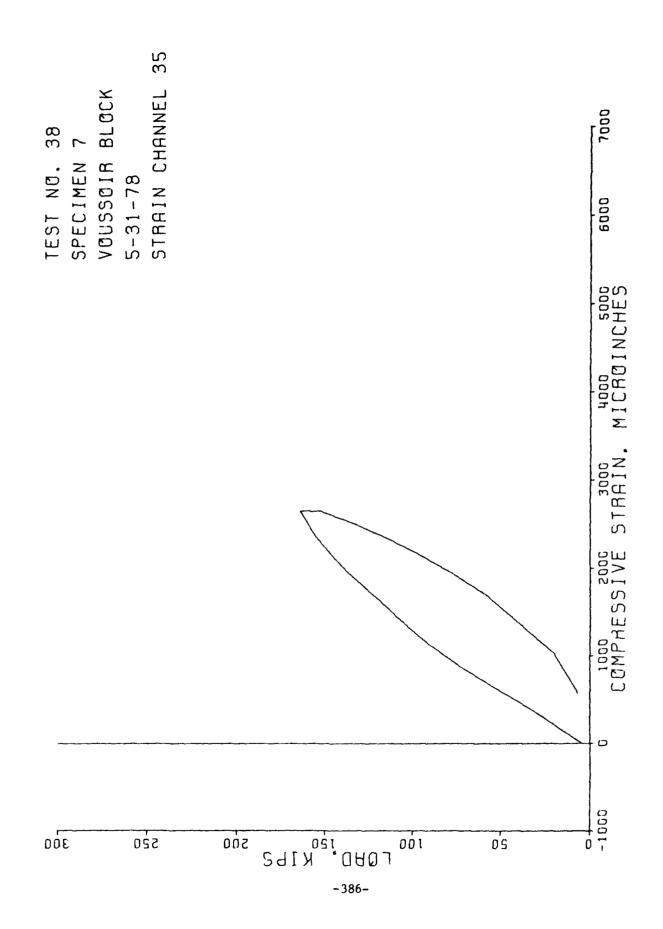


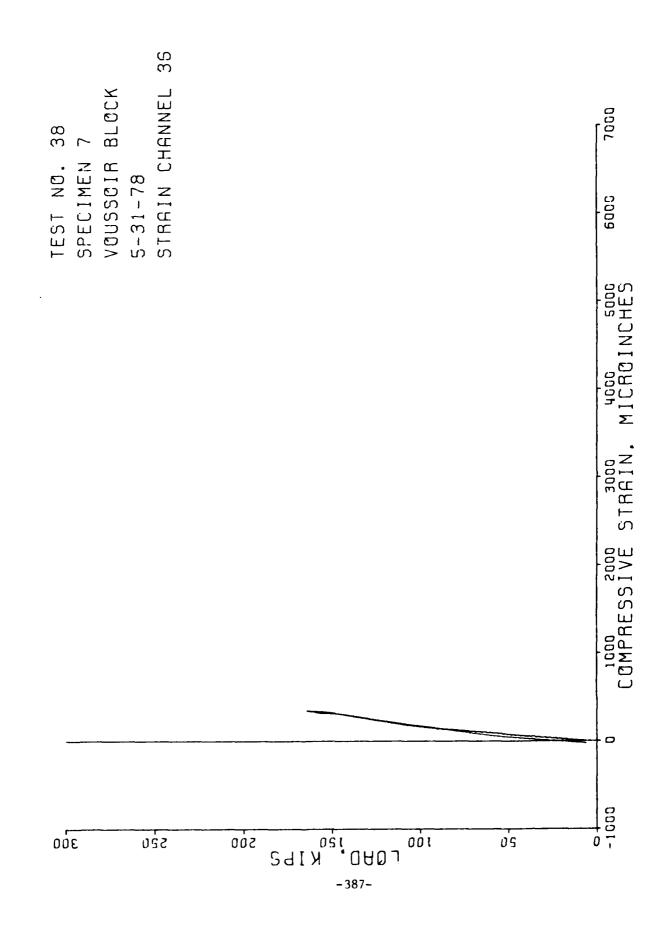


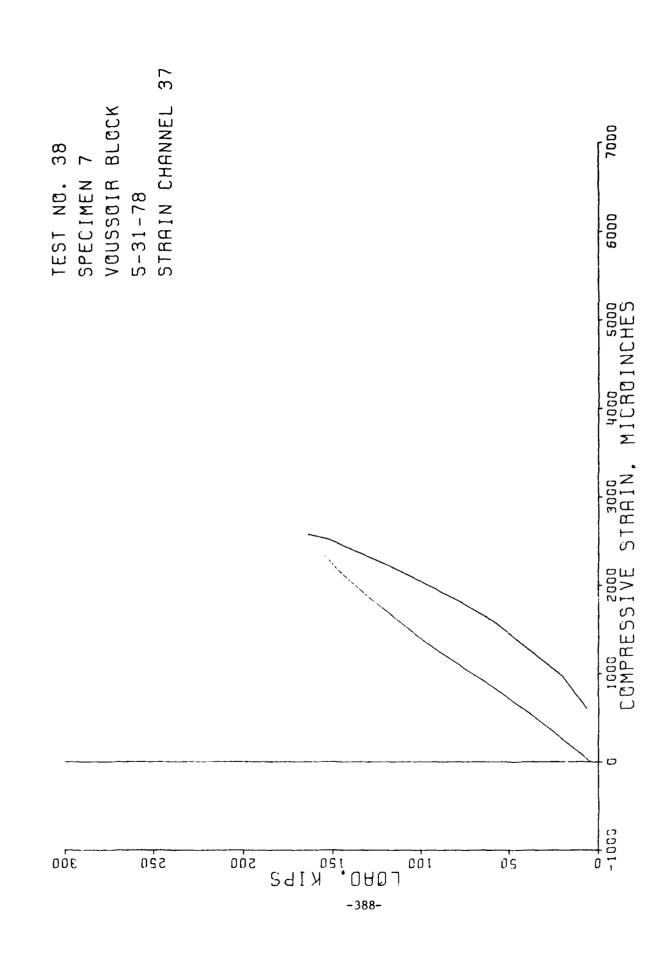


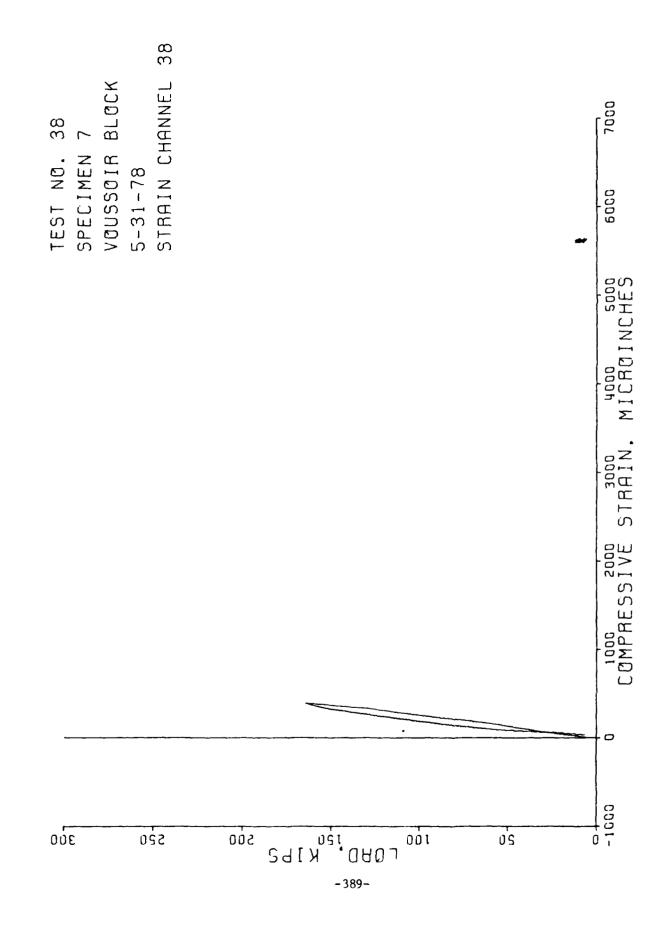


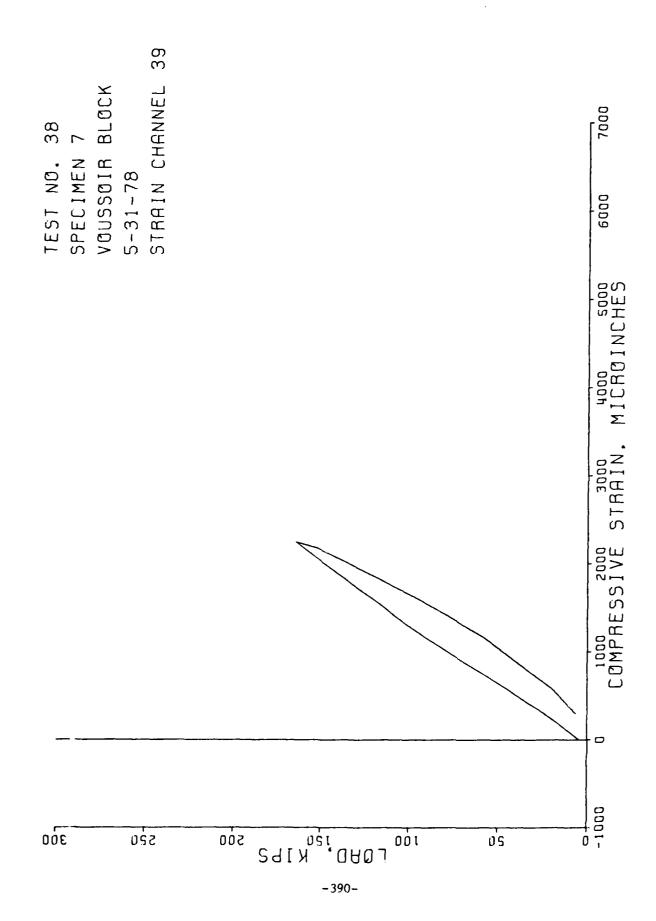


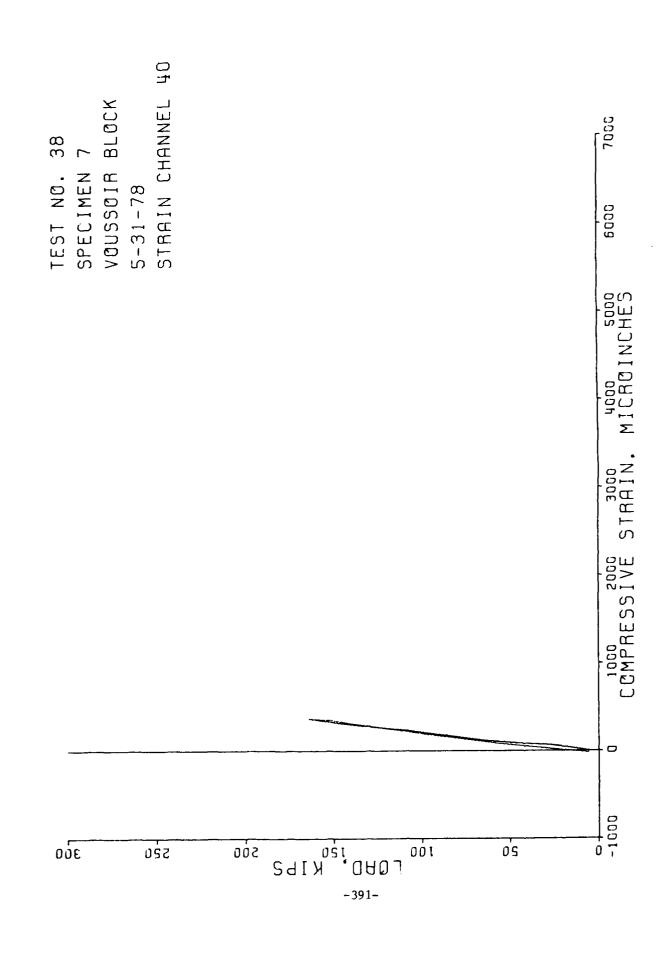


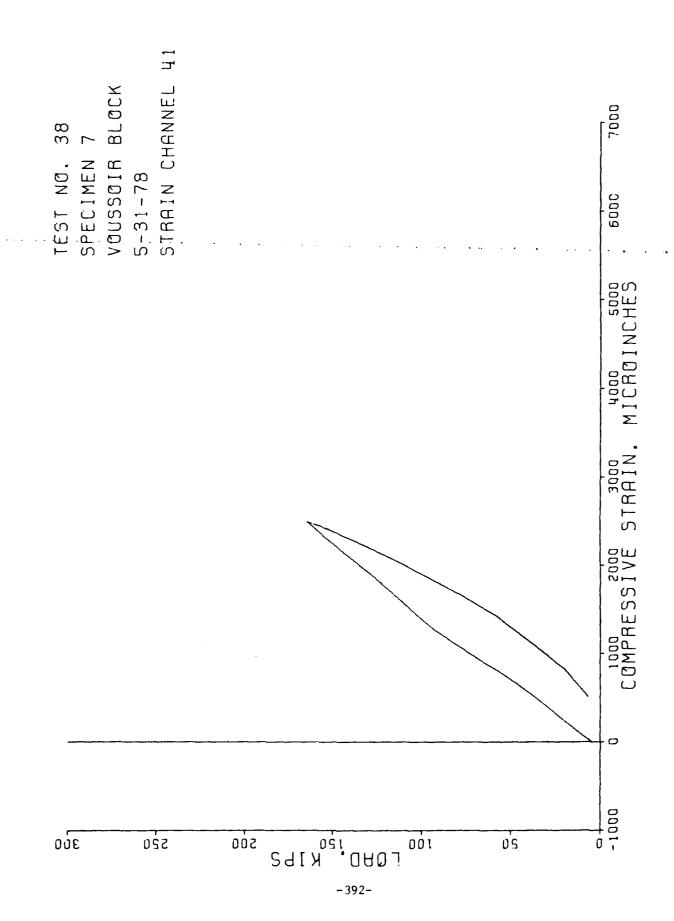


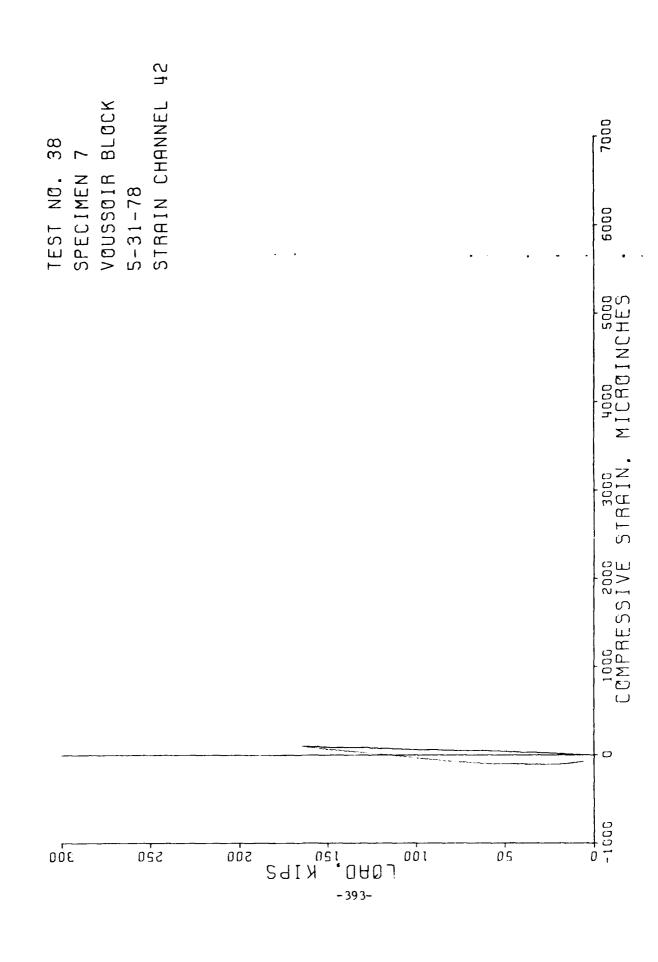


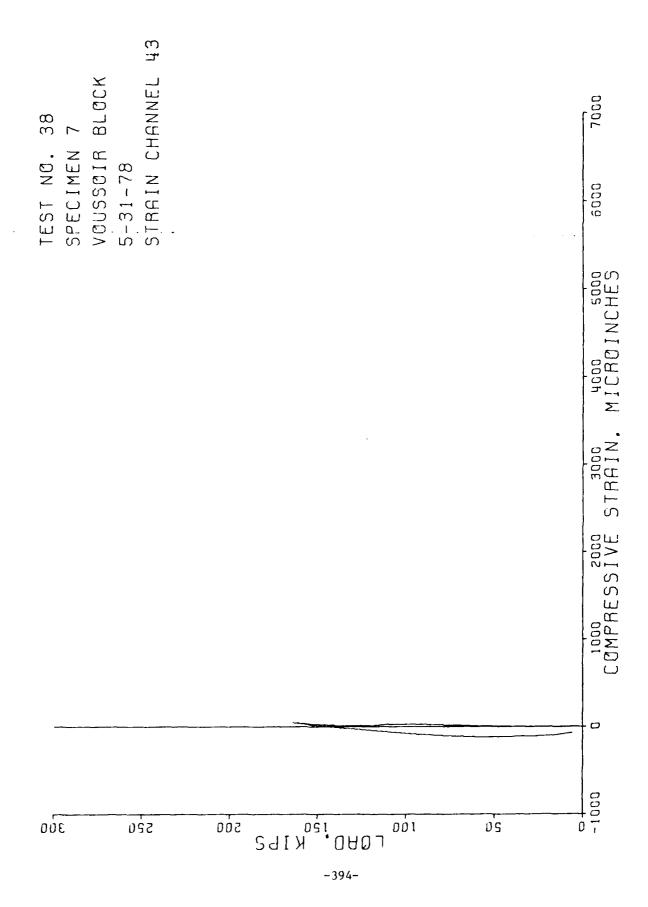


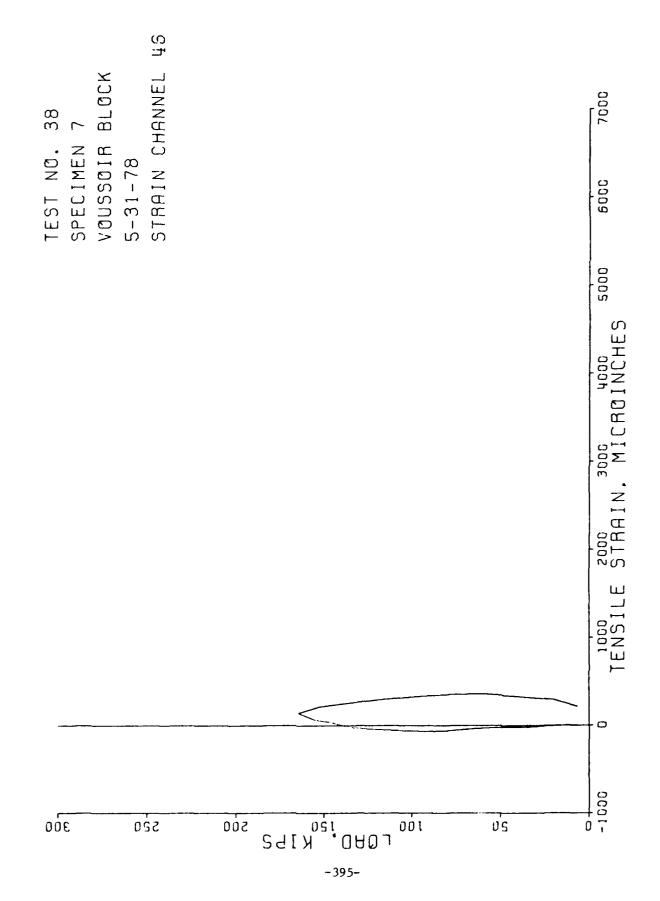


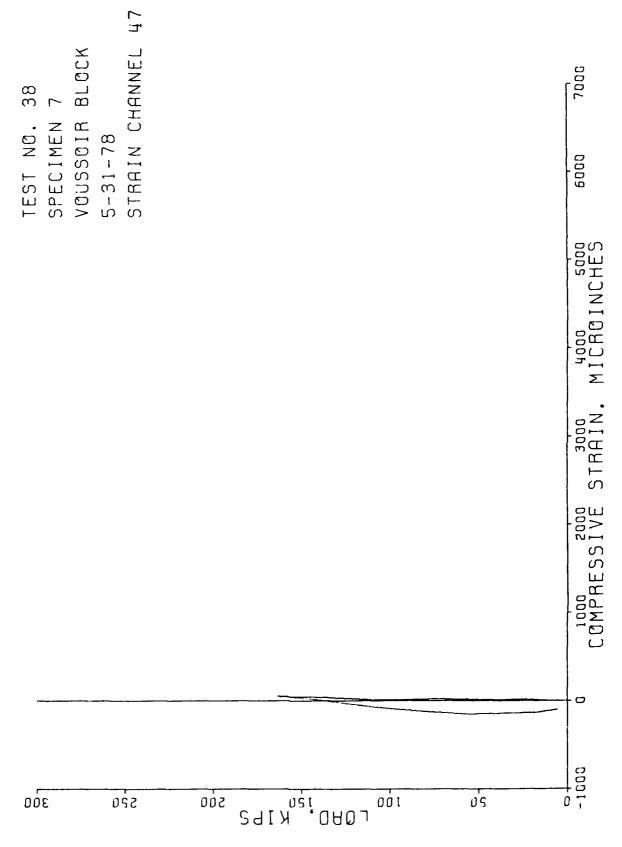


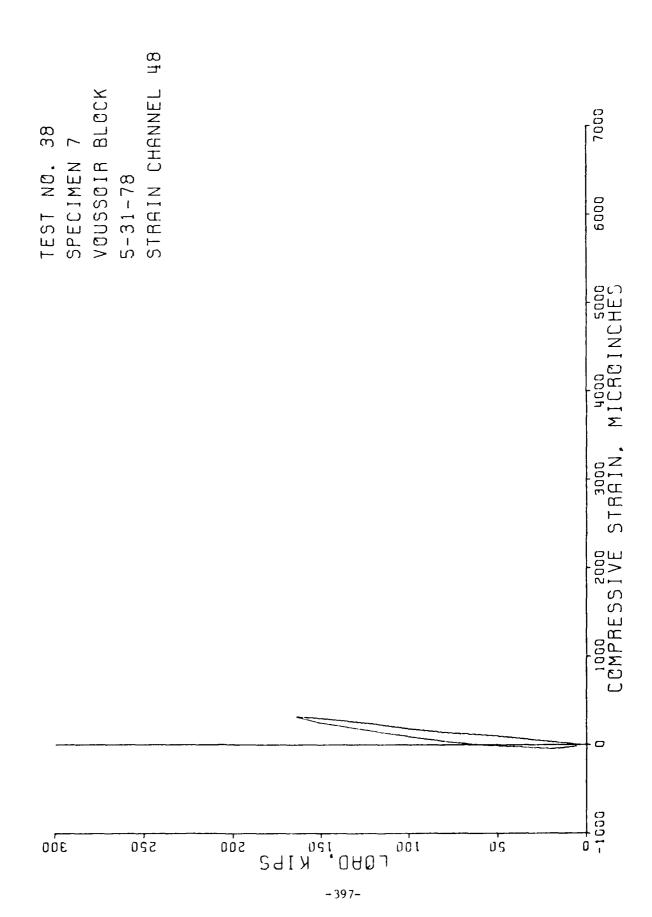


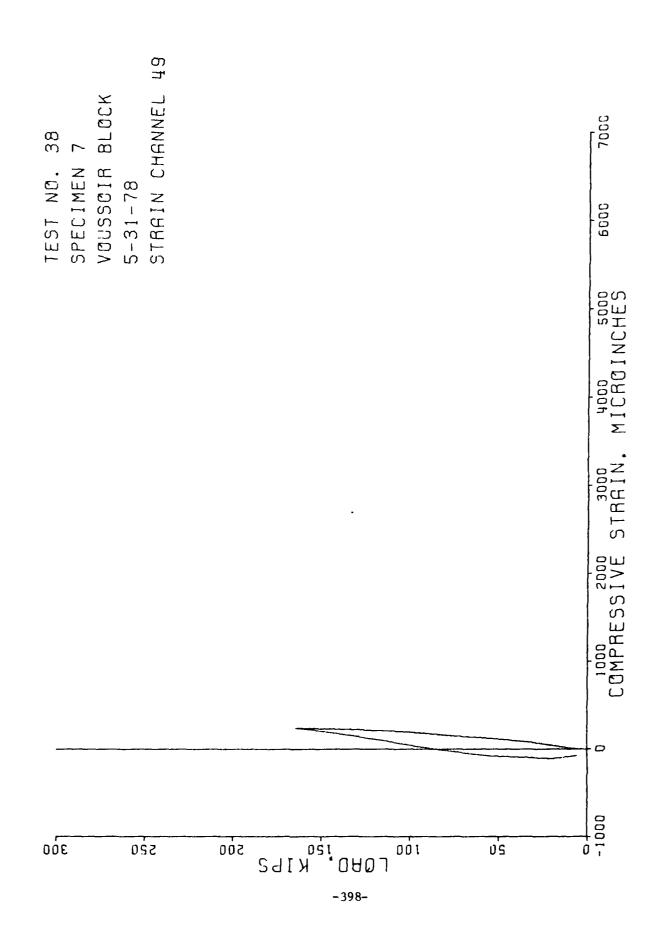












TEST NO. 38 SPECIMEN 7 VOUSSOIR I

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CH.26	5020.000	00	00	0	00	00	00	0	00	00	02920.00	00	22190.00	31530.00	40870.00	50020.00	59820.00	69800.00	57870.00	38880.00	19420.00	00	00	00	00	00
CH.27	4970.000	000	8	00	00	00	00	00	3	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	0
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CH.29	5540	620.0	0.0650	0.0540	0210.0	0.0810	0230.0	5780.0	9410.0	3986.0	8450.0	3496.0	3180.0	7850.0	7300.0	5910.0	5330.0	5850.0	3206.0	3010.0	3340.0	3460.0	3090.0	2550.0	1250.0	5190.0
TIME	31:10:18:18	1:10:23:3	1:10:28:2	1:10:32:5	1:10:37:2	1:10:41:4	1:10:46:1	1:10:51:	1:10:56:1	1:11: 0:4	1:11: 6:	1:11:12:	1:11:18:4	1:11:24:1	1:11:29:1	1:11:33:5	1:11:37:4	1:11:43:2	1:11:47:3	1:11:51:1	1:11:53:1	1:11:55:2	1:11:58:2	1:12: 0:5	1:12: 6:1	1:12: 8:5
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CH.51	60.4.000	370.8 370.8 370.8 563.0	780.87	1665.534 1563.039 1434.921 1255.556 1050.557	0024.9 973.6 768.7 448.4 166.5 604.9
CH.52	0.0 56.55 58.55 59.341	34.50 36.05 36.05 36.05 36.05 36.05	11.79 32.08 39.57 72.67	31.40 10.13 59.16 51.02	4420.070 5082.223 5082.223 50816.5941 5919.047 58457.488 48845.8884
CH.53	20.00	233.18 23.18 21.58 1.59	48.4 99.6 10.9	8079.0 935.2 140.2 383.5	1450.545 1755.216 2037.0206 2139.570 2126.758 1345.888 807.143
CH.54	102.4 102.4 102.4 192.1	20000000000000000000000000000000000000	932 265.5 496.2 50.0	2522.3 2522.3 2522.3 3.8 3.8 3.8	5368.141 5368.141 6958.520 6291.969 3536.056 2767.348 1652.722
CH.55	42,800	1018	2222	9000 C	. 388 . 730 . 384 . 334 . 384 . 384 . 384 . 384 . 153 . 742 . 151 . 247 . 125 . 624 . 25 . 624
CH.56	12.812 -204.989 -486.348 -307.483	102.494 345.918 627.778 948.073	716	3074.832 3574.491 4086.963 4637.867 5201.590	4919.750 4061.340 32061.340 2756.535 2344.559 1911.770 1114.626
CH.57	2.68 2.63 3.67 8.67	2011 2017 2017 2017 2017 2017 2017 2017	728.91 074.83 471.99 869.16	540.70 599.43 345.35 739.68	5496.258 4778.758 4048.797 5664.174 3664.174 2293.3879 1985.829
TIME	31:10:18 31:10:19 31:10:23 31:10:28		. 31:11: 0 . 31:11: 6 . 31:11: 6 . 31:11:12	31:11:29 31:11:29 31:11:29	0. 31:11:47:30 1. 31:11:51:15 3. 31:11:53:15 4. 31:11:58:29 5. 31:12: 6:18 7. 31:12: 8:59

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